Technical Report

Mirador Project, Morona Santiago Province, Ecuador

Prepared for:
Corriente Resources Inc.
by:
Susan Lomas, P.Geo

Effective Date: 22 October 2004

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CERTIFICATE OF AUTHOR

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I have practiced my profession continuously since 1987 and have been involved in: mineral exploration for gold, nickel, copper, zinc, and silver in Canada, United States, Mexico, Venezuela and Ghana and in underground mine geology, ore control and resource modelling for gold, nickel, copper, zinc, silver, potash and industrial mineral properties in Canada, United States, Peru, Thailand, China, Ecuador, Brazil, New Caledonia and Russia.

As a result of my experience and qualifications, I am a Qualified Person as defined in N.I. 43-101.

I am currently a Consulting Geologist and have been so since January 2000.

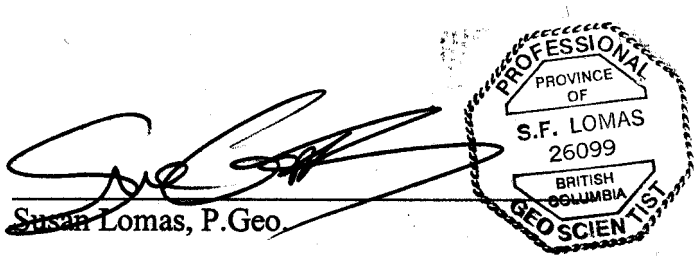
From January 19, 2004 until January 24, 2004 I visited the Mirador project in Ecuador. I completed the mineral estimation work for the Mirador Project. This report was prepared under my direct supervision.

I am not aware of any material fact or material change with respect to the subject matter of this technical report that is not reflected in this report and that the omission to disclose would make this report misleading.

I am independent of Corriente Resources Inc. in accordance with the application of Section 1.5 of National Instrument 43-101.

I have read National Instrument 43-101 and Form 43-101FI and this report has been prepared in compliance with same.

Dated at Vancouver, British Columbia, this 22nd day of October 2004.



Susan Lomas, P.Geo.

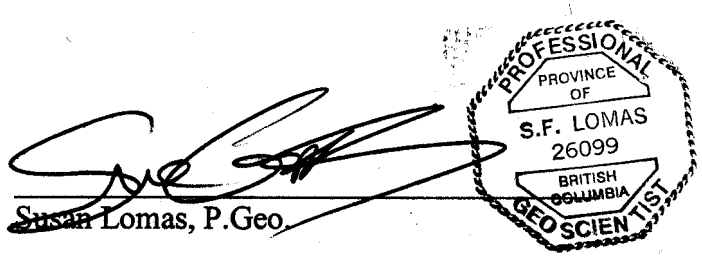
CONSENT OF QUALIFIED PERSON

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Securities Commission of Newfoundland
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Securities Registry, Government of the Northwest Territories

AND TO: Corriente Resources Inc.

I, Susan F. Lomas, P.Geo., do hereby consent to the filing of the technical report prepared for Corriente Resources Inc. and dated October 22, 2004 in respect of the Mirador project, Ecuador, in support of the news release dated September 22, 2004, which are based on and are consistent with the information contained within the technical report.

DATED at this 22nd day of October 2004.



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I am a member of the Engineering Council of South Africa. I graduated from the University of Strathclyde with a Bachelor of Science (Honours) degree in Chemical and Process Engineering in 1982.

I have practiced my profession continuously since 1982 and have been involved in: mine process production, research and development, engineering and construction for gold and silver, platinum group metals, uranium, chrome, coal and industrial minerals in South Africa and in process engineering and consulting for copper, zinc, gold, silver, platinum group metals, tantalum, uranium, iron ore, coal and industrial mineral properties in Canada, United States, Peru, Argentina , Chile, Ecuador, Ethiopia, Ukraine, Mongolia, Russia and the Middle East.

As a result of my experience and qualifications, I am a Qualified Person as defined in N.P. 43-101.

I am currently a Consulting Metallurgist and have been so since September 1995.

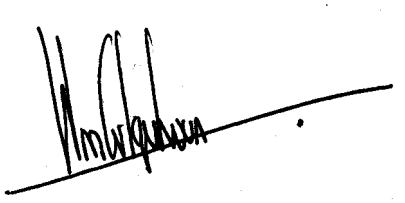
From November 10, 2004 until November 19, 2003 I visited the Mirador project in Ecuador. I also helped to direct the metallurgical sample collection. The metallurgical testwork supporting this report was conducted under my direct supervision and I prepared the metallurgical section of this report.

I am not aware of any material fact or material change with respect to the subject matter of this technical report that is not reflected in this report and that the omission to disclose would make this report misleading.

I am independent of Corriente Resources Inc. in accordance with the application of Section 1.5 of National Instrument 43-101.

I have read National Instrument 43-101 and Form 43-101FI and this report has been prepared in compliance with same.

Dated at Vancouver, British Columbia, this 22nd October 2004.



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1.0 SUMMARY

Corriente Resources Inc. (Corriente) engaged AMEC Americas Limited (AMEC) to provide a mineral resource estimate and Qualified Person's review and Technical Report for their Mirador Project in southeastern Ecuador. The work entailed estimating mineral resources in conformance with the CIM Mineral Resource and Mineral Reserve definitions referred to in National Instrument (NI) 43-101, Standards of Disclosure for Mineral Projects. It also involved the preparation of this Technical Report as defined in NI 43-101 and in compliance with the format set out in 43-101F1. Susan Lomas, P.Geo., an employee of AMEC, served as the Qualified Person responsible for preparing the resource estimation and this Technical Report. The author completed a site visit to the Mirador Project between the 19th and 24th of January, 2004. William Colquhoun, Pr Eng., an employee of AMEC, served as the Qualified Person responsible for the metallurgical study work and is responsible for the information presented in Section 16 (Mineral Processing and Metallurgical Testing) of this report.

The Mirador Project is located along the valley of the Rio Zamora (Zamora River) in the Morona Santiago Province of southeast Ecuador, adjacent to the border with Perú. The concessions are approximately 340 km south of Ecuador's capital city of Quito and 70 km east-southeast of the city of Cuenca.

Regional exploration was initiated in southeastern Ecuador by BHP Billiton S.A. in 1994 and they identified possible porphyry copper systems in the region. In October 1999, BHP Billiton entered into an option agreement with Corriente Resources Inc. covering 880 km^2 in the northern part of the porphyry belt. Subsequently, BHP Billiton and Corriente entered into a further agreement in April 2000 covering 230 km^2 in the southern part of the porphyry belt (the Mirador – Chancho property).

In 2002, after completion of 52 diamond drill holes, results of a polygonal resource estimate were released (12 February 2002). The estimated tonnage and grade, calculated at a 0.65% Cu grade, were 218 Mt grading 0.73% Cu, all in the Inferred Mineral Resource category.

In 2003, Corriente released a second mineral resource for the Mirador Project in a NI-43-101 Technical Report (February, 2003). The updated resource estimate was based on 10 additional holes and estimated using polygonal methods. This resource estimate, calculated at a 0.65 Cu % cutoff grade, yielded 182 Mt grading 0.76 % Cu and 0.221 g/t Au. The estimate was classified as Inferred Mineral Resources.

The porphyry copper mineralization of the region is associated with Late Jurassic porphyry intrusive phases of the Jurassic batholiths of the Abitigua Subdivision in the Cordillera Real and sub-Andean regions of Ecuador. The Zamora Batholith, which hosts the known porphyry mineralization, is part of the Abitigua Subdivision.

The core of the deposit is characterized by a circular area of breccia composed of clasts of the host porphyry and granite, and early mineral quartz-stockwork fragments. A series of syn- to post copper mineralization northeast trending, steeply northwesterly dipping, hornblende-feldspar porphyry dykes cut the breccia and the country rocks. Supergene zones of enrichment are weakly developed beneath a superficial leach cap that averages less than 22 m thick.

Mineralization at Mirador can be divided into early molybdenum, early copper ± gold, and late copper-gold stages. Molybdenum is associated with early quartz veining. Chalcopyrite occurs as mainly irregular masses between clasts in the early breccia and as fine disseminations in a halo zone around the breccia within the Zamora granite. A late stage series of 1 cm to 2 cm quartz sulphide stingers transect the project. They are subvertically emplaced but their strike is unknown. These veinlets are sulphide rich and have elevated gold and zinc values.

Since April 2000, Corriente has carried out exploration on the Mirador Project. The work completed has included geological mapping, geochemical soil sampling, rock chip sampling and the completion of 24,350 m of core drilling in 91 diamond drill holes arranged in a grid on approximately 75 m to 100 m centres.

Most drill holes at Mirador were drilled vertically. AMEC believes more angled drill holes should have been drilled due to the presence of various geologic features having sub-vertical contacts (e.g., post-mineral dykes, late quartz-sulphide stringers).

Core recovery is good and is >90% in the zones of primary mineralization. The RQD values measured from the core indicate that rock quality is very low through large parts of the deposit. The average RQD value from the drilling over the whole of the deposit is 38%.

For all drill phases the following procedures remained consistent. The whole sample was crushed to 75% passing –10 mesh, then 1 kg of sample was pulverized to 95% passing –150 mesh and a 100 g subsample was split from the mass and shipped to Chemex in Vancouver for 30 g Fire Assay analysis for gold and Cu was analyzed by acid digestion/AAS methods.

Insufficient or poor quality QA/QC samples were inserted in the sample shipments for the Phase 1, 2, and 3 drilling campaigns. The pulps for 5% of the samples from these phases were sent to ALS-Chemex for analysis. The reassay data returned values for Cu and Au that are well within the accepted range to indicate that the original assays are of reasonable quality for resource estimation purposes. The 2004 drilling campaign was supported with an appropriate QAQC protocol. With the inclusion of the reassay program and Corriente's current QA/QC protocols, the sample results are of sufficient quality to support a resource estimate.

Duplicate sample performance was reviewed by AMEC and the results for Cu indicated that the sampling protocols are producing good quality assay results. The data for the Au duplicates is indicating a minor sampling problem. AMEC considers ±10% variation for 90% of the pulp duplicate analyses to demonstrate good precision. The gold values however are reporting that 90% of the sample population has a relative difference of 15% probably due to the small subsample size of 100 g and the small aliquot size of 30 g.

AMEC completed a data quality check on 5% of the sample database used for the resource estimation. All the data was found to be of excellent quality and adequate for resource estimation purposes.

A significant amount of metallurgical testwork has been undertaken on mineralized samples from the Mirador porphyry copper-gold porphyry deposit since 2002. SGS Lakefield Research (Lakefield), in Lakefield, Ontario carried out the main program of feasibility testing between December 2003 and September 2004. This included flowsheet development and mineralogical and recovery variability mapping programs on a total of about 3,000 kg of split diamond drill core from twenty drill holes and at various depths across the deposit. Overall this represents a reasonable spatial distribution of the expected metallurgy across the deposit.

The mill flow sheet selected for Mirador will be a conventional copper-gold porphyry flowsheet, with relatively coarse primary SAG and ball mill grinding to about 150 µm followed by copper rougher flotation, concentrate regrind to 25 µm, and cleaner flotation and dewatering. The process will be designed to treat 25,000 t/d. Concentrates produced are predicted to average 30% copper at a recovery of 91%. Gold recovery is expected to average 47%. A laboratory analysis of concentrates indicated that no significant deleterious penalty element impurities were present.

Geologic models were created of the dykes and the supergene units. AMEC checked the shapes for interpretational consistency on section and plan, and found them to have been properly constructed. To constrain grade interpolation in each of the zones,

AMEC created 3-dimensional mineralized envelopes based on copper and gold grades. These were derived by a method of Probability Assisted Constrained Kriging (PACK) to initially outline a general shape. The threshold grade for Au was 0.2 g/t and for Cu it was 0.5%.

The data analyses were conducted on original and 6 m composited assay data. AMEC reviewed the compositing process and found it to have been performed correctly. Detailed data analysis indicated the domaining and tagging of the assay and the composite data functioned well.

Extreme grades were examined for copper and gold composite values. Cu grades had a smooth distribution with few extreme grades. Gold showed extreme grade values and a grade cap of 0.60 g/t was imposed on the assay data prior to grade interpolation.

Variography was completed for gold and copper on composite data form the main mineralized unit within and outside the grade probability shells. Only hypogene material was investigated. The copper correlograms showed ENE-WSW trending, steeply dipping structures while the gold correlograms showed NS trending, subvertical structures.

The Mirador grade block model limits are (in UTM coordinates) 783500 to 786005 east, 9603000 to 9605505 north and 2000 to 200 m elevation. Block size is 15 m in the easting and northing directions and 12 m in height.

Values for copper, capped and uncapped gold, and bulk density were interpolated into the block model using ordinary kriging (OK), inverse distance weighting to the eighth power (ID8) and the nearest-neighbour (NN) methods.

AMEC completed a review of the Mirador resource block model. The model was checked for proper coding of drill hole intervals and block model cells. Gold and copper grade interpolation was examined relative to drill hole composite values by inspecting the sections and plans. The checks showed good agreement between drill hole composite values and model cell values.

AMEC checked the block model estimates for global bias by comparing the average copper and gold grades from the model ID8 with means from OK and NN estimates. The results show no evidence of bias in the estimate.

AMEC checked for local trends in the grade estimates by plotting the results from the OK, ID, and NN estimate results on easting, northing and elevation swath plots. The

results for copper and gold grade inside the grade probability shells show close tracking between the three estimates and no local trends.

The final check performed, was to check the model for smoothing through the Discrete Gaussian or Hermitian polynomial change-of-support method described by Journel and Huijbregts (Mining Geostatistics, Academic Press, 1978). The grade-tonnage predictions produced for the model show that grade and tonnage estimates are validated by the change-of-support calculations over the likely range of mining grade cutoff values (0.4% to 0.6% Cu).

The mineral resources of the Mirador project were classified using logic consistent with the CIM definitions referred to in National Instrument 43-101. The project mineral resources were classified as either Indicated or Inferred Mineral Resources. Table 1-1 contains the results of the resource estimation for the Mirador Deposit as of 23 September 2004. The resource estimate result for Mirador is being declared using the 0.40 %Cu cutoff. The resources are reported to a depth of 850 m elevation, which is approximately 500 m below the surface. Preliminary open pit planning work, conducted as part of an ongoing Feasibility Study, have shown potential open pit bottoms to be around 1000 m elevation, 150 m above the deepest interpolated grade blocks.

Table 1-1: Mirador Deposit Mineral Resource Summary – 23 September 2004

Zone		Tonnes	Au (g/t)	Cu (%)
0.4 Cu % Cutoff				
Indicated Mineral Resource				
	Mixed	1,300,000	0.23	0.57
	Enriched	6,700,000	0.24	0.99
	MNZD	301,700,000	0.20	0.65
Totals	Indicated Hypogene	301,700,000	0.20	0.65
	Indicated Supergene	8,000,000	0.24	0.92
Inferred Mineral Resource				
	Mixed			
	Enriched	1,200,000	0.25	0.83
	MNZD	313,900,000	0.17	0.56
Totals	Inferred Hypogene	313,900,000	0.17	0.56
	Inferred Supergene	1,200,000	0.25	0.83

2.0 INTRODUCTION AND TERMS OF REFERENCE

Corriente Resources Inc. (Corriente) engaged AMEC Americas Limited (AMEC) to provide a mineral resource estimate and Qualified Person's review and Technical Report for their Mirador Project in southeastern Ecuador. The work entailed estimating mineral resources in conformance with the CIM Mineral Resource and Mineral Reserve definitions referred to in National Instrument (NI) 43-101, Standards of Disclosure for Mineral Projects. It also involved the preparation of a Technical Report as defined in NI 43-101 and in compliance with the format set out in 43-101F1. Susan Lomas, P.Geo., an employee of AMEC, served as the Qualified Person responsible for preparing the resource estimation and this Technical Report. The author completed a site visit to the Mirador Project between the 19th and 24th of January, 2004.

This work represents a significant change in the level of confidence of the mineral resource since the last disclosure on this deposit in a Technical Report on the Mirador Project, dated February 2003. In that report a resource estimate was completed on the Mirador Project using section polygonal method and determined an Inferred Mineral Resource of 182 Mt at 0.76% Cu reported at a 0.65 %Cu cutoff. Those resources were prepared under the supervision of David K Makepeace, P.Eng., and James Dawson, P.Eng., Qualified Persons.

2.1 Terms of Reference

The Mirador Project is a copper-gold porphyry deposit. All drill hole data used for the resource estimation were obtained from Corriente personnel both at site and from the Vancouver office.

All units in this report are metric.

3.0 DISCLAIMER

No disclaimer statement was necessary for the preparation of this report.

4.0 PROPERTY DESCRIPTION AND LOCATION

The Mirador Project is located along the valley of the Rio Zamora (Zamora River) in the Morona Santiago Province of southeast Ecuador, adjacent to the border with Perú (Figure 4-1). The concessions are approximately 340 km south of Ecuador's capital city of Quito and 70 km east-southeast of the city of Cuenca.

The Mirador Concession Group centre is found at 9 604 200 N, 785 000 E; UTM Zone 17S coordinates and is located in an area of steep topography at 1,350 m elevation. The group of six concessions are contiguous and encompass 13,640 ha. The claims are registered with the National Directorate of Mining and have not been legally surveyed.

There are currently no existing mine workings or tailings within the Mirador Project site

Figure 4-1: Location Map



4.1 Mineral Tenure

The location of the individual concessions that are collectively known as the Mirador Project are tabulated in Table 4-1, and shown in Figures 4-2 and 4-3.

Table 4-1: Mirador Concession Locations and Areas

Concession	Code number	Hectares	Owner
Mirador 1	500807	2,400	Ecuacorriente S.A.
Mirador 2	500805	1,200	Ecuacorriente S.A.
Curigem 18	4768	1,600	Minera Curigem S.A
Curigem 18 este	500806	800	Minera Curigem S.A
Curigem 19	4769	2,900	Minera Curigem S.A
Caya 36	500200	4,740	Minera Panantza B.V

The Mirador deposit and proposed infrastructure are located in the Zamora Province within concession Mirador 1 and surrounding concessions comprising Mirador 2, Curigem 18, Curigem 18 Este, Curigem 19, and Caya 36, with state code number, hectares and ownership as indicated in Table 4-1.

All companies, Ecuacorriente S.A., Curigem S.A and Minera Panantza B.V. are fully owned by Corriente Resources.

A number of important new regulations were added or changed in the Ecuadorian Mining Code in late 2000. This includes changing the title of concessions to a single title, which is good for 30 years. In addition, concessions can now be grouped and divided, and the federal royalty on mining has been removed.

Corriente has located the land maps containing the surface rights in the Mirador area. The surface rights have been purchased or under legalizing or buying process for all land affected by proposed mining, construction sites, dumps and other infrastructure needed for the Mirador Project. Figure 4-4 illustrates the current status of surface rights acquisition by Corriente Resources. The different colours show the current status of the surface rights where grey represents independently owned surface rights and the pink areas have been purchased. The magenta and yellow areas are in the process of being acquired by Corriente.

Figure 4-2: Concession Location Map

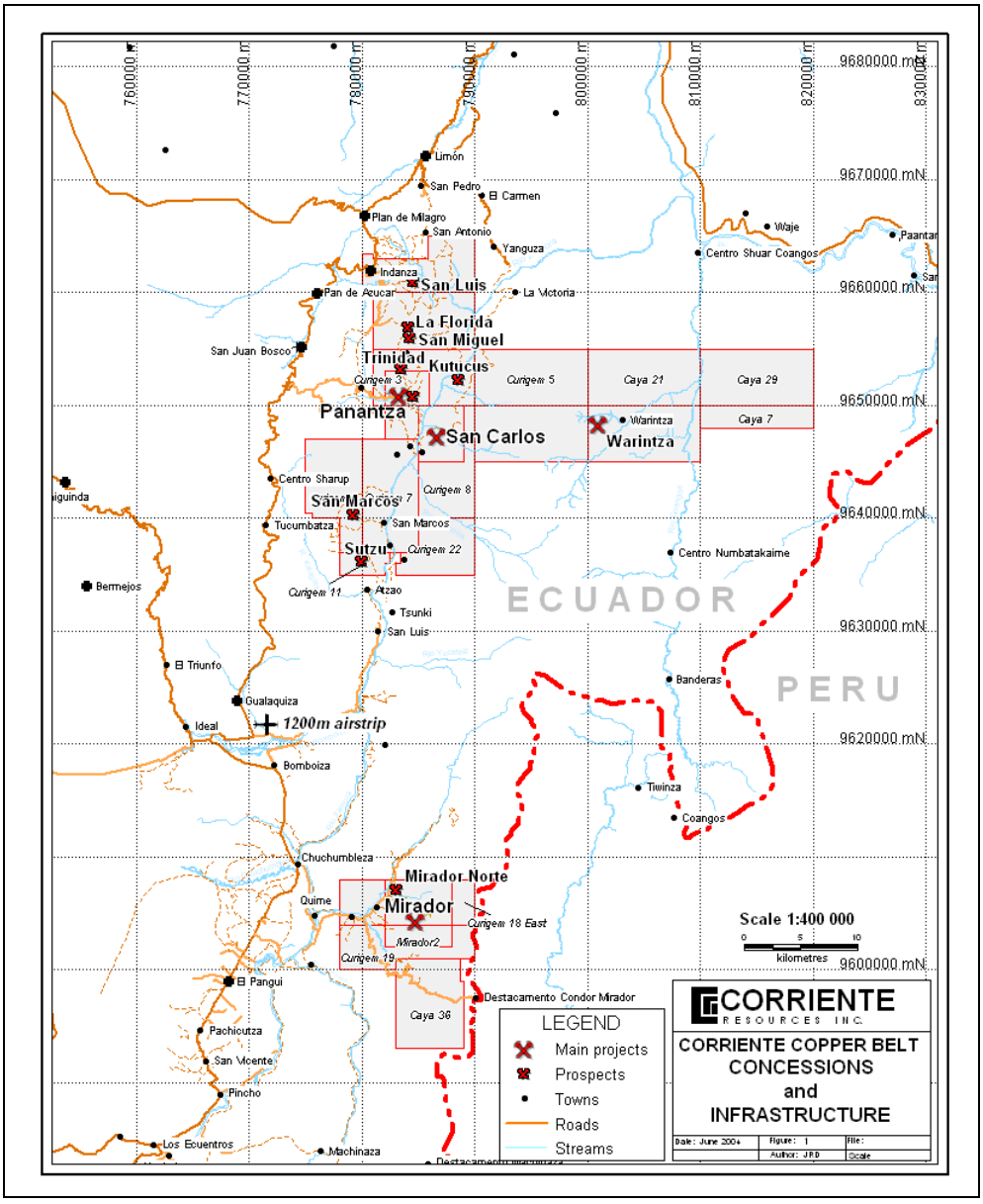


Figure 4-3: Detailed Map of the Mirador Concessions

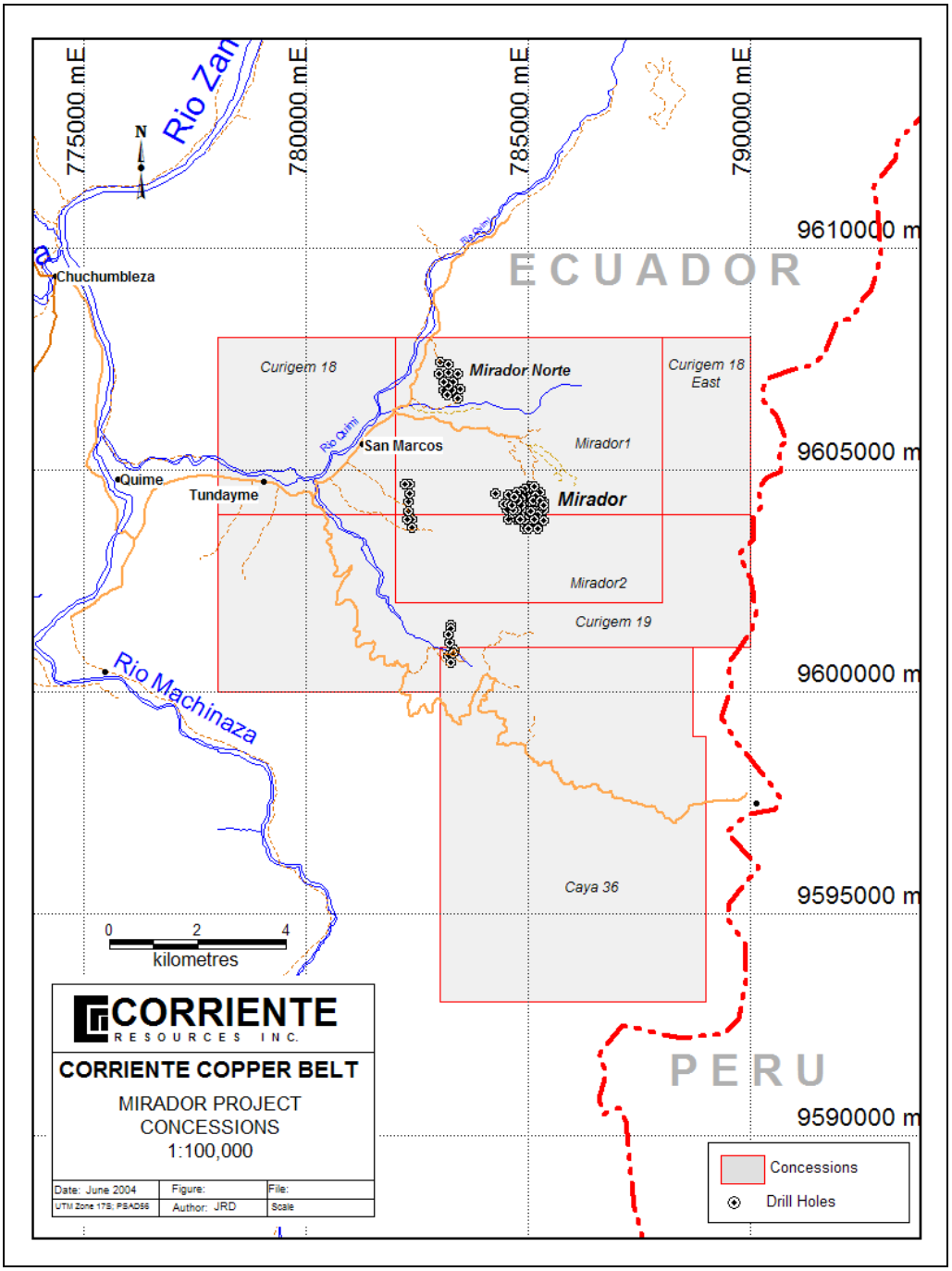
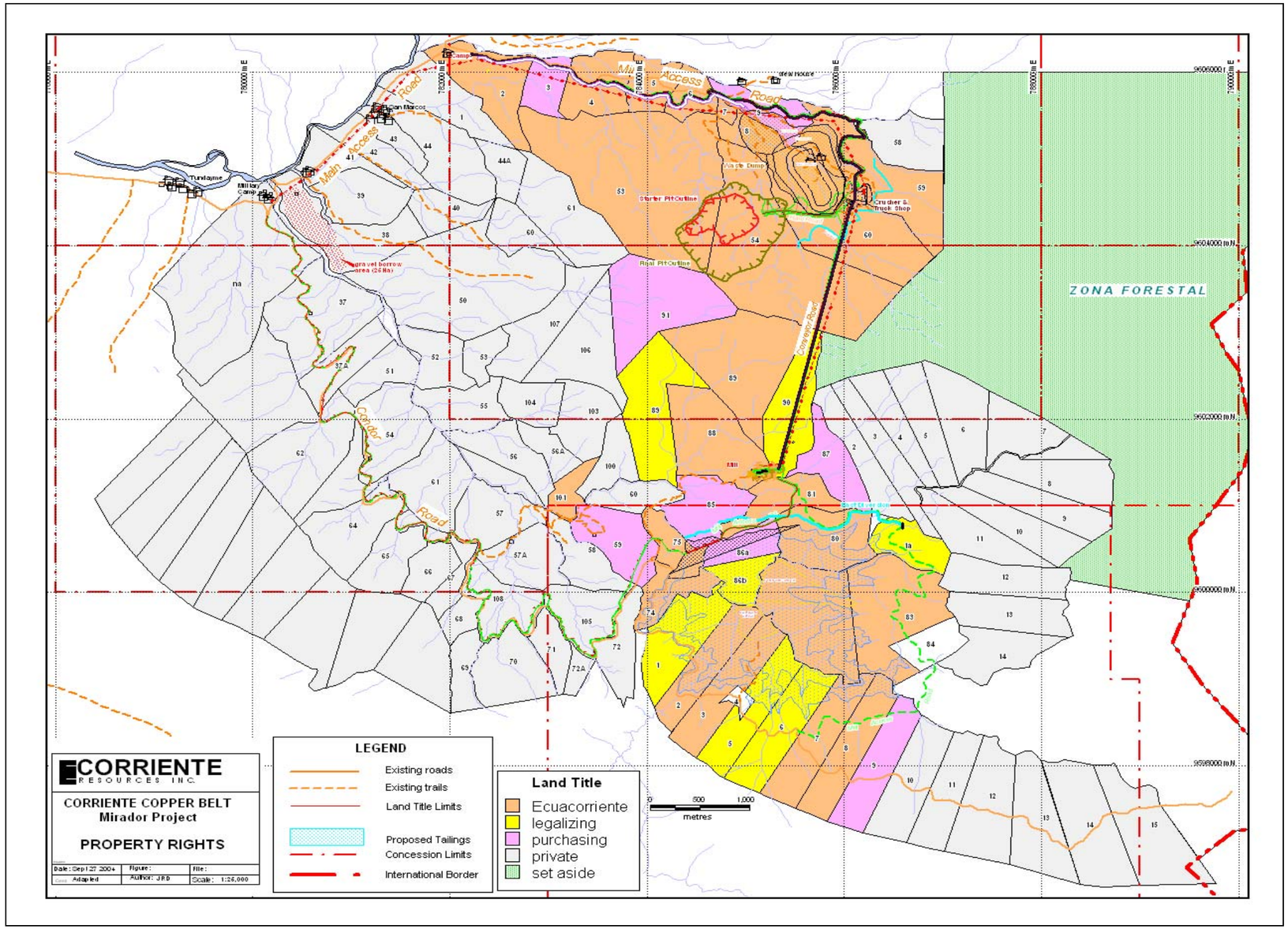


Figure 4-4: Surface Rights Ownership Map



4.2 Permits and Agreements

For the exploration phase, all the required permits are included in the approved Environmental Impact Assessment (EIA) that is currently filed with and accepted by the Ecuadorian Government.

For any future mine development, there are two basic permits that are required:

- *Mining Title* – this is similar to the exploration permit but a declaration of hectares is required to convert to a Mining Title. This has been completed by Corriente
- *Environmental License* – this is given after Corriente submits the Environmental Impact Study (EIS) and the Environmental Management Plan (EMP). The EIS and EMP are currently in progress and will be filed with the Ecuadorian Government at the end of October 2004.

Additional permits to be obtained after the completion of the ongoing Feasibility Study are:

- Permit for discharges and emissions
- Permit to modify water courses
- Permit for transportation and use of explosives.

In June 2004, Lowell Mineral Exploration exercised it's option to acquire a 100% interest in the Warintza project in Ecuador in exchange for the 10% interest Lowell Mineral Exploration held in all the Corriente concessions in Ecuador, (including Mirador, Panantza, and San Carlos).

BHP Billiton has elected to convert their interest in the Mirador Project to a 15% Net Profits Royalty.

4.3 Environmental Impact Assessment

The environmental regulations for mining activities in Ecuador were issued in 1997. These regulate the presentation of the Environmental Impact Statement (EIS). It has already been issued and approved for the primary exploration programs. Modifications to the report are required as drilling and development proceeds.

Corriente's exploration activities in the Mirador area are currently permitted under several EIS that have been filed with the government.

AMEC is not aware of any environmental factors that could impact the development of this project. As part of Corriente's ongoing Feasibility Study, AMEC Earth and Environmental are conducting an environmental study.

5.0 ACCESSIBILITY, CLIMATE, AND PHYSIOGRAPHY

5.1 Accessibility

The nearest village to the Mirador Deposit is Tundayme and it is 6 km from the project site. Scheduled air service is available from Quito to Cuenca and Loja (Figure 4-1). Small, chartered aircraft currently fly to Gualaquiza, the closest airfield to the deposit.

The village of Tundayme is accessed by a system of gravel roads from Cuenca. The road distance is approximately 230 km; about five to six hours travel time.

There is road access from Quito to Cuenca for the transport of samples or heavy equipment. There is also road access to the Pacific Ocean port of Machala.

There is currently road access accessed over approximately two kilometres of narrow walking trail from the dirt road. Core is carried by workers to the road using backpacks and the drill is mobilized manually.

5.2 Climate

The area has a wet equatorial climate with a reported rainfall of 2,300 millimetres (mm) per annum. Individual rainfall events can be over 60 mm in a 24-hour period. Due to variations in local topography, there is a wide range in rainfall levels, and the area could be characterized as having numerous microclimates. Fieldwork is possible all year round. The optimum period for airborne surveys or road and trail construction is from October to December because of drier weather conditions at this time.

5.3 Physiography

The valley of the Rio Zamora bisects the project area at an elevation of about 700 m ASL. The flanking highland areas of the Paramos de Matanga on the west, and the Cordillera de Condor on the east, rise to maximum elevations of 4,200 and 3,500 masl, respectively. The elevation of the Mirador prospect ranges from about 800 to 1,400 masl. Drainage is into the Rio Zamora via Rio Wawayme.

5.4 Infrastructure

The infrastructure within the immediate area of the Mirador Project is shown in Figure 4-2.

There is currently a 13.8 kV power line that ends somewhere to the north of Gualaquiza. A closer 69 kV power line apparently approaches the site from the north. The stability of these power lines is unknown.

The closest existing airstrip is at Gualaquiza about 40 km to the northwest of the deposit. It has an asphalt runway approximately 2,140 m long.

6.0 HISTORY

Regional exploration was initiated in southeastern Ecuador by BHP Billiton S.A. in 1994. BHP Billiton used silt sampling to identify favourable areas of base metal anomalies. With further mapping they identified possible porphyry copper systems associated with these anomalies. At least eight separate porphyry copper systems have been identified in the region.

The area of Mirador was recognized as an area of interest during the original reconnaissance geological and geochemical surveys completed in December 1994. These surveys, which included 315 pan concentrates of stream sediments, defined an area roughly 50 km^2 that contained anomalous values for Cu, Mo, Au, Zn, and Ag. However, BHP Billiton was forced to focus its efforts in the north part of the belt since the present property was off limits between 1995 and 1999 due to the border conflict in the area between Ecuador and Perú.

After a peace treaty was signed with Perú in July 1999, BHP Billiton completed detailed follow-up surveys to better define the anomaly areas at the Mirador property. They collected 746 soil samples along ridges and 219 rock chips from outcrops found in drainages traversing the anomalous zones. This work along with geological and alteration mapping defined the Mirador (previously known as Wawayme) zone and the Chancho and Chancho Norte Zones to the southwest.

In October 1999, BHP Billiton entered into an option agreement with Corriente Resources Inc. covering 880 km^2 in the northern part of the porphyry belt. Subsequently, BHP Billiton and Corriente entered into a further agreement in April 2000 covering 230 km^2 in the southern part of the porphyry belt (the Mirador – Chancho property).

In 2002, after completion of 52 diamond drill holes, results of a polygonal resource estimate were released (12 February 2002). The estimated tonnage and grade, calculated at a 0.65% Cu grade, were 218 Mt grading 0.73% Cu, all in the Inferred Mineral Resource category.

In 2003, Corriente released a second mineral resource for the Mirador Project in a NI-43-101 Technical Report (February, 2003). The updated resource estimate was based on 10 additional holes and estimated using polygonal methods. This resource estimate, calculated at a 0.65 Cu % cutoff grade, yielded 182 Mt grading 0.76 % Cu and 0.221 g/t Au. The estimate was classified as Inferred Mineral Resources.

7.0 GEOLOGICAL SETTING

7.1 Regional Geology

The porphyry copper mineralization of the region is associated with Late Jurassic porphyry intrusive phases of the Jurassic batholiths of the Abitigua Subdivision in the Cordillera Real and sub-Andean regions of Ecuador. The Zamora Batholith, which hosts the known porphyry mineralization, is part of the Abitigua Subdivision.

No detailed regional structural mapping is available for this area.

7.2 Local and Property Geology

The Zamora batholith forms the wall rocks of the Mirador porphyry system. Within the mineralized zone, the intrusion comprises mainly granodiorite, with some leucogranite dikes along the west and southwest margins. An early, hornblende-feldspar porphyry intrudes the Zamora rocks as north-south discontinuous dikes.

The core of the deposit is characterized by a circular area of breccia composed of clasts of the host porphyry and granite, and early mineral quartz-stockwork fragments. This breccia obscures the contact relationships between the granite and porphyry units. The porphyry and the granite were impregnated with anhydrite stringers during the chalcopyrite-mineralizing phase. Meteoric fluids percolated down from the surface and hydrated the anhydrite. The hydration of anhydrite created gypsum and a corresponding 50% volume increase that shattered the rock (Figure 7-1 and 7-2). Gypsum is soluble and leaches from the rock leaving weakly cemented to open fractures. The poor rock quality migrated downward in the deposit area as a hydration front. Away from the hydration front, the porphyry and the granite are less fractured and the anhydrite fracture filling is unaltered.

A series of mostly northeast trending, steeply northwesterly dipping, hornblende-feldspar porphyry dykes cut the breccia and the country rocks. These dykes, ranging in age from syn- to post copper mineralization, are more numerous and thickest along the southeast and northwest margins of the mineralization. A quartz-bearing variety appears to be the youngest in the series.

Figure 7-1: Drill Core Photo of M64 from 140.78 to 146.14 m showing low RQD prior to Core Cutting



Figure 7-2: Drill Core with unaltered Anhydrite (Below the Gypsum Front)



Post-mineralization, hydrothermal breccia dikes, with a polymictic clast assemblage of mineralized and unmineralized rock, are associated with the porphyry dikes and are also most common along the southeast margin. The breccia also occurs as irregular plugs around the north and northeast margins of mineralization. Copper grades within the breccia range from very weak to slightly below average for the deposit, depending on the amount of mineralized rock incorporated.

Fifty-metre to eighty-metre high cliffs of Cretaceous Hollin Formation quartz sandstone occur to the south, above Mirador. These resistant rocks cover the southern extent of the Mirador alteration/mineralization complex.

8.0 DEPOSIT TYPES

The copper and gold mineralization encountered at the Mirador Deposit display many of the characteristics of calc-alkaline type porphyry copper system. Supergene zones of enrichment are weakly developed beneath a superficial leach cap that averages less than 22 m thick.

9.0 MINERALIZATION

Mineralization at Mirador can be divided into early molybdenum, early copper ± gold, and late copper-gold stages. Molybdenum is associated with early quartz veining. Both copper-gold events are sulphide dominated. Chalcopyrite occurs as mainly irregular masses between clasts in the early breccia (with some disseminated) and as fine disseminations in a halo zone around the breccia within the Zamora granite. The syn- to post-mineral porphyry dykes are variably and weakly mineralized by the late copper-gold disseminations and sparse sulphide veins.

A late stage series of 1 cm to 2 cm quartz sulphide stingers transect the project. They are subvertically emplaced but their strike is unknown, as they have only been seen in drill core. These veinlets are sulphide rich and have elevated gold and zinc values. They were intersected in the vertical drill holes and were found running down the core over metres of core length.

The Mirador porphyry system exhibits well-defined alteration zoning, with a large (approximately 4 km^2), quartz-sericite alteration zone covering a large part of the wall rock and quartz diorite porphyry. This alteration has overprinted a potassic alteration whose remnants are small secondary biotite nuclei mainly in the quartz monzonite.

10.0 EXPLORATION

Since April 2000, Corriente has carried out exploration on the Mirador Project. The work completed has included geological mapping, pan concentrate sampling of drainages, geochemical soil sampling, rock chip sampling and the completion of 24,349 m of core drilling in 91 diamond drill holes. (The pan concentrate work was carried out by BHP Billiton previously to Corriente's participation, but Corriente conducted all subsequent sampling and project work.)

10.1 2000

In May the first phase drilling on Mirador began and 30 holes were completed resulting in 5,383 m of drill core under the supervision of J. David Lowell, who was under contract by Corriente. Corriente assumed total management of the project in October 2002.

10.2 2001

Between January and May of 2001, the second phase of drilling was completed at Mirador and 22 holes were drilled for 8,136 m of core.

10.3 2002

Between February and April of 2002, the third phase of drilling was completed where 10 holes were drilled for 2,739 m.

10.4 2003

In February a Preliminary Assessment Report of the Mirador Deposit was completed and was filed as a Technical Report entitled "Mirador Project, Corriente Copper Belt, Southeast Ecuador, Order of Magnitude Study, Part 1, Technical Report", under the supervision of Qualified Person David K. Makepeace, P.Eng. and James M. Dawson, P.Eng.. A polygonal resource estimation was completed for this study based on 62 drill holes completed on the Mirador Project.

In July, Sumitomo of Japan completed independent metallurgy tests showing favourable concentrate potential. AMEC reviewed this work and found it to be done to industry standard and subsequent follow-up work has confirmed their conclusions. Metallurgy is discussed in detail in Section 16 of this report.

In December the fourth phase of drilling at Mirador began.

10.5 2004

In April the fourth phase drilling was completed and 29 drill holes were drilled for 8,091 m of core.

11.0 DRILLING

The Mirador deposit has been intersected by 91 diamond drill holes totalling 24,350 m, arranged in a rough grid on approximately 75 m to 100 m centres. The drill hole information has been tabulated in Table 11-1 and the collar locations are illustrated in Figure 11-1.

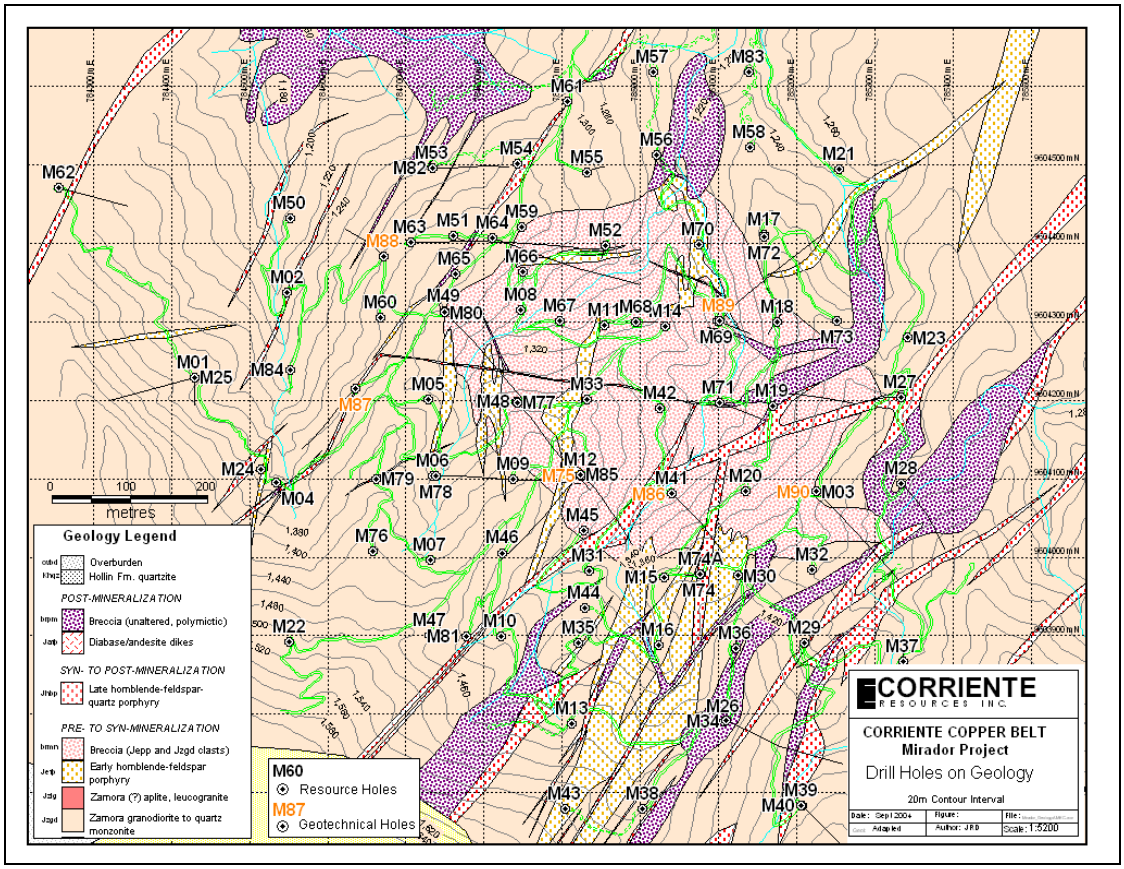
Table 11-1: Summary Table of Drill Holes

HoleID	X	Y	Z	Depth	Downhole Survey	Dip	Azimuth	Phase
M01	784429.06	9604229.02	1335.91	104.56	N	-70	180	1
M02	784548.07	9604336.79	1230.56	198.16	N	-90	360	1
M03	785225.46	9604083.82	1389.82	368.81	N	-90	360	2
M04	784533.41	9604095.86	1345.16	92.35	N	-90	360	1
M05	784728.65	9604200.73	1363.85	226.42	N	-90	360	1
M06	784734.12	9604104.12	1369.27	199.64	N	-90	360	1
M07	784731.22	9603996.78	1418.72	104.39	N	-90	360	1
M08	784846.97	9604315.52	1296.32	158.19	N	-90	360	1
M09	784837.34	9604099.41	1408.63	150.27	N	-90	360	1
M10	784821.49	9603899.27	1408.04	163.98	N	-90	360	1
M11	784954.04	9604295.75	1312.64	150.88	N	-90	360	1
M12	784923.83	9604105.48	1391.69	211.23	N	-90	360	1
M13	784912.06	9603788.57	1459.88	153.01	N	-90	360	1
M14	785031.76	9604294.29	1327.44	150.88	N	-90	360	1
M15	785030.21	9603974.82	1385.97	176.17	N	-90	360	1
M16	785022.78	9603887.73	1385.58	213.97	N	-90	360	1
M17	785158.22	9604410.25	1304.30	131.06	N	-90	360	1
M18	785175.45	9604299.31	1298.23	86.26	N	-90	360	1
M19	785168.60	9604192.59	1318.96	106.06	N	-90	360	1
M20	785134.51	9604084.62	1356.43	244.75	N	-90	360	1
M21	785254.51	9604493.84	1243.87	54.86	N	-90	360	1
M22	784551.19	9603892.78	1507.67	128.02	N	-90	360	2
M23	785342.00	9604280.11	1339.23	400.81	N	-90	360	1
M24	784514.99	9604112.03	1345.40	69.65	N	-60	260	1
M25	784429.06	9604229.02	1335.91	223.42	N	-60	255	1
M26	785106.59	9603790.80	1464.02	99.20	N	-90	360	1
M27	785332.78	9604204.01	1370.16	438.91	Y	-70	270	2
M28	785333.85	9604093.70	1325.75	258.47	Y	-70	135	2
M29	785209.72	9603890.66	1385.05	457.20	Y	-90	360	2
M30	785124.34	9603976.42	1419.83	175.26	N	-90	360	1
M31	784934.00	9603982.00	1360.65	279.50	N	-90	360	1
M32	785219.85	9603983.51	1361.20	295.35	N	-90	360	1
M33	784932.02	9604200.78	1378.04	285.60	N	-90	360	1
M34	785109.58	9603791.65	1464.04	429.77	Y	-70	90	2
M35	784920.79	9603890.85	1414.43	301.75	N	-90	360	1
M36	785121.42	9603884.58	1451.54	175.26	N	-90	360	1

HoleID	X	Y	Z	Depth	Downhole Survey	Dip	Azimuth	Phase
M37	785335.76	9603867.16	1354.07	400.00	Y	-90	360	2
M38	785002.46	9603680.09	1498.12	486.16	Y	-90	360	2
M39	785329.16	9603682.64	1395.37	272.49	N	-70	135	2
M40	785325.20	9603684.65	1394.52	298.70	N	-90	360	2
M41	785040.51	9604081.10	1311.76	249.94	N	-90	360	2
M42	785025.27	9604190.25	1330.42	294.13	N	-90	360	2
M43	784903.62	9603679.88	1539.60	399.29	N	-90	360	2
M44	784928.05	9603935.74	1391.86	419.10	Y	-90	360	2
M45	784927.04	9604034.14	1368.02	303.28	N	-90	360	2
M46	784822.81	9604005.57	1424.18	408.13	N	-90	360	2
M47	784730.04	9603900.14	1464.08	349.00	N	-90	360	2
M48	784840.47	9604198.33	1372.03	448.06	N	-90	360	2
M49	784748.93	9604313.58	1358.08	492.25	Y	-90	360	2
M50	784551.33	9604431.37	1208.15	341.06	N	-90	360	2
M51	784760.68	9604409.17	1357.24	449.58	Y	-90	360	2
M52	784955.70	9604396.72	1294.20	443.48	Y	-90	360	2
M53	784733.46	9604496.33	1291.29	198.42	N	-90	360	3
M54	784842.37	9604500.75	1335.86	188.67	N	-90	360	3
M55	784932.04	9604490.70	1316.40	363.02	Y	-90	360	3
M56	785020.91	9604512.41	1243.26	399.90	Y	-90	360	3
M57	785015.86	9604618.65	1239.11	250.85	Y	-90	360	3
M58	785139.87	9604521.79	1267.86	180.75	Y	-90	360	3
M59	784848.69	9604420.90	1352.61	391.67	Y	-90	360	3
M60	784667.52	9604304.61	1341.69	410.26	Y	-90	360	3
M61	784907.07	9604580.28	1307.20	171.91	Y	-90	360	3
M62	784256.02	9604470.38	1309.96	183.30	N	-60	105	3
M63	784706.16	9604401.16	1345.00	400.51	Y	-60	90	4
M64	784810.73	9604406.45	1352.00	400.81	Y	-60	110	4
M65	784763.08	9604360.13	1363.00	300.23	Y	-90	0	4
M66	784849.12	9604364.10	1322.00	300.23	Y	-90	0	4
M67	784896.78	9604300.56	1295.00	300.23	N	-90	0	4
M68	784994.73	9604299.24	1315.00	315.47	N	-85	90	4
M69	785098.00	9604300.56	1270.00	269.75	N	-80	110	4
M70	785074.16	9604398.51	1240.00	249.94	N	-90	0	4
M71	785100.63	9604197.31	1278.00	300.23	Y	-80	110	4
M72	785158.22	9604408.00	1305.00	286.51	Y	-90	0	4
M73	785251.53	9604300.56	1338.00	188.98	Y	-90	0	4
M74A	785077.89	9603978.05	1400.00	73.15	N	-90	0	4
M74	785076.00	9603978.05	1400.00	288.04	Y	-85	270	4
M75	784925.00	9604104.00	1391.69	300.25	Y	-60	135	4
M76	784657.38	9604007.78	1445.00	254.51	Y	-90	0	4
M77	784842.00	9604197.00	1372.03	300.25	Y	-60	135	4
M78	784738.37	9604103.27	1370.00	300.25	Y	-55	90	4
M79	784661.60	9604099.98	1410.00	269.75	Y	-90	0	4
M80	784750.00	9604312.00	1358.08	300.23	Y	-60	135	4

HoleID	X	Y	Z	Depth	Downhole Survey	Dip	Azimuth	Phase
M81	784776.95	9603899.64	1430.00	256.03	Y	-90	0	4
M82	784734.50	9604496.35	1280.00	225.55	Y	-65	90	4
M83	785138.24	9604618.10	1225.00	150.88	Y	-90	0	4
M84	784552.00	9604239.00	1260.00	249.94	Y	-90	0	4
M85	784923.83	9604105.48	1392.00	300.23	Y	-60	225	4
M86	785040.51	9604081.10	1312.00	202.69	Y	-60	135	4
M87	784635.92	9604215.19	1342.00	300.23	Y	-70	225	4
M88	784671.06	9604383.53	1310.00	349.91	Y	-80	315	4
M89	785100.63	9604300.56	1270.00	358.14	Y	-60	45	4
M90	785225.46	9604083.82	1390.00	298.70	Y	-60	135	4

Figure 11-1: Mirador Drill Hole Location Plan



Kluane International Drilling Inc. of Canada was contracted to complete the diamond drilling programs. They used a man-portable wire-line drill and all platforms were

accessed via hand-cut mule trails. There is no road access to the drill pads; access is by a walking trail over the final 1,500 m from the road.

Drill core was recovered in standard core tubes at sizes of NTVV (5.2 cm diameter) and TVV (4.8 cm diameter). The smaller size core was recovered in the lower parts of the deeper drill holes. Standard HQ size core was taken from a few of the geotechnical holes.

Most drill holes at Mirador were drilled vertically. AMEC believes more angled drill holes should have been drilled due to the presence of various geologic features having sub-vertical contacts (e.g., post-mineral dykes, late quartz-sulphide stringers). The copper grades do not appear to be influenced by the angle of the holes. However, because the quartz-sulphide stringers contain elevated gold values, samples hosting them were treated conservatively during gold grade interpolation (see section 17).

Core is stored in wooden boxes each holding five metres of core. When picked up at the drill, all the core box lids are secured and the boxes are packed out on foot by workers to the road and loaded onto trucks, and delivered to the Mirador Camp. Corriente staff then open the boxes and the footage markers are converted into metres. The core is then placed on a stand and photographed.

The core is marked in one-metre intervals by a geothechnician, who then measures the core recoveries and RQD. Technicians complete a preliminary drill log where they capture the core recovery, structural features, fracture density and orientation, and rock quality data (RQD).

The drill hole collars were surveyed using differential GPS equipment to a reported instrument accuracy of ±1 m (X-Y) and ±2 m (Z) Segundo Toledo Peláez of Topcon Survey S.A. of Ecuador. Some of these surveys were only done on the excavated pads before drilling. The accuracy here will be somewhat less than the accuracy of the equipment, in of the order of ±3 m.

Table 11-1 includes a column to indicate which drill holes were down hole surveyed. The surveys were completed using a Tropari instrument for the 20 holes in the second and third phases of drilling. A Sperry-sun instrument was used during the fourth phase of drilling in 2004. Of the 91 drill holes completed, 50 have no down hole survey data. Five of the unsurveyed drill holes were drilled at an angle between 60° and 70°; M01, M25, M25, M39, and M62. These holes were drilled on the periphery of the deposit and have no impact on the resource estimation. Drilling deviation on vertical holes can be very small but it is best practice to complete down hole surveys on all drill holes.

When a drill hole is completed, the collar location is marked with a large PVC pipe capped with a plastic cover (Figure 11-2).

Figure 11-2: Drill Hole Collar Marker



Core recovery is good and is >90% in the zones of primary mineralization. The RQD values measured from the core indicate that rock quality is very low through large parts of the deposit. The average RQD value from the drilling over the whole of the deposit is 38%. The poor RQD at Mirador is the result of the shattering process due to the hydration of anhydrite mineralization.

Bulk Density was determined on pieces of core that ranged in size from 10 g to 30 g each. The samples were collected at 40 m intervals. For phases 1 to 3 the bulk density was determined by weighing the sample dry, then immersing the sample in water and measuring the weight of the water displaced. This was not a very efficient method as it was slow and water could soak into the samples. The procedure was changed for Phase 4 where the samples were suspended with thin nylon monofilament and weighed dry, then immersed in water and weighed wet. There are 665 values in the database for the hypogene samples, 21 for the Leached, 22 for the Mixed and 46 for the Enriched samples for a total of 754 samples tested.

12.0 SAMPLING METHOD AND APPROACH

The entire length of all the drill holes was sampled and assayed. When Corriente receives the core at the camp, the core technicians mark up the core into one metre samples and assign each of these intervals a sample number. The samples are combined into composite samples according to the rock type. The Leached rock type was sampled in 5 m lengths. Within the zone of supergene-copper enrichment the sample length was two meters. The Mixed lithology was identified at the end of the 4th phase of drilling therefore these samples can be either 5 or 2 m in length. There was poor identification of these units during the primary logging so the samples typically cross boundaries between these three rock types (Leached, Mixed and Enriched). Sample lengths through the zone of primary mineralization are 3 m. The sample interval was frequently extended to five metres within barren post-mineral dikes.

Table 12-1 contains a list of the proposed and the resulting sample lengths by rock type. The Enriched samples were often found to be longer than the proposed upper limit of 2 m where 57 samples or 22% of the samples are over 3 m.

The sampling program was planned and executed in a satisfactory manner and the resulting assays are acceptable for resource estimation purposes.

Table 12-1: Sample Lengths by Lithology Unit Mineral Zone

Lithology Name	Lithology Code	Sample Length (m)	Number of Samples	Mean Length	Min Length	Max Length
Leached	90	5	440	4.80	2	14
Mixed	93	5 or 2	169	2.77	2	10
Enriched	95	2	261	2.25	1	7
Mineralized	100 to 150	3	5743	2.98	0.75	6
Post Mineral Dykes	10 and 50	5	966	3.79	1.6	13

The geologist marks up a sample sheet where the samples are composited by rock type and receive a sample number. The samples are split and placed in plastic sample bags. The core is split using a Boart rock saw (Figure 12-1). When the core is strongly broken, fragments from one half of the core are picked out of the box. The sampler is instructed to collect the pieces randomly. No line is marked on the core. The sample bags are doubled and the sample numbers are well secured to the bags. The sample bags are then weighed and the weight is recorded on the sample sheet.

The current sample number system uses a 10-digit number, e.g., 2722190680. The number breaks down into the following components:

2_72_219_068_0

- 2 The Project Number (Mirador is 2)
- 72 The drill hole number for M72
- 219 The "to" interval the sample interval. If the sample is an SRM then this number is used to indicate which SRM was inserted into the sample stream. The code used and the corresponding SRM samples are listed in the following table:

Code	SRM
500	GEM1
600	GEM2
700	GEM3
800	MS1
900	MS2

- 068 The sample number for the drill hole
- 0 This number is used as a QA/QC marker
  - 0 = core sample
  - 7 = ½" Crush Duplicate
  - 8 = Coarse Reject Duplicate
  - 9 = Pulp duplicate

AMEC recommends that Corriente change their sample numbering protocols and use assay laboratory sample tag books. Sample numbers should never identify the hole number, the sample interval or puts emphasis on QA/QC samples by giving them unique identifiers. Going to standardized sample books will minimize risk of recording errors and be consistent with industry best practices.

The sample bags are put into rice bags for shipping. Each bag is marked with the project number, the drill hole number and then another number for the shipping bag. AMEC advised Corriente that this was not an accepted practice and the bags should only be marked with the bag number, not the drill hole number. The rice bags are secured with tape and rope. The samples are sent to Quito by a contracted driver and are not zip secured or in a locked box.

When the truck arrives in Quito, it goes to Corriente's office and picks up the Office Manager and immediately proceeds to the Chemex prep lab. The office manager prepares the duplicate and SRM list for insertion of the QA/QC samples. The Chemex prep lab receives a sample shipment form that lists which samples to duplicate and the placement of the SRM samples.

Figure 12-1: Core Saw Facility



The remaining half of the sampled core was then logged in detail by Corriente geologists.

13.0 SAMPLE PREPARATION, ANALYSES, AND SECURITY

Sample pulps were prepared at Chemex Laboratories in Quito by laboratory personnel. Earlier samples were processed and analysed by Bondar Clegg prior to the merging of the two companies. The preparation procedure for the samples and duplicates and standard insertion changed over the four different phases of drill programs.

For all drill phases the following procedures remained consistent. The whole sample was crushed to 75% passing –10 mesh, then 1 kg of sample was pulverized to 95% passing –150 mesh and a 100 g subsample was split from the mass and shipped to Chemex in Vancouver for 30 g Fire Assay analysis for gold and Cu was analyzed by acid digestion/AAS methods.

No QA/QC samples were inserted in the sample shipments for the Phase 1 drilling campaigns. Five percent of the samples from these drill programs were reanalysed with the benefit of SRM samples.

For Phase 2 drilling, the only QA/QC sample inserted into the sample shipments was a 100 g Lab Check Duplicate. This sample was taken on a 1 in 10 basis and was shipped to Chemex in Vancouver for analysis. The check lab was changed to Acme Labs in Vancouver after ALS Chemex purchased Bondar Clegg. No SRM samples were included in the shipment of any samples for these drill programs. The Lab Check Duplicate sample results were insufficient to certify the analysis results so a reassay program was set up by AMEC. Five percent of the samples from these drill programs were reanalysed with the benefit of SRM samples.

For the phase 1 and 2 drilling programs the samples were analysed for gold using fire assay analysis and for copper, silver, lead, molybdenum and zinc using four acid digestion/AAS methods.

The sampling procedures were modified in February of 2001 to introduce some QA/QC samples into the sample shipments. The new protocol included inserting one pulp duplicate and one of three standards, GEM1, GEM2 and GEM3 into each batch of 20 samples sent to the labs. These standards were insufficiently homogenous to be used for a QA/QC program. This situation does not impact the quality of the grade values since 5% of the samples were reanalysed with the benefit of SRMs.

In late 2002, for the third phase of drilling, Corriente changed the insertion rate of the pulp duplicates and SRM samples to 1 in 40 samples. MS1 was the SRM sample being included in the lab shipments for this drilling campaign. The check samples

were now being shipped to Acme labs in Vancouver but no SRM samples were being included in the shipments of the Lab Check Duplicate.

Samples for the third drilling phase on the project were analysed for gold using fire assay analysis and for copper, molybdenum and zinc using four acid digestion/AAS methods.

In late 2003, the sampling protocols were modified to include more QA/QC samples. During the 4th phase drilling program, the insertion rate of all QA/QC samples was increased back to a 1 in 20 insertion rate. The two SRMs included in the sample shipments were MS1 and MS2. A coarse reject duplicate was also included in the sample shipments. (A coarse split at -2 mesh was done only for samples destined for metallurgy test work and were only applied to drill holes M65 to M70.)

Samples for the fourth drilling phase on the project were analysed for gold using fire assay analysis and for copper and molybdenum using four acid digestion/AAS methods.

No blank samples were inserted into any of the sample shipments. Blank samples are used to certify sample preparation procedures by guarding against inter-sample contamination. They also are useful to identify sample mix-ups. It is recommended that Corriente include blank sample insertion in any future sampling programs.

With the inclusion of the reassay program and Corriente's current QA/QC protocols, the sample results are of sufficient quality to support a resource estimate.

13.1 ICP Sample Analysis

Three of the angled holes through the deposit, M75, M77and M80, were selected to check for any significant levels of potentially deleterious elements. 281 samples were analyzed for the following elements by ICP analysis; Au, Ag, Al, As, Ba, Be, Bi, Ca, Cd, Co, Cr, Cu, Fe, K, Mg, Mn, Mo, Na, Ni, P, Pb, S, Sb, Sr, Ti, V, W, Zn and Hg. No elements reported ranges that would cause potential problems for the concentrate quality. This topic is discussed further in Section 16 of this report. Results from these analyses are presented in a table in Appendix A.

13.2 Reassay of Phase 1 and 2 Drilling Samples

The drill core samples from Drill Phases 1, 2, and 3 were initially assayed without the benefit of adequate SRM samples. Phase 1 samples were sent to the assay lab with

no SRM samples and Phase 2 and 3 samples were sent with an SRM that was insufficiently homogeneous. The pulps for 5% of the samples from these phases, 523 samples, were sent to ALS-Chemex under a blind sample-numbering scheme. Standards (MS1 and MS2) and pulp duplicates were inserted into batches of 20 samples.

The reassay data returned values for Cu and Au that are well within the accepted range to indicate that the original assays are of reasonable quality for resource estimation purposes. AMEC considers ±10% variation for 90% of the pulp duplicate analyses to demonstrate good precision. For the Cu grades, 90% of the population has an absolute relative difference of 11% whereas for the gold grades it was 18% (Figure 13-1 to 13-4). All SRMs submitted with these sample shipments returned values within the SRM accepted ranges. The Au grade differences are a little on the high side, probably due to the small subsample size of 100 g and the small aliquot size of 30 g.

Figure 13-1: QA/QC Reassay of Historical Data, Cu (ppm)

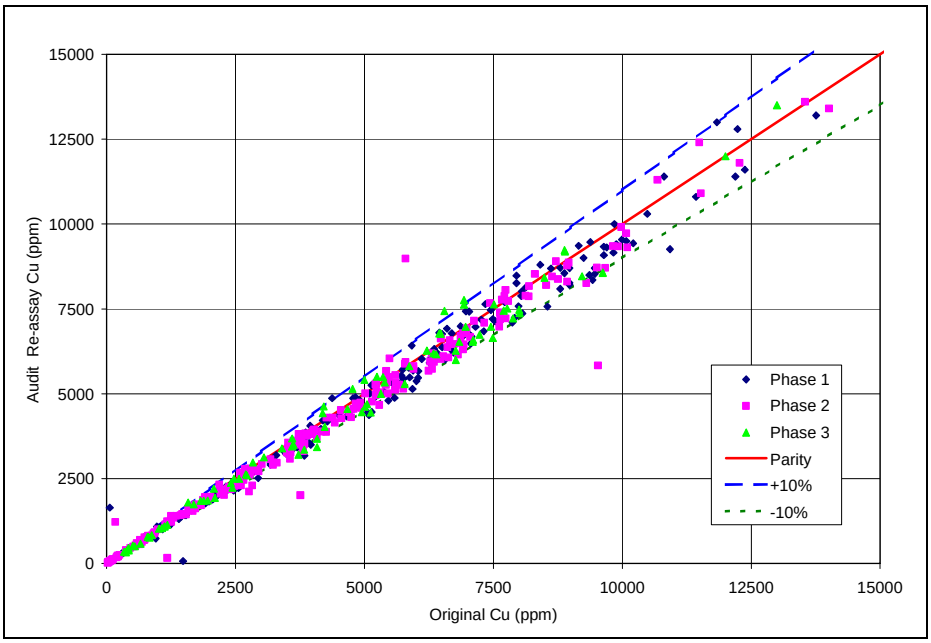


Figure 13-2: Reassay of Historical Data, Au (g/t)

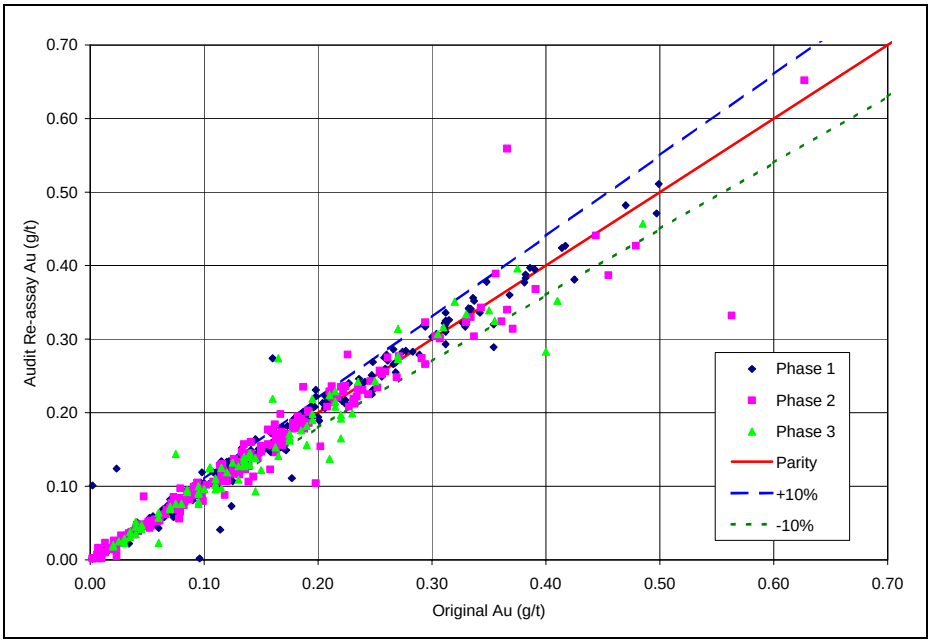


Figure 13-3: Percentile Rank Chart, Reassay Results, Cu (ppm), 501 Samples

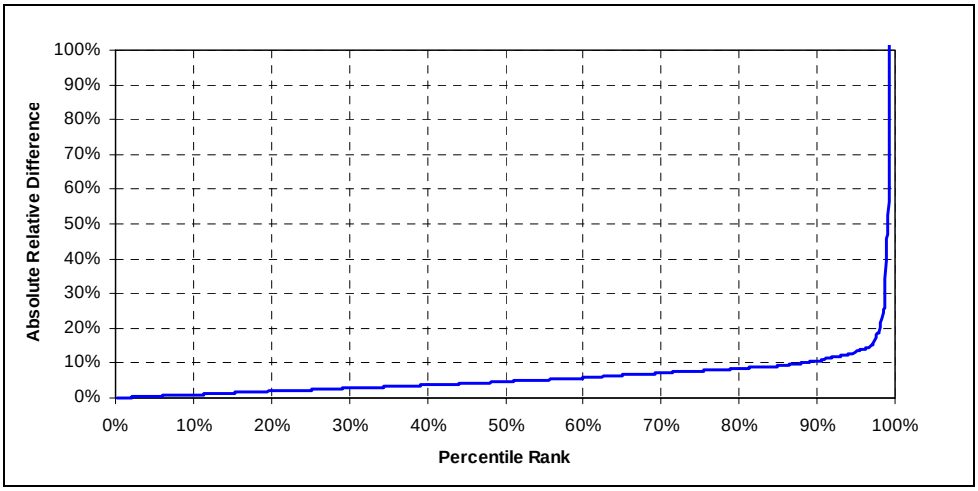
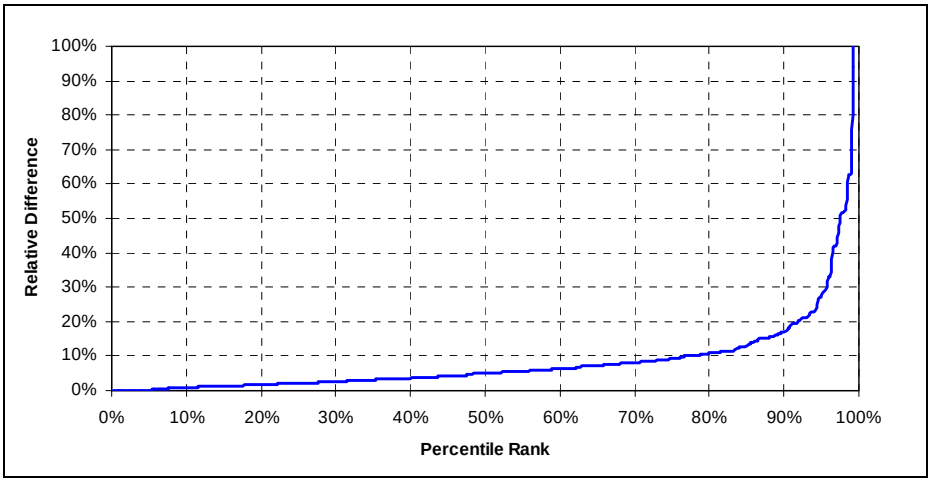


Figure 13-4: Percentile Rank Chart, Reassay Results, Au (g/t), 442 Samples



13.3 Standard Reference Material

In 2003, Corriente had the ALS prep lab in Quito prepare two new SRMs for them: MS1 and MS2. The procedures outlined below were used for making these SRMs.

The SRMs were prepared by extracting 100 kg of material from a homogenized 500 kg bulk sample of drill core rejects (-10 mesh). The material was pulverized in a standard laboratory rod mill by grinding the 100 kg of drill core rejects to –150 mesh and then blanket rolling them (four corners technique) to homogenize. The pulp was immediately stored in paper envelopes (100 g) ready for submission for round robin analysis.

MS1 represents the middle grade range for Cu and Au at the Mirador deposit (0.80 Cu % and 0.287 Au g/t) and MS2 is a low-grade Cu-Au standard (0.37 Cu % and 0.16 Au g/t). Both SRMs were submitted for round-robin analysis at four laboratories, Analytical Laboratories Ltd, ALS Chemex, International Plasma Laboratories (IPL) and Assayers Canada. Each laboratory received 10 samples. The round robin analysis results were of sufficiently good quality to establish the acceptance limits for the SRMs (See Figures 13-5 to 13-8). They were inserted into the sample shipments on a 2 in 40 basis.

If a SRM result was found to exceed twice the standard deviation value from the round robin study then the batch of 20 samples was reanalysed until the SRM returned an acceptable value. Some samples on the SRM charts are outside of the acceptable limits. These were not reassayed as they were in areas outside of the mineralized envelope or in areas of below background grade range.

Figure 13-5: MS1 Round Robin and Sampling Results, Au (g/t), (DDH M63 to M90)

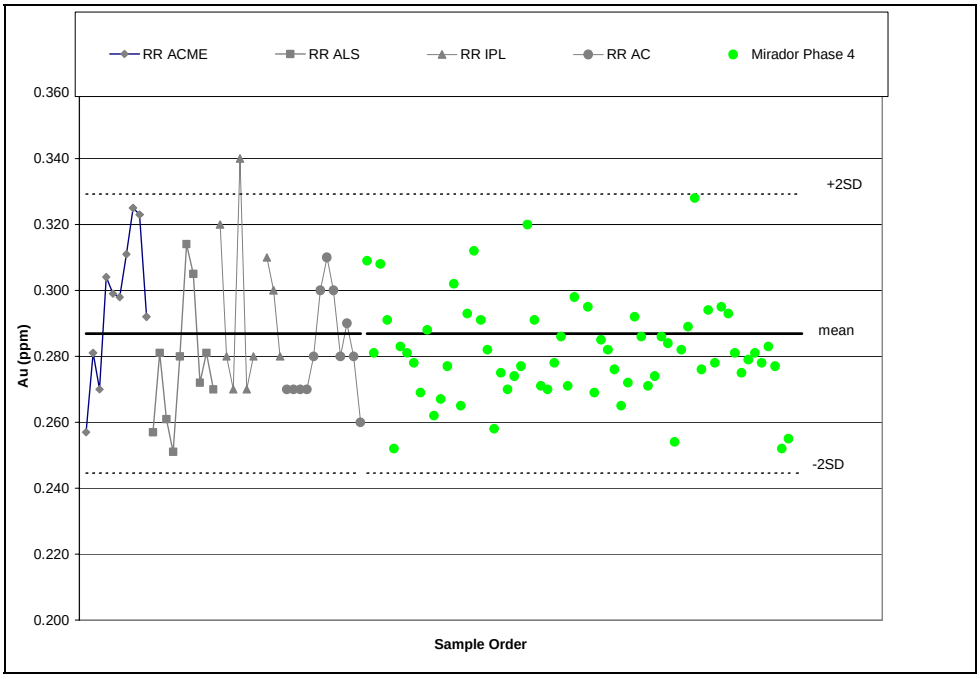


Figure 13-6: MS1 Round Robin and Sampling Results, Cu (%), (DDH M63 to M90)

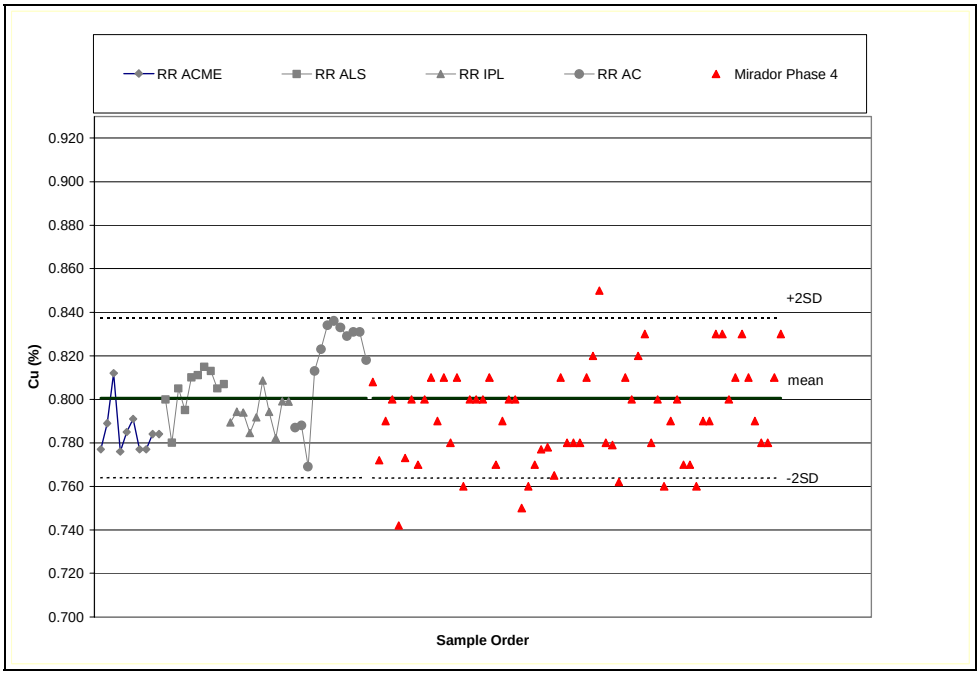


Figure 13-7: MS2 Round Robin and Sampling Results, Au (g/t), (DDH M72 to M90)

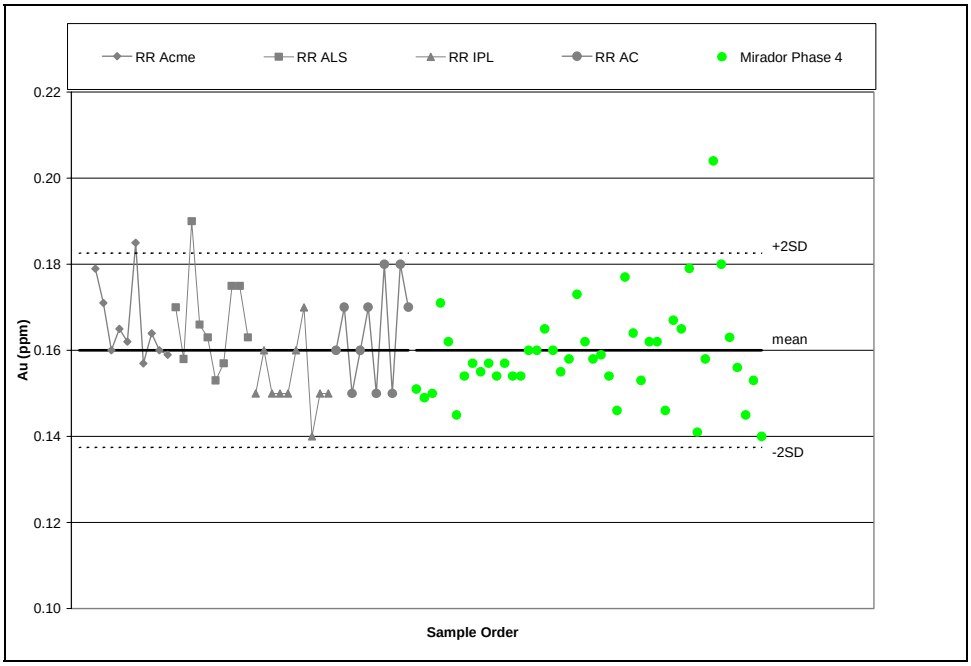
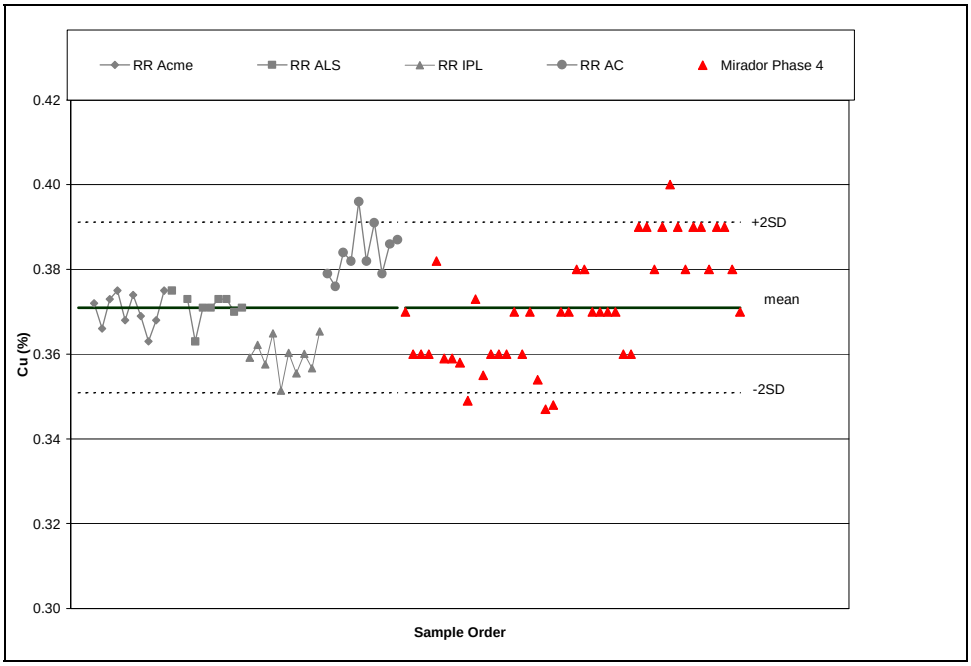


Figure 13-8: MS2 Round Robin and Sampling Results, Cu (%), (DDH M72 to M90)



13.4 Duplicate Samples

Four different types of duplicate samples were variably used at Mirador.

- Phase 1 Only Lab Check Duplicates were taken during this phase of the drilling campaign on a 1 in 10 basis. AMEC has not reviewed the results from these samples. They have been superseded by the reassay results.
- Phase 2 Pulp duplicates were included in the sample shipments on a 1 in 20 basis.
- Phase 3 Pulp duplicates were included in the sample shipments on a 1 in 40 basis.
- Phase 4 Pulp duplicates were included in the sample shipments on a 1 in 20 basis. Coarse Reject duplicates were introduced into the QA/QC program and were taken on a 1 in 20 basis. A small program was begun where for metallurgical holes, the samples were being crushed to ½" and a 1 to 2 kg sample was taken for metallurgical test work. For these holes, a duplicate was taken every 20 samples to monitor the performance of the assay results and study the impact of removing the subsample.

13.4.1 Coarse Crush Duplicates, ½" Crush Material

These duplicates were taken from drill holes M65 to M70 resulting in only 27 duplicate pairs. This is too small of a sample population for a detailed analysis but the few results that are present indicate no bias to the sample analysis results for Cu or Au (Figure 13-9 and 13-10).

13.4.2 Coarse Reject Duplicates

This duplicate type was only introduced during the 4th drilling campaign in 2003 to 2004. Corriente currently has 85 coarse reject duplicates in their database, representing coverage of 3.4% of total assayed samples.

The results of the coarse reject duplicate assays are shown in Figures 13-11 to 13-14. The performance of the Cu results is of excellent quality and reproduces well.

AMEC considers ±20% variation for 90% of the coarse reject duplicate analyses to demonstrate good precision. As seen in Figures 13-13 and 13-14, the variance for both the Cu and Au results are well below the accepted upper limit of 20%.

Figure 13-9: Coarse Crush Duplicate Results, Cu %, 27 Data Pairs

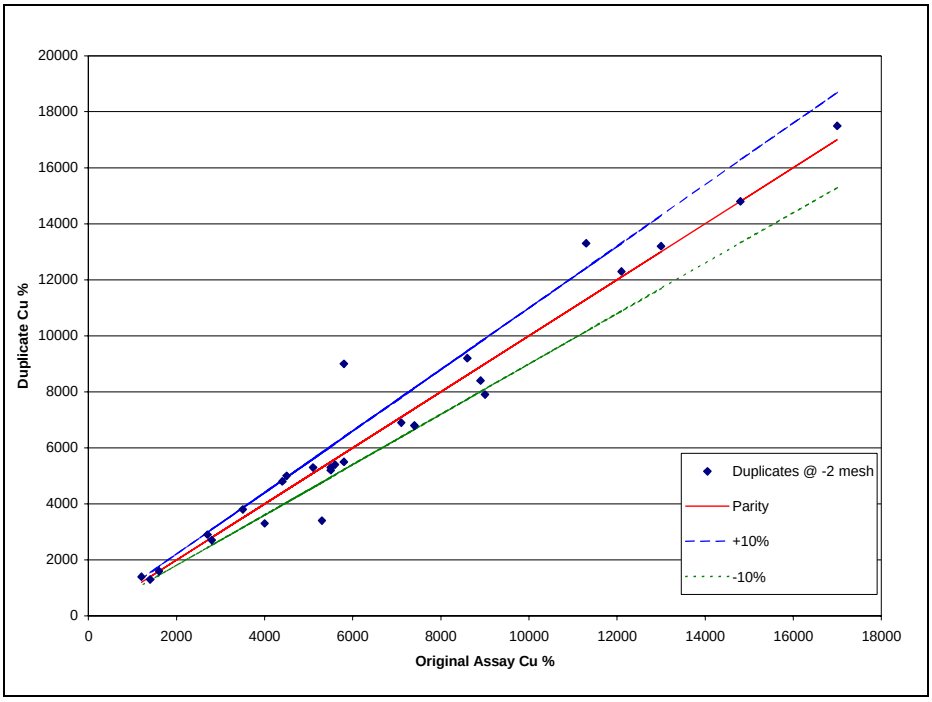


Figure 13-10: Coarse Crush Duplicate Results, Au g/t, 27 Data Pairs

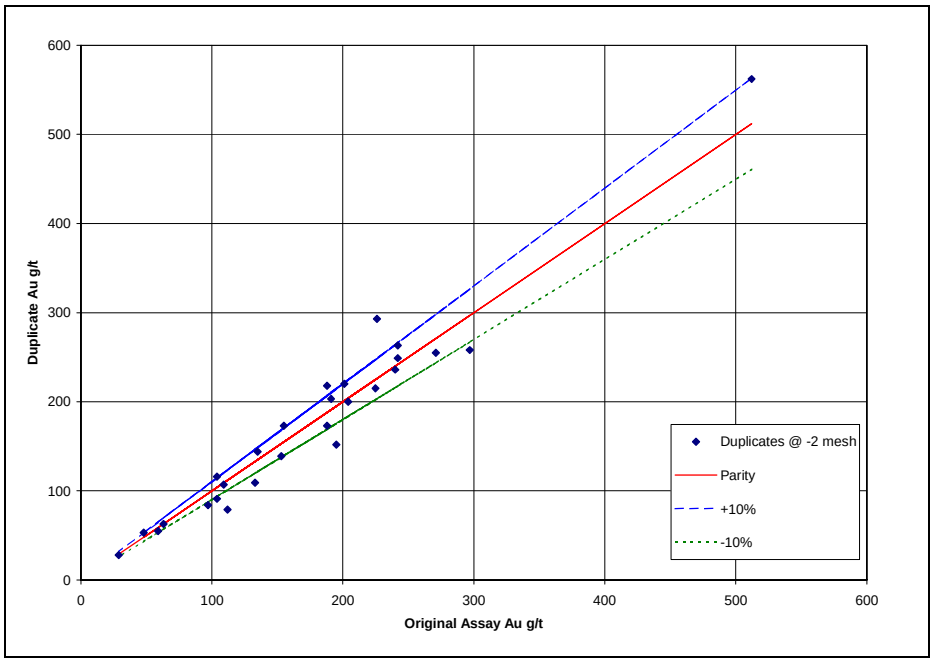


Figure 13-11: Coarse Reject Duplicate Results, Cu %, Scatter Plot

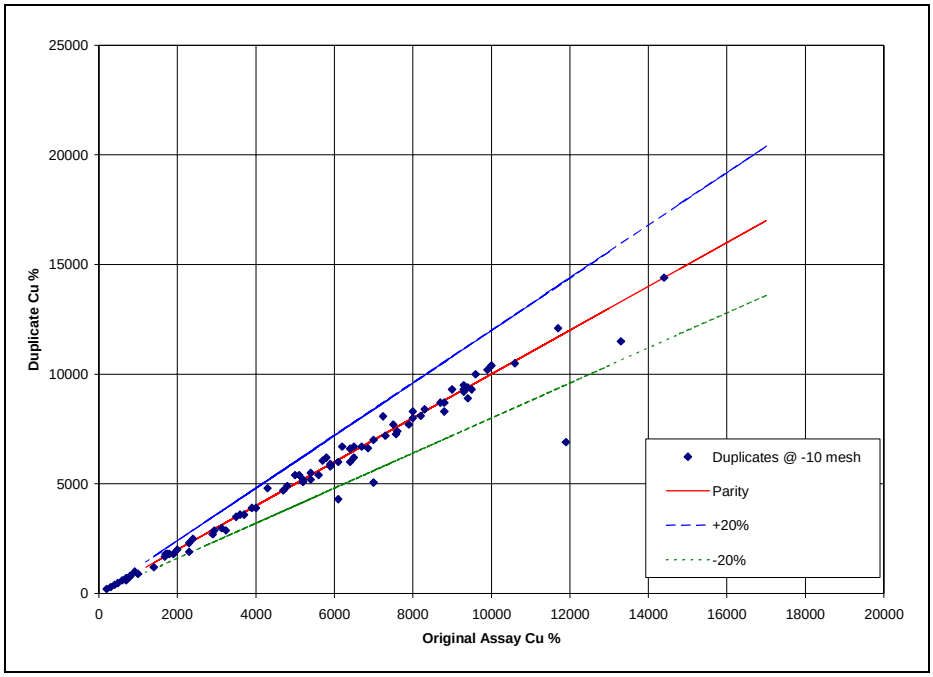


Figure 13-12: Coarse Reject Duplicate Results, Au g/t, Scatter Plot

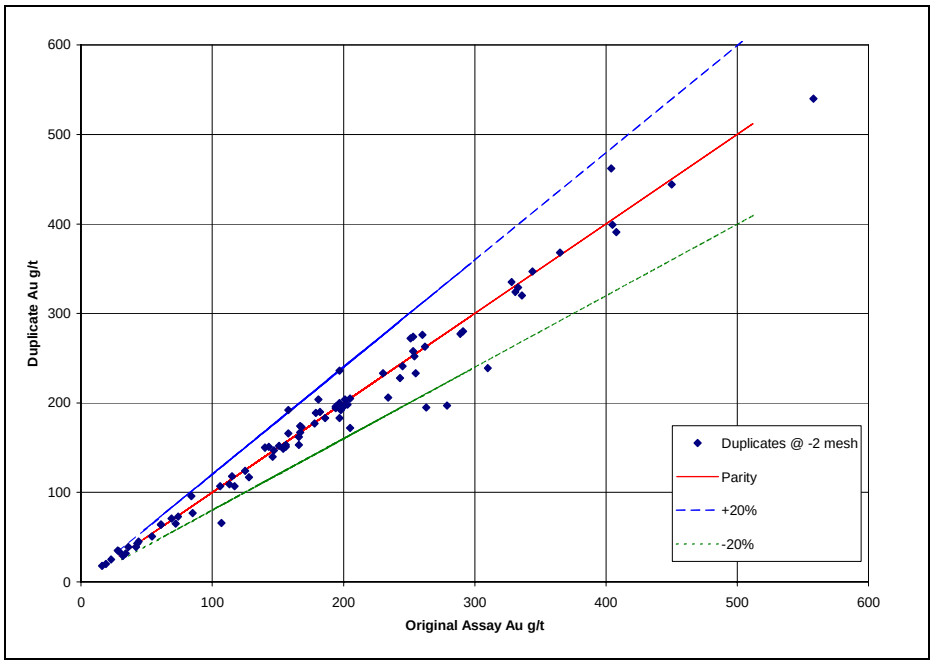


Figure 13-13: Duplicate Results, Cu %, Percentile Rank Chart

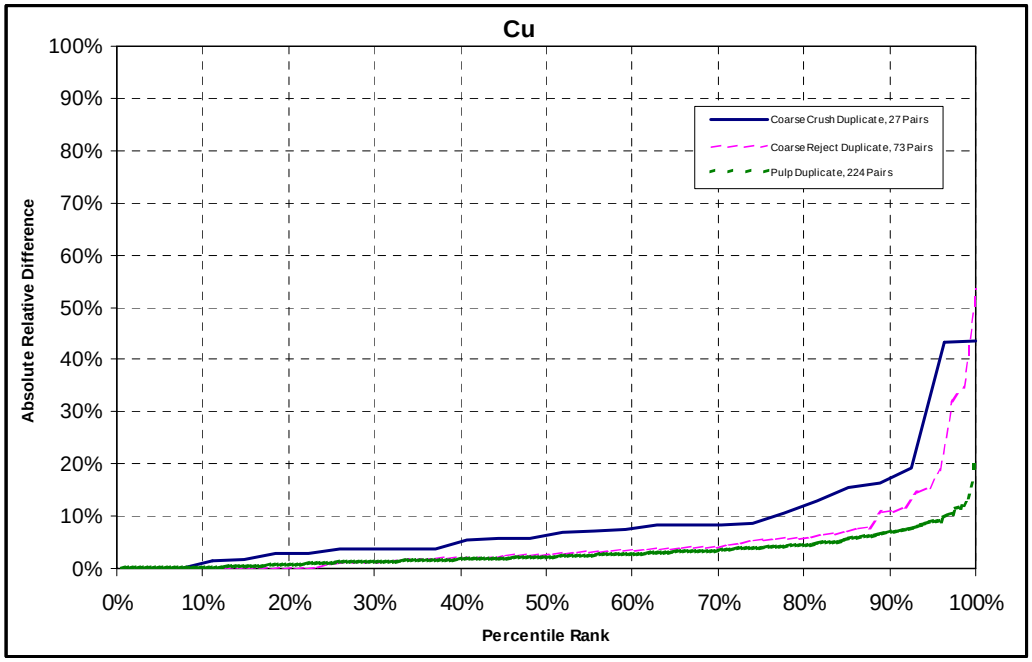
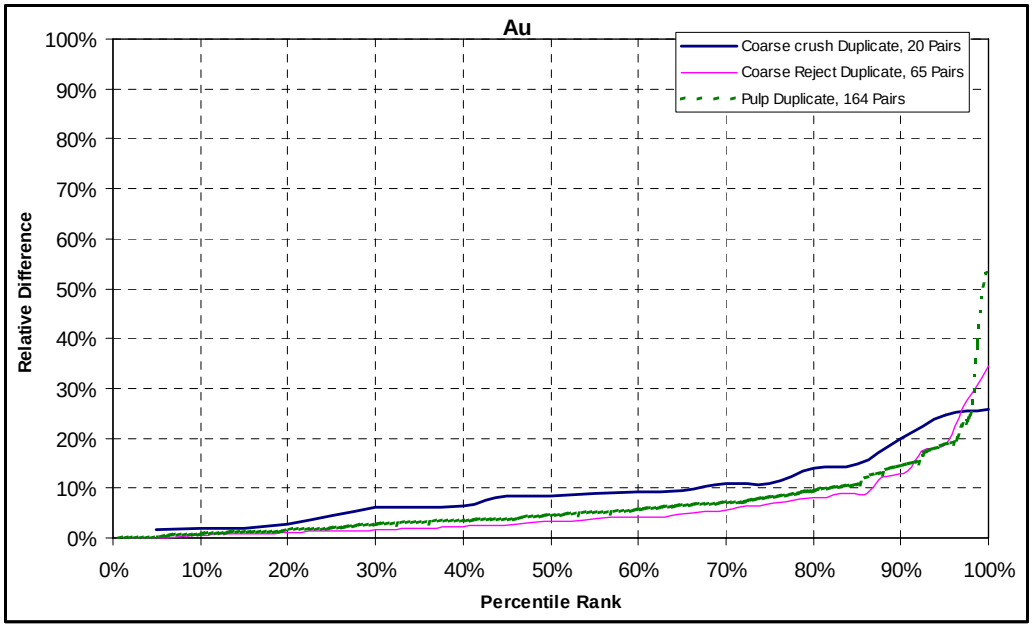


Figure 13-14: Duplicate Results, Au g/t, Percentile Rank Chart



13.4.3 Pulp Duplicates

There are 248 pulp duplicates in the Mirador database representing 4.3% of the assay database.

The results of the pulp duplicate assays are shown in Figures 13-13 and 13-16. Performance for the Cu values is excellent. The performance for the Au values is of acceptable quality considering its minor economic role in the deposit.

AMEC considers ±10% variation for 90% of the pulp duplicate analyses to demonstrate good precision. The Cu values are plotted in Figure 13-13 on a percentile rank chart. This chart shows that the Cu sample pairs are reporting 90% of the samples have a less than a 10% relative difference. The gold values however are reporting that 90% of the sample population has a relative difference of 15% (Figure 13-14); probably due to the small subsample size of 100 g and the small aliquot size of 30 g.

Figure 13-15: Pulp Duplicate Results, Cu %, Scatter Plot

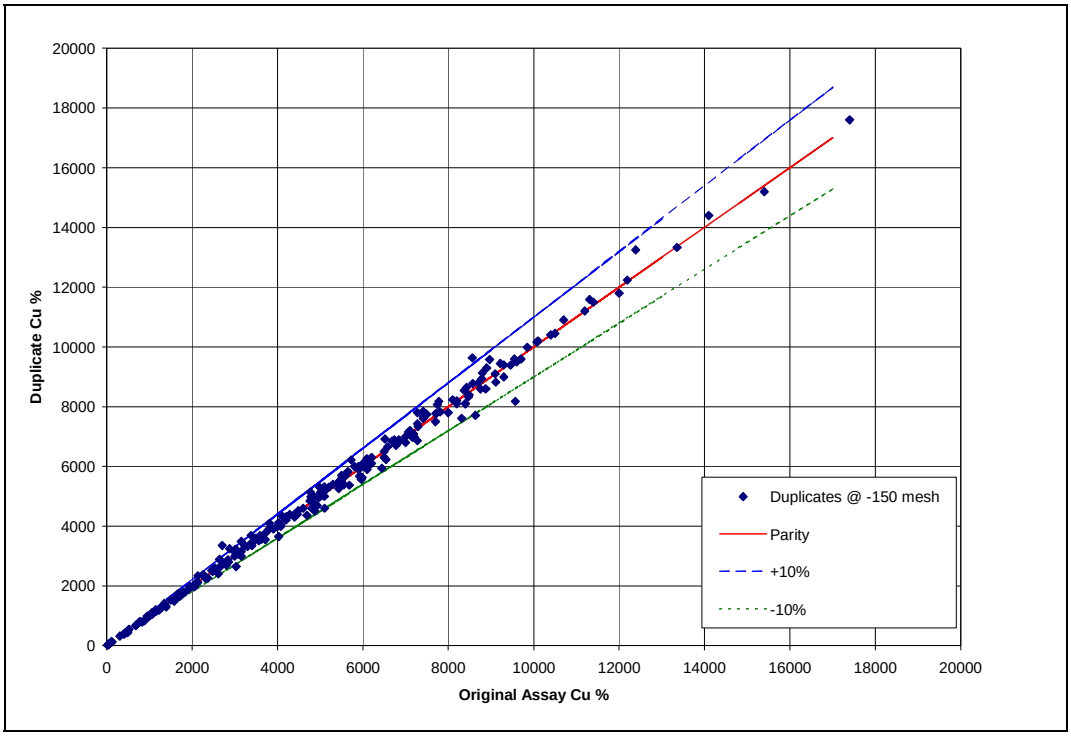
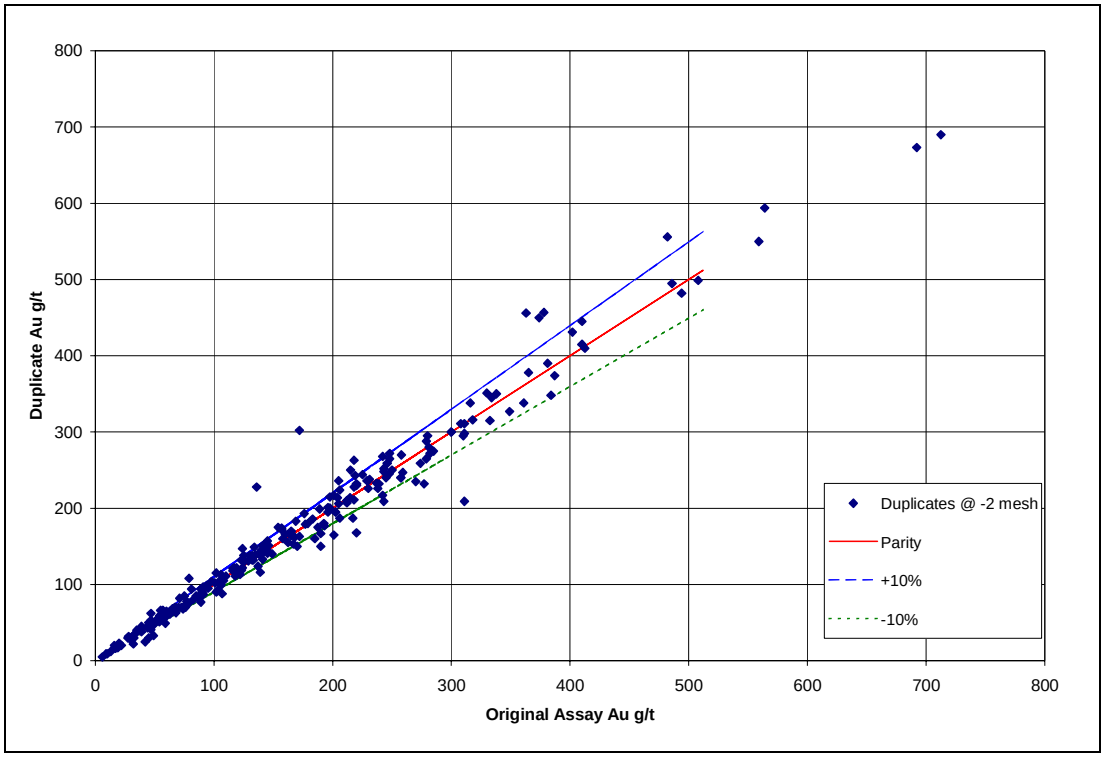


Figure 13-16: Pulp Duplicate Results, Au g/t, Scatter Plot



14.0 DATA VERIFICATION

AMEC completed a data quality check on 5% of the sample database used for the resource estimation. AMEC reviewed the collar surveys, downhole surveys, assay results and bulk density data and used original data sources to confirm the values in the database. The drill holes selected were M02, M12, M18, M33, M46, M54, M67, M77 and M87.

All the data was found to be of excellent quality and adequate for resource estimation purposes.

14.1 Assay Results and Lithology Codes

The assay results for 5% of the copper and gold were reconciled back to the original assay certificates issued by the assay laboratory. The sample intervals and sample number were confirmed by reconciliation to the drill logs for each of the drill holes. The lithology codes were confirmed using the drill logs. No errors were found during this review.

14.2 Downhole Surveys

AMEC checked all the survey disks for the downhole surveys during the site visit to the project. It was found that the geologists were not reading the down-hole tests correctly. On vertical holes, an incorrect azimuth was read on all holes. Corriente did not have a disk reader at the time but have since acquired one. All tests were reread using the proper instrument prior to completing the resource estimation.

During the phase 1 to 3 drill programs, two to three people read the survey disks and the results would be averaged. AMEC found many errors in the averaged value and some instances of errors in the readings. If the three readings are not in agreement than the results should be reviewed and the disks measured again until all are in agreement. Survey results should never be averaged.

14.3 Bulk Density

A total of 20 samples were sent to Teck-Cominco Labs in Vancouver for auditing; results agreed to within 3% for the first method and 0.6% for the second method (See Table 14-1). During the AMEC site visit, Corriente was advised that 5% of these samples should be validated at an independent laboratory.

Overall the averaged values differ very little between the original and the check result. The bulk density values are of sufficient quality for resource estimation purposes.

Table 14-1: Bulk Density Independent Check Results

Hole_ID	Date	Depth	Unit	Method	Corriente	TeckCominco	Relative % Difference
M16	2003	160	Jefp	1	2.67	2.56	-4.2
M44	2003	300	Jzgd	1	2.72	2.66	-2.2
M46	2003	280	Jzgd	1	2.78	2.54	-9.0
M48	2003	350	brmn	1	2.65	2.55	-3.8
M49	2003	400	Jzgd	1	2.75	2.69	-2.2
M51	2003	200	Jzgd	1	2.64	2.53	-4.3
M52	2003	220	Jzgd	1	2.62	2.59	-1.2
M55	2003	300	Jzgd	1	2.60	2.53	-2.7
M56	2003	340	Jzgd	1	2.63	2.66	1.1
				Avg:	2.67	2.59	-3.2
M63	2004	40.0		2	2.24	2.41	7.3
M63	2004	110.0		2	2.65	2.62	-1.1
M63	2004	170.0		2	2.85	2.83	-0.8
M64	2004	67.0		2	2.56	2.50	-2.3
M64	2004	290.0		2	2.72	2.69	-0.9
M64	2004	380.0		2	2.61	2.56	-1.9
M65	2004	140.0		2	2.53	2.48	-2.1
M65	2004	260.0		2	2.56	2.56	0.0
M66	2004	110.0		2	2.68	2.64	-1.6
M66	2004	140.0		2	2.57	2.52	-2.1
M66	2004	230.0		2	2.58	2.55	-1.3
				Avg:	2.60	2.58	-0.6

Methods: **1** = sample weighed dry, then immersed in water, and water displaced weighed; arm balance. **2** = suspended sample weighed in air, then immersed in water; electronic balance

15.0 ADJACENT PROPERTIES

There are no adjacent property activities of importance to the Mirador Project.

16.0 MINERAL PROCESSING AND METALLURGICAL TESTING

A significant amount of metallurgical testwork has been undertaken on mineralized samples from the Mirador porphyry copper-gold porphyry deposit since 2002. SGS Lakefield Research (Lakefield), in Lakefield, Ontario carried out the main program of feasibility testing between December 2003 and September 2004. At present, Lakefield's report is being finalized.

In April 2002, Resource Development Inc. (RDI) conducted three batch rougher flotation tests on an unidentified sample. In June 2003, Sumitomo Metal Mining Co., Ltd (Sumitomo) conducted a scoping level metallurgical program on five drill core samples. This testing included batch rougher and cleaner flotation, mineralogical and chemical analysis of concentrates, and a bond work index determination. The liberation characteristics of the ore were also investigated. Overall the results of the RDI and Sumitomo testwork are consistent with subsequent Lakefield testing.

In late 2003 and early 2004 a total of about 3,000 kg of split diamond drill core were collected from twenty drill holes and shipped to SGS Lakefield Research (Lakefield) in Lakefield Ontario, for feasibility metallurgical testing. In addition, two whole core metallurgical holes were drilled and collected specifically for comminution testwork.

The feasibility metallurgical testwork carried out by Lakefield was done under the direction of AMEC. Lakefield also provided samples to MinnovEx and G&T Metallurgical Services (G&T) to conduct SPI grindability testwork, and mineralogical and flotation quality control testwork respectively.

Four master composites were produced from the core samples for initial flowsheet and design criteria development testwork. This indicated the mill flow sheet for Mirador will be a conventional copper-gold porphyry flowsheet, with relatively coarse primary SAG and ball mill grinding to about 150 µm followed by copper rougher flotation, concentrate regrind to 25 µm, and cleaner flotation and dewatering. Metallurgical testing and mineralogical quantitative modal liberation analysis, conducted by G&T, supported the selection of the grind parameters.

Variability mapping test work completed during the second quarter of 2004 subsequently confirmed that the ore is quite simple metallurgically and mineralogically, and responds consistently well to the conventional flowsheet and reagent scheme selected. Over forty-five variability samples were produced and tested by depth. Each composite was subjected to chemical and mineralogical analysis, grindability testing, and locked cycle flotation. Locked cycle concentrates were subjected to chemical, mineralogical and dewatering testing. Two drill holes consisting of whole core were

used for additional grinding testwork, including JK drop-weight and MinnovEx SPI testing.

Considerable effort has gone into the characterization of the orebody variability using automated quantitative microscopy methods. Each of the Variability Composites was studied by QemSCAN (Quantitative Evaluation of Mineralogy by Scanning Electron Microscopy) analysis at Lakefield. This indicated the deposit is relatively simple and homogenous mineralogically. Copper is hosted dominantly as chalcopyrite, in a primary sulphide zone that is open at depth, with minor amounts of secondary copper enrichment mainly developed as a shallow 0 m to 20 m thick chalcocite blanket zone overlying the primary sulphide ore. Overall mineralogically, it is reasonable to expect the ore will respond well metallurgically to conventional copper porphyry flotation processing at moderate grinds and with acceptably good commercial copper recoveries and concentrate grades. This assessment is consistent with the metallurgical performance achieved in the variability testing.

Pyrite occurs widely throughout the deposit, but at relatively low levels, and the pyrite to chalcopyrite ratio, at about 3:1, is in the lower quartile of the industry. The pyrite is also coarse, averaging 98 µm, relative to the chalcopyrite grain size, which is quite consistent and averages about 40 µm. Both these factors favour good flotation cleaner metallurgy; even using the relatively neutral bulk sulphide rougher flotation mode of operation selected, and results in a relatively clean concentrate with a 30% copper grade. Silicates are predominantly quartz, feldspars and micas, the three groups constituting 95.4% of the non-sulphide gangue, while clays (2.1%) and carbonates (1%) comprise the remainder.

The secondary copper mineral grain size is moderately finer and the rougher flotation will be operated in a more selective mode to avoid activating pyrite during regrinding. As a result, the early production of copper from the secondary copper zone requires a higher rougher flotation pH and a finer regrind scheme, and sufficient flexibility has been incorporated in the design of the mill to accommodate this.

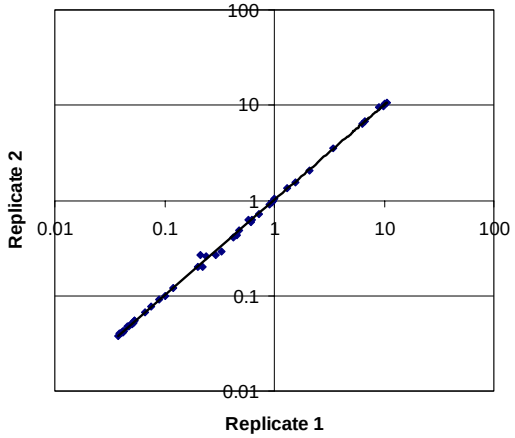
Concentrates produced are predicted to average 30% copper at a recovery of 91%. Gold recovery is expected to average 47%. A gold behaviour model developed from flotation test data suggests gold tracks chalcopyrite, pyrite and gangue, with near equal weighting throughout the process. A laboratory analysis of concentrates indicated that no significant deleterious penalty element impurities were present.

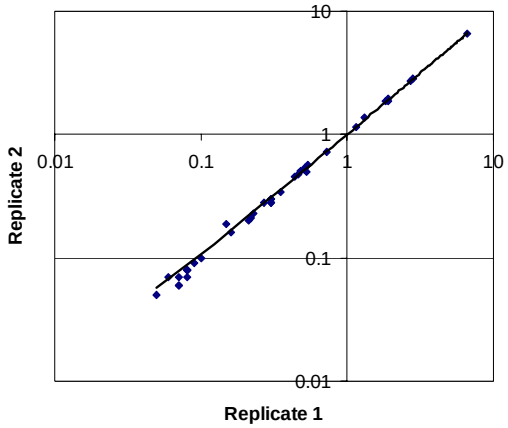
Grindability tests were conducted on intervals of core from individual drill holes during the test programme. These included Bond Work Index tests, J-K drop weight and SMC tests (an abbreviated form of JK test), and MinnovEx SPI tests. All tests were

conducted at Lakefield, except the latter, which were conducted at MinnovEx on samples provided by SGS Lakefield Research. Tests indicated an average Bond ball mill work index of 14.5 kWh/t, and rank the ore hardness as average to moderately low relative to other copper porphyry ores in Lakefield's industry database and with moderately low variability.

A replicate assay quality control programme was conducted as an ongoing evaluation of the assay data obtained during this project. The results are shown in Figure 16-1. The replicate assay programme, determining to deviation in assay due to procedural variances in the laboratory, shows excellent assay repeatability. Relative assay deviations are typically 1% to 3%. Typical variability in these programmes on copper porphyry ores are 3% to 4%.

Figure 16-1: Results from Replicate Assay QC Programme





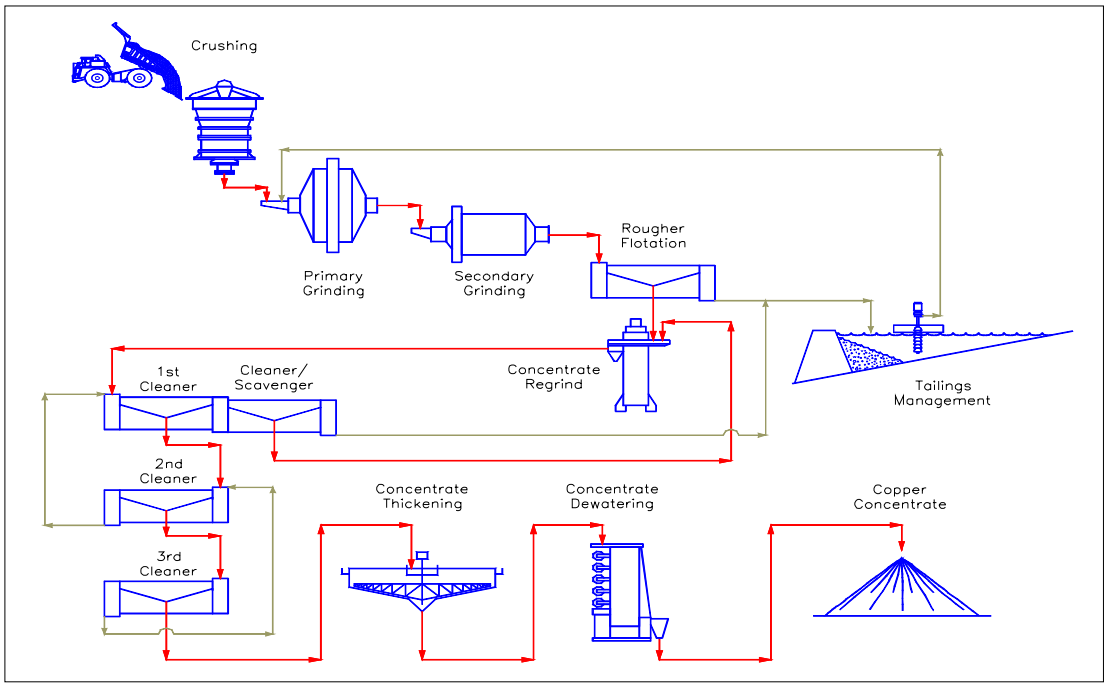
Copper: Assay Relative Deviations: >1% (fusion XRF), 1.2% (fusion XRF), 0.1-1%, 3.2%, <0.1% (AA), 1.6%

Gold: Assay Relative Deviation: 2.0%.

The estimated mineral reserves included in the mine plan total 115 Mt grading 0.67% Cu and 0.22 g/t Au. Silver and molybdenum are present but the grades are relatively low. Approximately 85 Mt of overlying waste rock will be removed over the mine life, resulting in an average strip ratio of 0.8:1. The process will be designed to treat 25,000 t/d of material.

A simplified schematic drawing of the proposed flowsheet is provided in Figure 16-2. Run-of-mine open pit ore will be crushed in a gyratory crusher. The crushed ore will be processed by means of semi-autogenous and ball mill grinding followed by rougher flotation, regrind, cleaner flotation and dewatering to produce copper concentrate. The concentrate will be trucked via the existing road network in the area to a port facility in Machala for shipment to smelters. Tailings from the process will be impounded in a tailings pond; water will be reclaimed from the tailings pond and reused in the process.

Figure 16-2: Simplified Mirador Flowsheet



16.1 Metallurgical Recoveries

A summary of the projected metallurgical recoveries and metal balance from Lakefield's testwork is provided in Table 16-1.

Table 16-1: Mirador Metallurgical Recoveries and Metal Balance

Ore Type Depth/Phase	Supergene (<20 m)	Shallow (Mixed) (0-5 yr) #1	Mid Primary (6-10 yr)	Deep Primary (11-15 yr)	Overall (0-15 yr)
Copper concentrate grade, %	27.4	30.0	29.2	30.5	29.8
Copper recovery, %	88.4	89.8	91.7	92.9	91.2
Gold recovery, %	44.2	48.1	46.1	46.2	47.0
Copper losses:					
Rougher tails, %	7.9	6.7	5.8	5.0	6.0
Cleaner Scav tails, %	3.7	3.4	2.5	2.1	2.8
Gold losses:					
Rougher tails, %	27.7	29.2	28.6	34.3	30.2
Cleaner Scav tails, %	28.1	22.7	25.3	19.5	22.9

17.0 MINERAL RESOURCE AND MINERAL RESERVE ESTIMATES

The mineral resource for the Mirador Deposit was estimated under the direction of Susan Lomas, P.Geo., of AMEC. The estimate was made from a 3-dimensional block model utilizing commercial mine planning software (Gemcom®).

17.1 Geology and Grade Domains

Key geologic units at Mirador comprise intrusive phases of the host porphyry and post mineral dykes. These comprise:

- Zamora Granodiorite to Quartz Monzonite (JZGD)
- Breccia with JZGD and JEFP Fragments (BRMN)
- Early Hornblende-Feldspar Porphyry (JEFP)
- Late Hornblende-Feldspar-Quartz Porphyry (JHBP)
- Late Breccia, Unaltered, Polymictic (JHPM)

Also investigated were the various supergene-altered phases: Leach, Enriched and Mixed. Geologic models were created of the intrusive and altered units. AMEC checked the shapes for interpretational consistency on section and plan, and found them to have been properly constructed.

To constrain grade interpolation in each of the zones, AMEC created 3-dimensional mineralized envelopes based on copper and gold grades. These were derived by a method of Probability Assisted Constrained Kriging (PACK) to initially outline a general shape. Threshold grades were 0.2 g/t for Au and 0.5 % for Cu. The probability that gold or copper in any block in the model exceeded the threshold was estimated using indicator variograms and ordinary kriging. Contoured probability values (in increments of 0.05) defined potential volumes used to delineate mineralized and non-mineralized populations. The boundary formed by each contour line was called an estimation envelope or “shell”. The grade outline selection was done by inspecting the contoured probability values (in increments of 0.05) in Gemcom®. Final probability values were 0.40 for Au and 0.48 for Cu. Additionally, a Cu shell at around the 0.30 probability value was made to help constrain grade interpolation in the background (or Outside Shell) domain. These shapes were then edited on plan and section views to be consistent with the structural and lithologic models and the drill assay data so that the boundaries did not violate data and current geologic understanding of mineralization controls.

The solids were used to code the drill hole data and block model cells. A set of cross sections and plans with drill holes colour-coded by domain and blocks similarly coloured were plotted and inspected to determine the proper assignment of domain.

17.2 Data Analysis

The data analyses were conducted on original and composited assay data. Assays were composited into 6 m down-hole composites. The compositing for the data analysis honoured the main lithology categories according to logged data and then were segregated by zone and grade shell or background codes. AMEC reviewed the compositing process and found it to have been performed correctly.

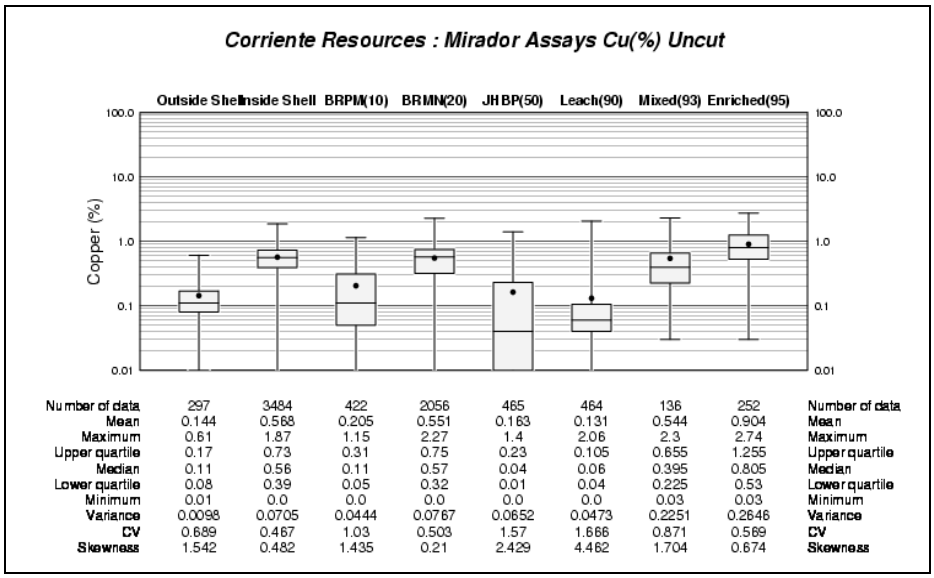
Descriptive statistics (boxplot analyses), contact plots, and histograms have been completed for copper and gold. Results obtained were used to guide the construction of the block model and the development of estimation plans.

Grade distributions of the assays by rock and alteration type, and grade probability shell are shown as box plots in Figures 17-1 and 17-2 (assays) and Figures 17-3 and 17-4 (6 m composites). Box-plots show the frequency distribution of the assay values by way of a graphical summary. The vertical axis of the plot gives the range of values for the particular assay (total copper). The box shows the portion of the sample data that falls between the 25^{th} and the 75^{th} percentiles. In other words, the box captures the half of the data, which falls in the middle of the distribution. The horizontal line that appears in the box represents the median of the data, or that value where half of the assays are greater and the remaining half are less than this median value. The mean or average of the data is shown with a dot. The vertical lines that extend away from the box reach to the minimum toward the bottom of the plot and to the maximum value toward the top.

Key observations from these analyses are:

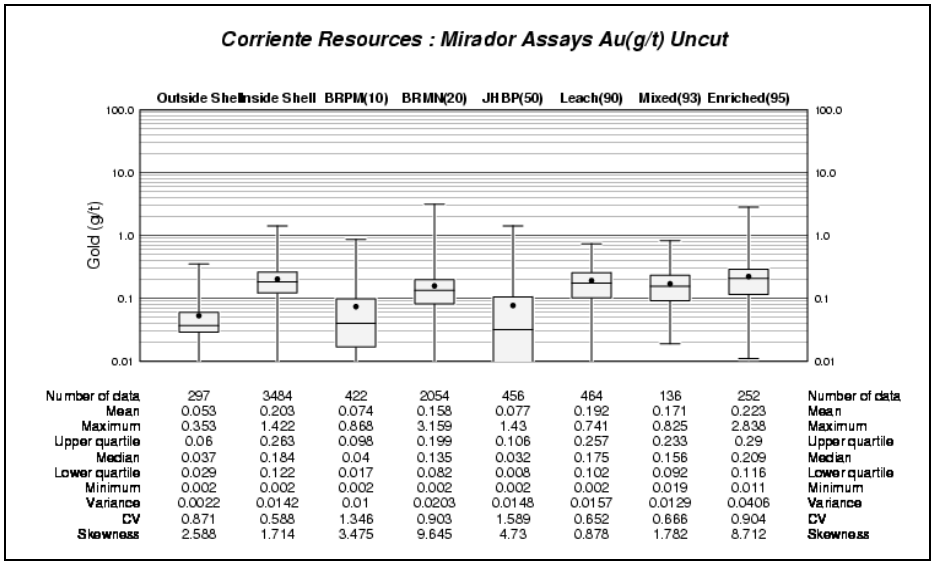
- The domaining and tagging of the assay and the composite data functioned well. The domains used for grade interpolation (Inside Shell and BRMN (20)) and waste (BRPM (10) and JHBP (50)) were well selected as indicated by the grade populations inside each domain.
- The mean values per domain agree within accepted limits between the assay results and the subsequent composited data.

Figure 17-1: Box Plot of Cu Assay Results by Litho Code



	Outside Shell	Inside Shell	BRPM(10)	BRMN(20)	JHBP(50)	Leach(90)	Mixed(93)	Enriched(95)	
Number of data	297	3484	422	2056	465	464	136	252	Number of data
Mean	0.144	0.568	0.205	0.551	0.163	0.131	0.544	0.904	Mean
Maximum	0.61	1.87	1.15	2.27	1.4	2.06	2.3	2.74	Maximum
Upper quartile	0.17	0.73	0.31	0.75	0.23	0.105	0.655	1.255	Upper quartile
Median	0.11	0.56	0.11	0.57	0.04	0.06	0.395	0.805	Median
Lower quartile	0.08	0.39	0.05	0.32	0.01	0.04	0.225	0.53	Lower quartile
Minimum	0.01	0.0	0.0	0.0	0.0	0.0	0.03	0.03	Minimum
Variance	0.0098	0.0705	0.0444	0.0767	0.0652	0.0473	0.2251	0.2646	Variance
CV	0.689	0.467	1.03	0.503	1.57	1.666	0.871	0.569	CV
Skewness	1.542	0.482	1.435	0.21	2.429	4.462	1.704	0.674	Skewness

Figure 17-2: Box Plot of Au Assay Results by Litho Code



	Outside Shell	Inside Shell	BRPM(10)	BRMN(20)	JHBP(50)	Leach(90)	Mixed(93)	Enriched(95)	
Number of data	297	3484	422	2054	456	464	136	252	Number of data
Mean	0.053	0.203	0.074	0.158	0.077	0.192	0.171	0.223	Mean
Maximum	0.353	1.422	0.868	3.159	1.43	0.741	0.825	2.838	Maximum
Upper quartile	0.06	0.263	0.098	0.199	0.106	0.257	0.233	0.29	Upper quartile
Median	0.037	0.184	0.04	0.135	0.032	0.175	0.156	0.209	Median
Lower quartile	0.029	0.122	0.017	0.082	0.008	0.102	0.092	0.116	Lower quartile
Minimum	0.002	0.002	0.002	0.002	0.002	0.002	0.019	0.011	Minimum
Variance	0.0022	0.0142	0.01	0.0203	0.0148	0.0157	0.0129	0.0406	Variance
CV	0.871	0.588	1.346	0.903	1.589	0.652	0.666	0.904	CV
Skewness	2.588	1.714	3.475	9.645	4.73	0.878	1.782	8.712	Skewness

Figure 17-3: 6 m Composite Box Plot, Cu (%)

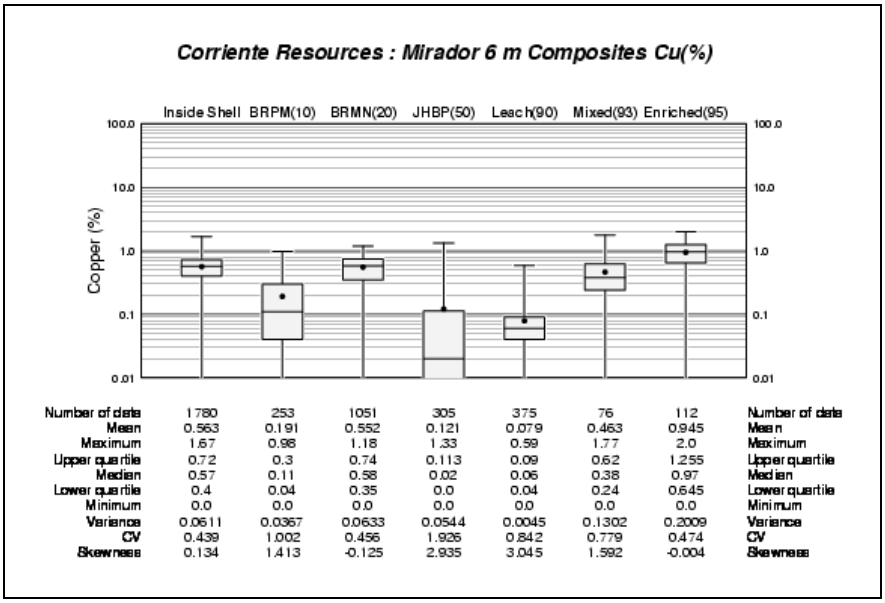
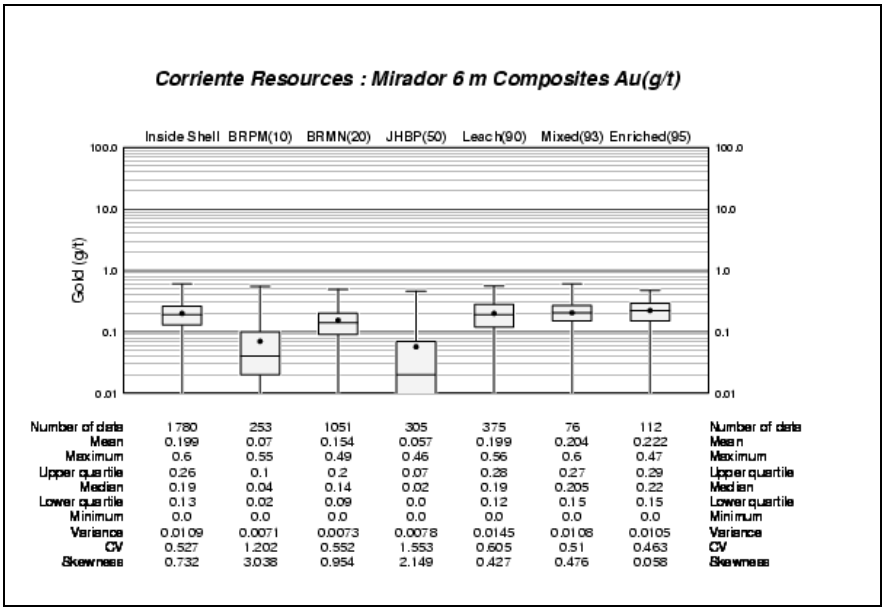


Figure 17-4: 6 m Composite Box Plot, Au (g/t)



Contact plots were generated to explore the relationship between grade and grade shell codes. The plots are constructed with software that searches for data with a given code, and then searches for data with another specified code and bins the grades according to the distance between the two points. This allows for a graphical

representation of the grade trends away from a “contact”. If average grades are reasonably similar near a boundary and then diverge as the distance from the contact increases, the particular boundary should probably not be used as a grade constraint. In fact, if a hard boundary is imposed where grades tend to change gradually, grades may be overestimated on one side of the boundary and underestimated on the opposite side. If there is a distinct difference in the averages across a boundary, there is evidence that the boundary may be important in constraining the grade estimation.

Contact profiles, or plots, were made for Cu and Au across the grade probability shells. The chart for Cu is shown in Figure 17-5 and gold is shown in Figure 17-6. The charts show that the two populations (inside and outside the grade probability shells) have a gradual grade change over a distance of approximately 25 m. Beyond this distance the grade ranges of the two populations are distinct. Beyond the 25 m buffer, Cu grades inside the grade probability shell are just above 0.60 % while outside of the shell the grades are below 0.40 % Cu. Beyond the 25 m buffer, Au grades inside the grade probability shell are just above 0.225 g/t while outside of the shell the grades are below 0.150 g/t Au.

Figure 17-5: Contact Profile – Inside and Outside of Cu Grade Probability Shell

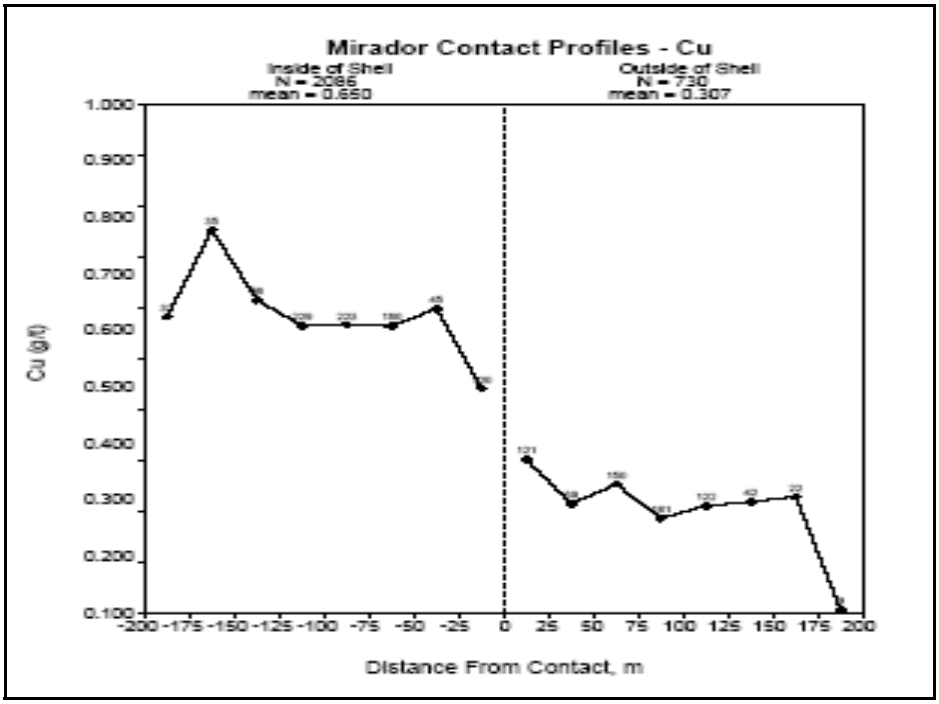
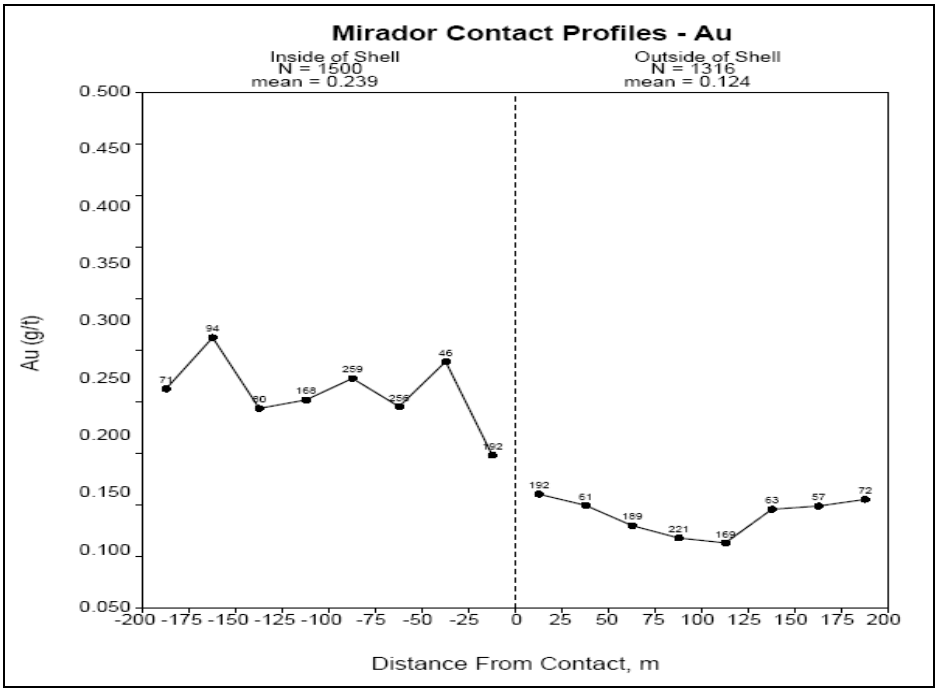


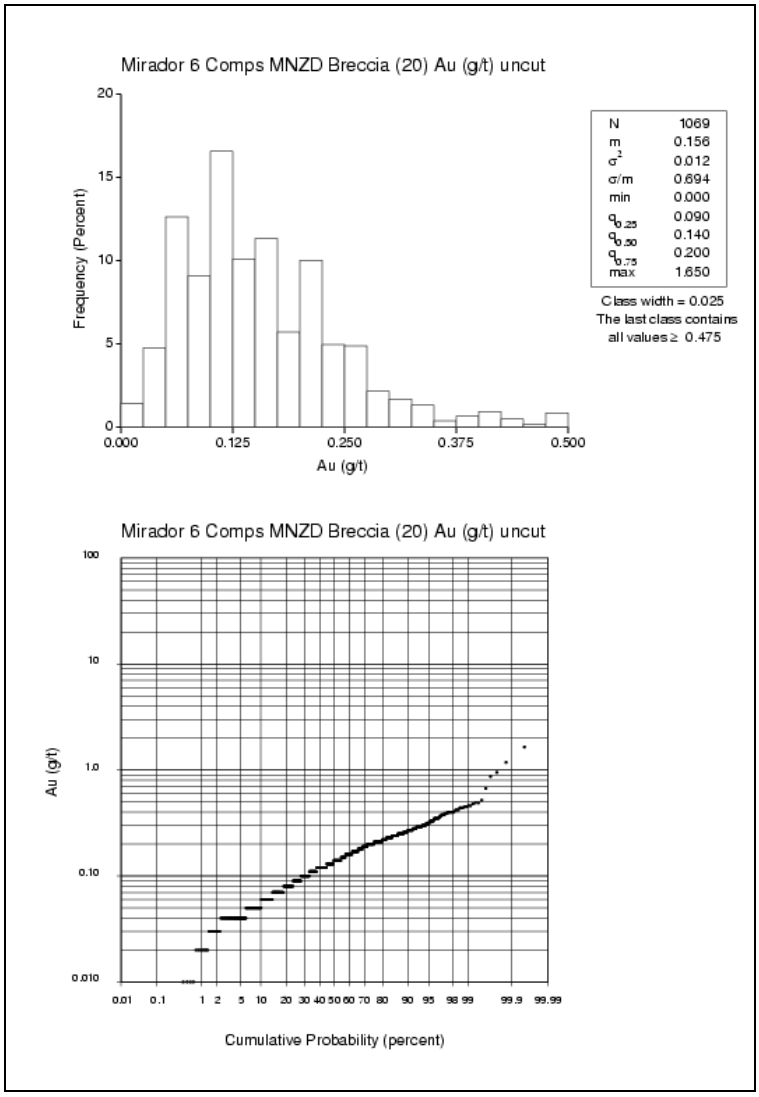
Figure 17-6: Contact Profile – Inside and Outside of Au Grade Probability Shell



17.3 Evaluation of Extreme Grades

Extreme grades were examined for copper and gold composite values, mainly by histograms and probability plots. Generally, the distributions do not indicate a problem with extreme grades for copper. Gold showed extreme grade values (Figure 17-6) where a clear break in the sample trend is observed at 0.60 Au g/t. AMEC implemented a gold grade cap at the break value (0.60 g/t) to the assay data prior to grade interpolation.

Figure 17-7: Histogram – Probability Plot of 6m Composites, Au g/t



17.4 Variography

Variography is the study of the spatial variability of an attribute. AMEC prefers to use a correlogram, rather than the traditional variogram, because it is less sensitive to outliers and is normalized to the variance of data used for a given lag. The correlogram ranges from -1 to +1, although models are usually made over the interval [0,1], where 0 represents no correlation (statistical independence) and 1 represents perfect correlation.

Correlograms were calculated for copper and gold for all hypogene samples and then for the composites inside the grade probability shells. The approach to correlogram model development is to calculate a relatively large number of sample correlograms in several directions using composite samples. Directional sample correlograms are calculated along horizontal azimuths of 0°, 30°, 60°, 90°, 120°, 150°, 180°, 210°, 240°, 270°, 300° and 330°. For each azimuth sample correlograms are also calculated at a dip of -30, -60 in addition to horizontally. Finally a correlogram is calculated in the vertical direction. Using the 37 sample correlograms, an algorithm determines the best-fit model. This model consists of a nugget effect; single or two-nested structure variance contributions; ranges for the variance contributions; and the model type (spherical or exponential type). After fitting the variance parameters, the algorithm then fits an ellipsoid to the ranges from the directional models for each structure. The anisotropy in grade variation is given by the two ellipsoids.

Variography was completed for gold and copper on composite data form the main mineralized unit within and outside the grade probability shells. Only hypogene material was investigated (due to paucity of data in the supergene domains). Variogram model parameters and orientation data of rotated variogram axes are shown in Table 17-1. The correlograms are included in this report in Appendix B for gold and copper.

Table 17-1: Variogram Results, ZYZ Rotations and rotated variogram axes

Metal and Structure	Structure	Nugget Effect	Sill	Axis	Orientation (Azimuth/Dip)	Gemcom Rotation Type	Rotation Angles	Range
Cu	1st	0.100	0.585	X	221/0			43
				Y	131/35	ZYZ	-42, -36, -89	72
				Z	312/54			150
	2nd		0.315	X	65/9			301
				Y	336/-1	ZYZ	16, -10, 8	126
				Z	254/81			200
Au	1st	0.190	0.365	X	160/23			47
				Y	44/46	ZYZ	2, -55, -61	25
				Z	268/35			22
	2nd		0.445	X	94/2			79
				Y	4/0	ZYZ	7, -2, -11	244
				Z	263/88			200

Note: Models are spherical. ZYZ rotation is right-hand-rule

The copper correlograms showed ENE-WSW trending, steeply dipping structures while the gold correlograms showed NS trending, subvertical structures. These

observations match the property geology where observed trends are in similar orientations.

The nugget effects, or random variation components of spatial variation, tend to be moderate. Copper variograms generally have nugget effects of 0.10 or was modelled as 10% of the total variability. The gold variograms had a nugget effect of 0.19 or accounted for 19% of the variability.

17.5 Grade Model and Interpolation Plan

The Mirador grade block model limits are (in UTM coordinates) 783500 to 786005 east, 9603000 to 9605505 north and 2000 to 200 m elevation. Block size is 15 m in the easting and northing directions and 12 m in height.

The geology and grade solids were used to assign rock codes to the block model as listed in Table 17-2. Blocks above the topographic surface were tagged as air and blocks outside of the Outer Shell were tagged as waste. A percent model was used to control the volume of blocks inside the solids. The data analyses demonstrated that the post mineral dykes should be treated as separate domains, representing unmineralized material and were treated as waste.

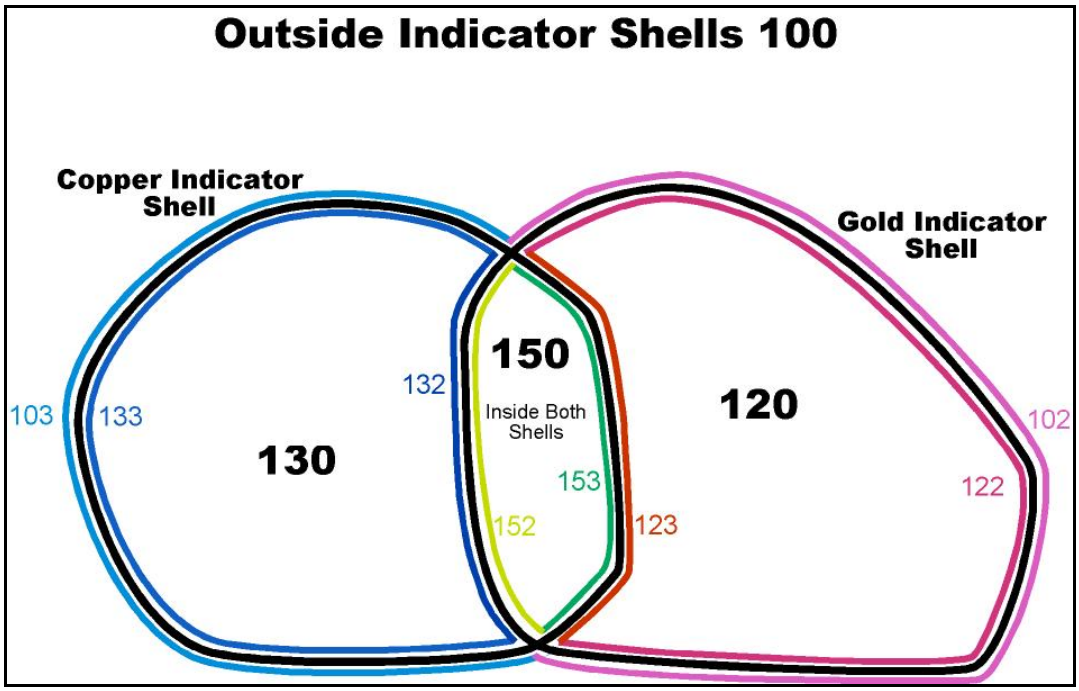
Table 17-2: Block Model Rock Codes

Rock Codes	Zone Name
90	Leached
93	Mixed
95	Enriched
100 series	Outside Grade probability shells but Inside Krige Shell
120 series	Au Grade probability shell
130 series	Cu Grade probability shell
150 series	Inside Both Au and Cu Grade probability shells
900	Waste
999	Air

The grade probability shells were used as soft boundaries for interpolation purposes. This means that the blocks around the boundary of the indictor shells were able to see the composites from holes found both outside and inside the shells. A FORTRAN program was written to identify blocks that were within 30 m of the shell boundaries and they were given a lithology code based on their position relative to the shell

boundaries. A schematic diagram of the lithology coding system is presented in Figure 17-8.

Figure 17-8: Lithology Codes for Sulphide Blocks



Lithology codes in the block model were used to make certain block selections for interpolation runs. Table 17-3 lists the lithology codes used to control the blocks used for interpolation runs. These block selections were necessary as composite files were made to contain the composites within these shell selections. Composite files were also made that contain all of the composites for the blocks coded in the proximal wall areas of the grade probability shells to be allowed to use data on either side of the shell boundaries.

Table 17-3: Lithology Groups for Grade Interpolation Runs

Interpolation Run	Lithology Codes Used
Inside Cu grade probability shell	130, 132, 133, 150, 152, 153
Outside Cu grade probability shell	100, 102, 103, 120, 122, 123
Inside Au grade probability shell	120, 122, 123, 150, 152, 153
Outside Au grade probability shell	100, 102, 103, 130, 132, 133

Values for copper, capped and uncapped gold, and bulk density were interpolated into the block model using ordinary kriging (OK), inverse distance weighting to the eighth power (ID8) and the nearest-neighbour (NN) methods. Interpolation was restricted by rock code. A minimum of 5 and maximum of 20 composites were used, with an additional parameter for maximum composites per drill hole set to 4. This forces the interpolation to require a minimum of two holes within the search ellipse before a grade value can be assigned to a block.

The search ellipsoid for material in the hypogene was oriented as defined by the variography. Search ranges comprised 400 m along the long axis, orientated at 045°, 200 m down the dip direction (at -80° to the NW) and 300 m vertically. Block discretization is 4 x 4 x 3.

The interpolation of grade for Cu and Au in the supergene blanket area used an isotropic search to find samples within a certain radius of a block centre. The search radii were 150 m in the X and Y directions and 50 m in the Z direction. A minimum of two holes within the search ellipse was required for grade to be interpolated into a block. The data were interpolated using inverse distance weighting to the second power (ID2). A minimum of 3 composites and maximum of 12 composites were required.

17.5.1 Bulk Density interpolation

There are 665 bulk density values for the MNZD (hypogene) rock type with an overall average of 2.64 g/m^3. This is a sufficient quantity of data for interpolation of the values into the block model. Inverse distance to the third power ID3 was used with sufficient ranges to fill all the blocks. A minimum of 3 and maximum of 8 values were used for each block.

The supergene rock types contained only limited density data: 21 Leached zone, 22 Mixed zone and 46 Enriched zone measurements. These values were averaged and the result was tagged into the blocks for the appropriate rock type. The average bulk density values for the Leached, Mixed and Enriched zones are 2.42, 2.47 and 2.51, respectively.

The distribution and summary statistics for the bulk density values by rock type are presented in Appendix C.

17.6 Model Validation

17.6.1 Visual Inspection

AMEC completed a review of the Mirador resource block model. The model was checked for proper coding of drill hole intervals and block model cells. The coding was found to be properly done. Gold and copper grade interpolation was examined relative to drill hole composite values by inspecting the sections and plans. The checks showed good agreement between drill hole composite values and model cell values. Examples of representative sections containing block model copper and gold grades, drill hole composites and grade probability shell outlines are included in Appendix D.

17.6.2 Global Means

AMEC also checked the block model estimates for global bias by comparing the average copper and gold grades from the model ID8 with means from OK and NN estimates. The NN estimator produces a theoretically unbiased estimate of the average value when no cutoff grade is imposed and is a good basis for checking the performance of different estimation methods. Results in Table 17-4 show no evidence of bias in the estimate.

Table 17-4: Comparison of OK, ID and NN Global Mean Values

Zone	ID8 Cu (%)	OK Cu (%)	NN Cu (%)	ID8 Au (g/t)	OK Au (g/t)	NN Au (g/t)
Hypogene	0.50	0.50	0.50	0.161	0.162	0.160
Supergene						
Leached	0.07	0.07	0.09	0.165	0.170	0.181
Mixed	0.35	0.34	0.36	0.174	0.163	0.191
Enriched	0.86	0.81	0.91	0.213	0.199	0.236

17.6.3 Swath Plots

AMEC also checked for local trends in the grade estimates by plotting the results from the OK, ID, and NN estimate results on easting, northing and elevation swath plots. The OK and ID estimates should be smoother than the NN estimate and the ID should be smoother than the OK estimate. The NN estimate should fluctuate around the ID and OK estimates on the plots. The results for the copper grade inside the grade probability shell are presented in Figures 17-9 to 17-11, and they show close tracking between the three estimates and no local trends. The plots for copper values outside of the grade probability shells and all gold results are found in Appendix E.

Figure 17-9: Eastings Swath Plot – Cu (%), Inside Cu Grade Probability Shell

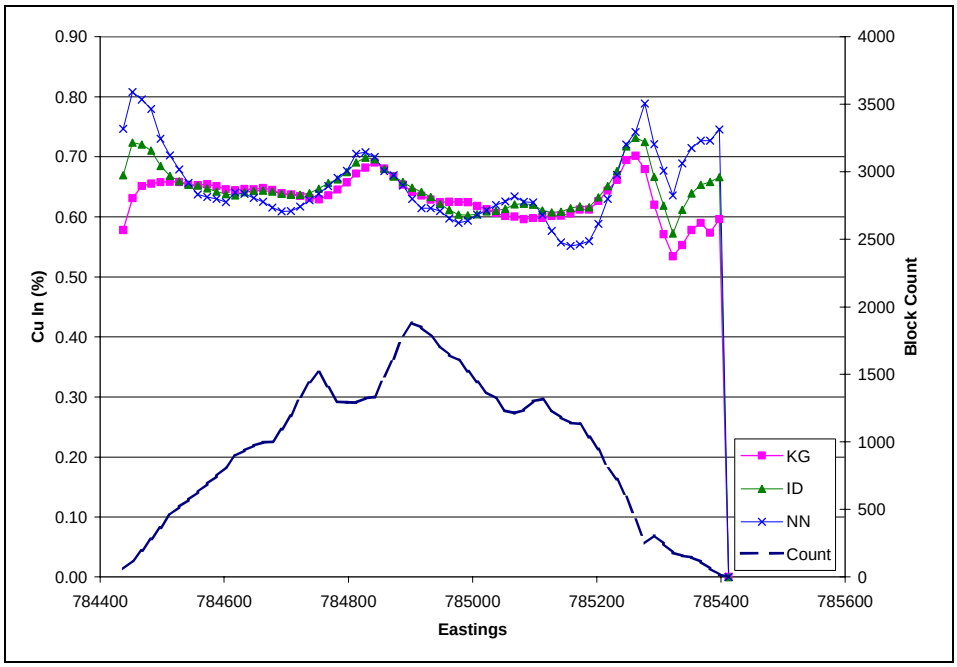


Figure 17-10: Northings Swath Plot – Cu (%), Inside Cu Grade Probability Shell

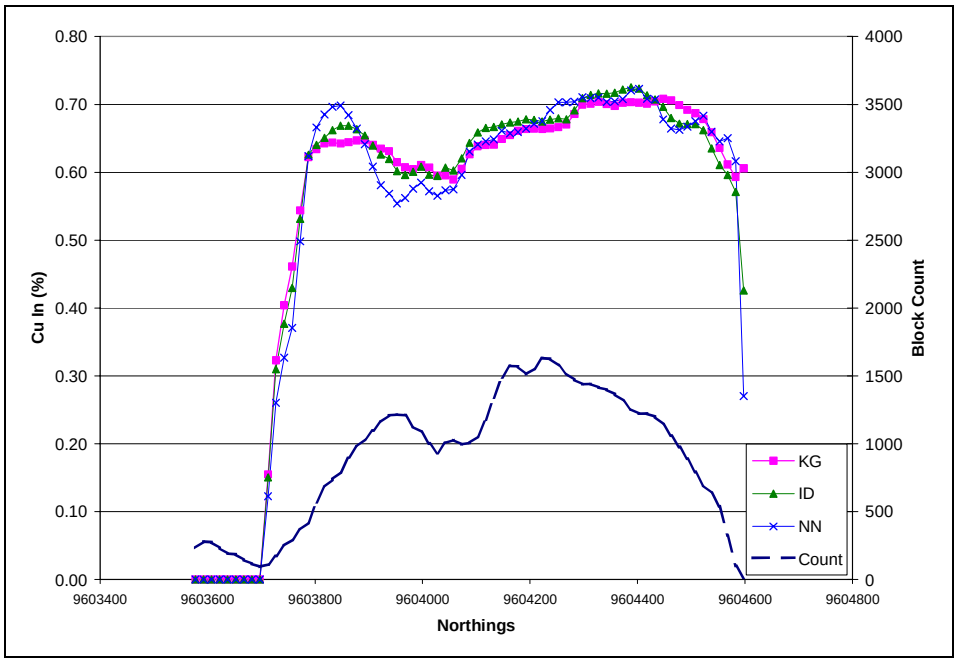
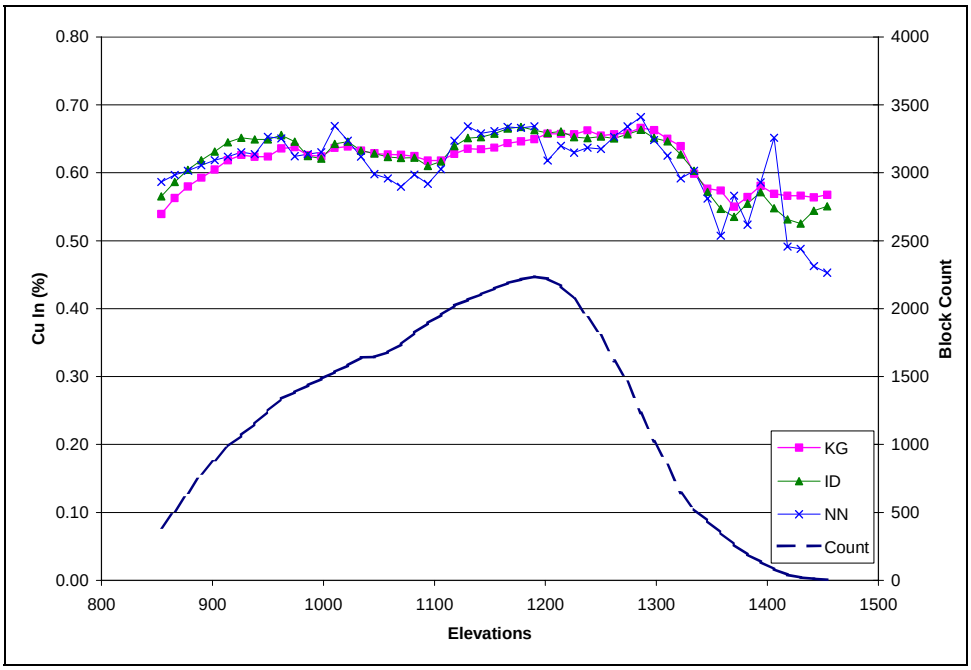


Figure 17-11: Elevations Swath Plot – Cu (%), Inside Cu Grade Probability Shell



17.6.4 Change of Support

The final check on the block model performed by AMEC was to check the model for smoothing through the Discrete Gaussian or Hermitian polynomial change-of-support method described by Journel and Huijbregts (Mining Geostatistics, Academic Press, 1978). The distribution of hypothetical block grades derived by this method is compared to the estimated model grade distribution by means of grade-tonnage curves. The grade-tonnage curves allow comparison of the histograms of the two grade distributions in a format familiar to mining. If the estimation procedure has adequately predicted grades for the selected block size, then the grade-tonnage curves should match fairly closely. If the curves diverge significantly, then there is a problem with the estimated resource.

This method uses the "declustered" distribution of composite grades from a nearest neighbour or polygonal model to predict the distribution of grades in blocks. In this case the blocks used in the model are 15 m x 15 m x 12 m. The unadjusted polygonal model assumes much more selectivity for ore and waste than is actually possible in mining practice, since many sample-sized volumes are averaged together within a block. This means that part of the sample-sized volumes in the block may be ore (above the mining cutoff) and part may be waste. Hence, the distribution of the grade of the blocks is not likely to resemble the distribution of grades from composite

samples derived from the polygonal estimate. The method assumes that the distribution of the blocks will become more symmetric as the variance of the block distribution is reduced, i.e., as the mining blocks become bigger.

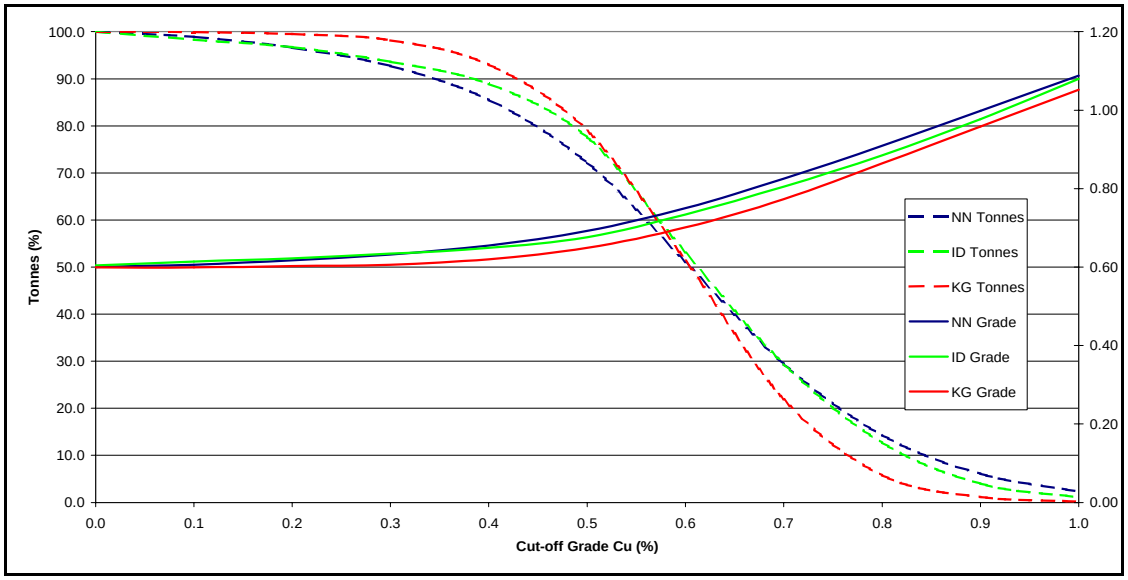
The histogram for the blocks is derived from two calculations:

- the block-to-block variance (sometimes referred to in statistics as the between-block variance), which is calculated by subtracting the average value of the variogram within a block from the variance for composite samples (the sill of the variogram)
- the frequency distribution for the composite grades transformed by means of hermite polynomials (Herco; hermite correction) into a less skewed distribution with the same mean as the declustered grade distribution and with the block-to-block variance of the grades

The distribution of hypothetical block grades derived by the Herco method is then compared to the estimated grade distribution to be validated by means of grade-tonnage curves.

The distribution of calculated 15 m x 15 m x 12 m block grades for copper inside the grade probability shell is shown with dashed lines on the grade-tonnage curves in Figure 17-12. This is the distribution of grades based on 15 m blocks obtained from the change-of-support models. The continuous lines in the figures show the grade-tonnage distribution obtained from the block estimates. The grade-tonnage predictions produced for the model show that grade and tonnage estimates are validated by the change-of-support calculations over the likely range of mining grade cutoff values (0.4% to 0.6% Cu).

Figure 17-12: Change of Support Grade Tonnage Curve, Cu (%)



17.7 Resource Classification and Summary

The mineral resources of the Mirador project were classified using logic consistent with the CIM definitions referred to in National Instrument 43-101. The project mineral resources were classified into one of two categories; Indicated or Inferred Mineral Resources. Review of the model relative to the drill hole data, in sections and in plans, showed good geologic and grade continuity in areas were sample spacing is around 100 m. The current drill hole spacing is nominally 100 m with some areas approaching 75 m. Combined with spatial statistical work and investigation of confidence limits in predicting planned annual production work, AMEC decided that blocks covered by this data spacing may be classified as Indicated Mineral Resources. A two-hole rule was used where blocks containing an estimate resulting from two or more samples from different holes. Locally a second pass utilizing a one-hole rule was necessary to prevent a "striping" effect of isolated Inferred Mineral Resource blocks amongst mostly Indicated Mineral Resource blocks. In the hypogene mineralization two drill holes needed to be within 100 m of the block centre or a single drill hole within 35 m to be classified as Indicated Mineral Resources. Supergene mineralization needed to have two drill holes within 75 m of a block centre or a single drill hole within 35 m.

All interpolated blocks that did not meet the criteria for Indicated Mineral Resources were assigned as Inferred Mineral Resources if they fell within 200 m of a drill hole composite in the hypogene mineralization or 150 m if in the supergene zone.

Table 17-5 contains the results of the resource estimation for the Mirador Deposit as of 23 September 2004. The estimate is made by mineralization type. The resource estimate result for Mirador is being declared using the 0.40 %Cu cutoff. For comparative purposes, additional copper grade cutoffs equal to 0.50. 0.55. 0.60. 0.65 and 0.70 % were also tabulated and they are included in Table 17-6. The resources are reported to a depth of 850 m elevation, which is approximately 500 m below the surface. Preliminary open pit planning work, conducted as part of an ongoing Feasibility Study, have shown potential open pit bottoms to be around 1,000 m below the surface, 150 m above the deepest interpolated grade blocks.

Table 17-5: Mirador Deposit Mineral Resource Summary, 23 September 2004

Zone		Tonnes	Au (g/t)	Cu (%)
0.4 Cu % Cutoff				
Indicated Mineral Resource				
	Mixed	1,300,000	0.23	0.57
	Enriched	6,700,000	0.24	0.99
	MNZD	301,700,000	0.20	0.65
Totals	Indicated Hypogene	301,700,000	0.20	0.65
	Indicated Supergene	8,000,000	0.24	0.92
Inferred Mineral Resource				
	Mixed			
	Enriched	1,200,000	0.25	0.83
	MNZD	313,900,000	0.17	0.56
Totals	Inferred Hypogene	313,900,000	0.17	0.56
	Inferred Supergene	1,200,000	0.25	0.83

Table 17-6: Mirador Deposit Mineral Resource Summary – Comparative Cutoffs, 23 September 2004

	Zone	Tonnes	Au (g/t)	Cu (%)
0.5 Cu % Cutoff (Cu ID)				
Indicated Mineral Resource				
	Mixed	800,000	0.25	0.65
	Enriched	6,600,000	0.24	1.00
	MNZD	254,800,000	0.21	0.68
Totals	Indicated Hypogene	254,800,000	0.21	0.68
	Indicated Supergene	7,400,000	0.24	0.96
Inferred Mineral Resource				
	Mixed			
	Enriched	1,200,000	0.25	0.83
	MNZD	215,300,000	0.18	0.62
Totals	Inferred Hypogene	215,300,000	0.18	0.62
	Inferred Supergene	1,200,000	0.25	0.83
0.6 Cu % Cutoff (Cu ID)				
Indicated Mineral Resource				
	Mixed	500,000	0.28	0.76
	Enriched	6,200,000	0.24	1.03
	MNZD	182,400,000	0.22	0.73
Totals	Indicated Hypogene	182,400,000	0.22	0.73
	Indicated Supergene	6,700,000	0.24	1.01
Inferred Mineral Resource				
	Mixed			
	Enriched	900,000	0.22	0.89
	MNZD	93,300,000	0.20	0.71
Totals	Inferred Hypogene	93,300,000	0.20	0.71
	Inferred Supergene	900,000	0.22	0.89
0.65 Cu % Cutoff (Cu ID)				
Indicated Mineral Resource				
	Mixed	400,000	0.25	0.75
	Enriched	6,000,000	0.25	1.05
	MNZD	140,600,000	0.23	0.77
Totals	Indicated Hypogene	140,600,000	0.23	0.77
	Indicated Supergene	6,400,000	0.25	1.03
Inferred Mineral Resource				
	Mixed			
	Enriched	800,000	0.25	1.00
	MNZD	56,900,000	0.22	0.76
Totals	Inferred Hypogene	56,900,000	0.22	0.76
	Inferred Supergene	800,000	0.25	1.00
0.7 Cu % Cutoff (Cu ID)				
Indicated Mineral Resource				
	Mixed	200,000	0.35	1.05
	Enriched	5,800,000	0.24	1.05
	MNZD	101,600,000	0.24	0.80
Totals	Indicated Hypogene	101,600,000	0.24	0.80
	Indicated Supergene	6,000,000	0.25	1.05
Inferred Mineral Resource				
	Mixed			
	Enriched	800,000	0.25	1.00
	MNZD	40,400,000	0.23	0.79
Totals	Inferred Hypogene	40,400,000	0.23	0.79
	Inferred Supergene			

18.0 OTHER RELEVANT DATA AND INFORMATION

This section is not applicable to the Mirador Project.

19.0 REQUIREMENTS FOR TECHNICAL REPORTS ON PRODUCTION AND DEVELOPMENT PROPERTIES

This section is not applicable to the Mirador Project.

20.0 CONCLUSIONS AND RECOMMENDATIONS

AMEC reviewed the drilling and sampling data from the Mirador Project to obtain a sufficient level of understanding to assess the Mineral Resource estimate for the Mirador Deposit. AMEC's general conclusions from this review are as follows:

- The geology for the Mirador Project is well understood. The Mirador Deposit is considered to be a Cu-Au porphyry system. The copper and gold mineralization encountered at the Mirador Deposit is thought to be a calc-alkaline type porphyry copper system. Supergene zones of enrichment are weakly developed beneath a superficial leach cap. Mineralization at Mirador can be divided into early molybdenum, early copper ± gold, and late copper-gold stages. Chalcopyrite occurs as mainly irregular masses between clasts in the early breccia and as fine disseminations in a halo zone around the breccia. A late stage series of 1 to 2 cm quartz sulphide stingers transect the deposit and are subvertically emplaced. AMEC believes more angled drill holes should have been drilled due to the presence of various geologic features having sub-vertical contacts (e.g., post-mineral dykes, late quartz-sulphide stringers).
- Downhole survey data should be captured for all drill holes in the future.
- The database used to estimate the mineral resources for the Mirador Project consists of samples from 91 core drill holes drilled by Corriente between 2000 and 2004. The data underwent a 5% check of the assay results to original assay certificates and no errors were found.
- Sample security issues need to be addressed by Corriente where sample numbers should be assigned through the use of standard sample books and not include the hole number, sample depth or give unique identifiers to the QA/QC samples. The sample shipping bags should be secured with security tabs and emplaced in a locked box prior to release from the project site.
- A review of the QA/QC database revealed a paucity of QA/QC samples for the 1st, 2nd and 3rd drilling programs, so 5% of the samples were selected for reanalysis. These samples were selected by AMEC and were selected randomly to ensure coverage over time and the deposit area. The samples were analyzed with the benefit of SRMs and duplicates. The reanalysis results indicated that the original results were of the appropriate grade for inclusion in the resource estimation.
- The pulp duplicates indicate that the 100gm pulp size currently being submitted for fire assay analysis for gold is too small and any future samples should be increased to a 250 g pulp.

- The Mirador resource model was developed using industry accepted practices. AMEC validated the model estimates and found them to reasonably estimate the grade and tonnage for the Mirador Deposit.
- The classification applied to the resource estimation at the Mirador Deposit adheres to the guidelines set out in the CIM definitions referred to in National Instrument 43-101 into Indicated and Inferred Mineral Resource categories.

This independent mineral resource estimate and review by AMEC supports the September 2004 Mirador Deposit Mineral Resource statement.

21.0 REFERENCES

Corriente Copper Belt Project, Southeast Ecuador, Order-of-Magnitude Study (Preliminary Assessment Technical Report), David K. Makepeace, P.Eng., June 22, 2001.

Mirador Project, Corriente Copper Belt, Southeast Ecuador, Preliminary Assessment Technical Report, David K. Makepeace, P.Eng., February 12, 2002.

Mirador Project, Corriente Copper Belt, Southeast Ecuador, Order of Magnitude Study, Part 1, Technical Report, David K. Makepeace, P.Eng., James M. Dawson, P.Eng., February 2003.

APPENDIX A ICP ANALYSIS RESULTS

DDH	SAMPLE DESCRIPTION	Au ppm	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd ppm	Co ppm	Cr ppm	Cu ppm	Cu Final %(AMEC)	Fe %	K %	Mg %	Mn ppm	Mo ppm	Na %	Ni ppm	P ppm	Pb ppm	S %	Sb ppm	Sr ppm	Ti %	V ppm	W ppm	Zn ppm	Cu OD %	Cert #	Hg ppm	HG Cert #
M75	2750050010	0.178	1	5.76	8	320	0.2	1	0.01	0.2	0.5	93	365	0.037	3.18	1.78	0.24	168	18	0.04	5	200	190	0.02	2	18	0.16	184	20	17		QU04013369	0.03	QU04020684
M75	2750100020	0.222	4.5	5.37	17	340	0.2	2	0.01	0.2	0.5	110	459	0.046	4.38	2.16	0.33	184	22	0.04	3	130	173	0.02	13	17	0.12	182	10	15		QU04013369	0.03	QU04020684
M75	2750150030	0.226	2.6	7.67	2	360	0.6	2	0.01	0.2	0.5	80	625	0.063	4.42	2.75	0.44	160	34	0.06	3	130	174	0.03	2	20	0.17	168	10	20		QU04013369	0.02	QU04020684
M75	2750200040	0.257	3.1	6.58	2	390	0.5	3	0.01	0.2	0.5	100	499	0.050	4.74	2.49	0.35	135	58	0.07	3	180	156	0.03	2	27	0.16	154	10	16		QU04013369	0.02	QU04020684
M75	2750250050	0.201	2.9	6.5	12	410	0.5	5	0.01	0.2	0.5	120	560	0.056	5.1	2.65	0.39	174	32	0.07	4	180	145	0.03	2	26	0.15	156	0.5	16		QU04013369	0.02	QU04020684
M75	2750300060	0.173	3.7	7.91	2	600	0.6	1	0.01	0.2	0.5	77	622	0.062	5.02	3.23	0.48	193	22	0.09	2	230	264	0.03	2	38	0.16	144	10	14		QU04013369	0.01	QU04020684
M75	2750350070	0.203	5	7.14	2	620	0.5	1	0.01	0.2	0.5	126	566	0.057	4.82	2.8	0.39	132	30	0.1	4	180	146	0.03	5	39	0.15	148	10	12		QU04013369	0.005	QU04020684
M75	2750400080	0.24	5.7	6.07	28	530	0.5	3	0.01	0.2	0.5	150	657	0.066	7.67	2.55	0.37	140	25	0.07	4	570	364	0.05	10	25	0.12	184	10	10		QU04013369	0.01	QU04020684
M75	2750440090	0.199	8.3	6.89	10	3260	0.5	2	0.01	0.2	1	128	695	0.070	6.23	3.05	0.41	180	24	0.11	2	150	104	0.24	2	33	0.15	160	10	11		QU04013369	0.01	QU04020684
M75	2750470100	0.258	10.3	6.62	11	210	0.2	1	0.01	0.2	5	144	5560	0.556	6.1	2.84	0.44	156	18	0.08	2	120	33	2.42	2	30	0.13	161	0.5	24		QU04013369	0.01	QU04020684
M75	2750500110	0.239	4.5	6.45	12	260	0.2	1	0.01	0.2	3	140	2750	0.275	4.91	3.16	0.37	129	29	0.11	4	190	68	1.04	2	53	0.15	164	10	18		QU04013369	0.01	QU04020684
M75	2750530120	0.291	5.3	7.16	10	280	0.5	1	0.01	0.2	1	86	2940	0.294	4.93	3.4	0.38	141	13	0.11	2	130	92	0.92	7	62	0.15	172	10	12		QU04013369	0.02	QU04020684
M75	2750530128	0.28	5.7	7	18	330	0.5	2	0.01	0.2	2	127	2880	0.288	4.9	3.34	0.37	136	14	0.11	2	130	91	0.89	7	61	0.15	168	0.5	13		QU04013369	0.02	QU04020684
M75	2750560130	0.277	4	5.16	7	880	0.2	1	0.01	0.2	1	75	1315	0.132	5.21	2.76	0.27	140	9	0.09	1	80	24	0.55	2	54	0.12	152	10	12		QU04013369	0.01	QU04020684
M75	2750590140	0.273	4.9	6.4	14	220	0.2	2	0.02	0.2	12	170	>10000	1.05	5.1	3.61	0.35	168	11	0.11	6	100	22	4.39	2	62	0.14	186	10	27	1.05	QU04013369	0.01	QU04020684
M75	2755590140	0.145	1.3	7.85	2	150	0.8	1	0.96	0.5	16	61	3590	0.359	3.64	3.97	0.77	657	90	1.2	2	490	37	2.22	2	176	0.13	100	0.5	105		QU04013369	0.04	QU04020684
M75	2750620150	0.205	3.4	6.16	8	240	0.2	1	0.02	0.5	12	121	>10000	1.01	5.13	3.77	0.35	151	21	0.13	5	60	27	5.46	2	78	0.13	157	10	41	1.01	QU04013369	0.01	QU04020684
M75	2750650160	0.196	3.2	6.32	5	270	0.5	1	0.02	0.9	10	112	8040	0.804	5.3	3.82	0.49	222	26	0.13	4	90	36	5.57	2	72	0.14	150	0.5	90		QU04013369	0.02	QU04020684
M75	2750680170	0.185	3.5	6.74	13	290	0.5	1	0.02	1.5	9	131	>10000	1.03	5.41	3.77	0.57	320	27	0.13	4	140	42	5.86	7	69	0.12	152	10	209	1.03	QU04013369	0.06	QU04020684
M75	2750710180	0.31	5	5.98	15	290	0.2	1	0.02	0.8	9	101	9570	0.957	4.84	4.4	0.62	465	18	0.19	1	160	31	4.93	2	106	0.13	175	10	97		QU04013369	0.02	QU04020684
M75	2750710189	0.295	4.3	4.9	11	240	0.2	1	0.02	0.5	9	78	8180	0.818	3.81	3.71	0.52	392	16	0.15	3	130	25	3.9	2	90	0.11	146	0.5	77		QU04013369	0.02	QU04020684
M75	2750740190	0.266	4.5	6.08	2	230	0.2	1	0.05	0.9	9	132	8010	0.801	4.5	4.08	0.63	512	42	0.23	3	140	29	4.51	5	96	0.13	144	0.5	132		QU04013369	0.04	QU04020684
M75	2750770200	0.226	4.5	6.45	7	290	0.6	2	0.08	0.8	9	138	6890	0.689	4.49	4.57	0.71	593	19	0.24	2	240	30	4.46	2	112	0.13	142	10	146		QU04013369	0.04	QU04020684
M75	2750800210	0.277	5.2	6.48	5	260	0.6	1	0.11	0.7	9	124	7410	0.741	4.2	4.51	0.71	794	14	0.41	4	360	25	4.15	2	122	0.15	136	0.5	184		QU04013369	0.05	QU04020684
M75	2750830220	0.303	4.3	5.74	5	170	0.5	1	0.1	0.2	11	130	7490	0.749	4.65	3.99	0.7	643	12	0.34	4	310	20	4.64	2	108	0.14	150	0.5	64		QU04013369	0.02	QU04020684
M75	2750860230	0.205	4.4	6.89	5	210	0.6	3	0.1	0.2	13	135	7590	0.759	4.92	4.2	0.63	422	10	0.13	2	370	10	5	2	96	0.13	146	0.5	43		QU04013369	0.02	QU04020684
M75	2750890240	0.187	4.5	5.41	9	240	0.6	1	0.05	0.2	12	172	8570	0.857	4.51	3	0.5	410	8	0.06	5	140	11	4.55	5	43	0.1	153	0.5	158		QU04013369	0.03	QU04020684
M75	2750920250	0.201	3.8	6.8	10	230	0.7	3	0.1	0.2	12	128	6860	0.686	5.62	3.48	0.76	755	26	0.13	6	300	18	5.3	9	74	0.13	149	0.5	95		QU04013369	0.03	QU04020684
M75	2750920258	0.204	3.3	6.02	8	170	0.7	1	0.08	0.2	14	142	6630	0.663	4.97	3.41	0.66	647	15	0.11	5	250	17	4.8	5	63	0.14	150	0.5	107		QU04013369	0.03	QU04020684
M75	2750940260	0.182	1.6	7.59	8	240	0.9	1	0.21	0.2	11	118	6530	0.653	3.8	3.94	1.18	861	10	0.98	5	420	14	2.01	7	176	0.17	152	0.5	106		QU04013369	0.05	QU04020684
M75	2750990270	0.002	0.2	9.33	2	1020	1	1	2.52	0.2	8	27	192	0.019	3.42	3.2	1.09	1340	1	2.8	3	970	6	0.05	6	398	0.23	91	10	95		QU04013369	0.005	QU04020684
M75	2751040280	0.002	0.2	8.89	8	1060	1	1	2.06	0.2	7	25	61	0.006	3.48	2.72	1.07	1615	1	3.26	2	790	5	0.06	8	422	0.21	85	0.5	93		QU04013369	0.01	QU04020684
M75	2751090290	0.002	0.2	9.32	2	1100	1.1	1	1.06	0.2	8	33	12	0.001	3.64	2.77	1.12	1435	0.5	3.55	3	830	4	0.01	2	469	0.21	91	10	108		QU04013369	0.01	QU04020684
M75	2751140300	0.012	0.2	9.07	2	1000	0.8	1	1.76	0.2	7	30	104	0.010	3.14	2.48	1.06	1195	0.5	4.39	0.5	840	8	0.11	2	393	0.23	87	10	132		QU04013369	0.005	QU04020684
M75	2756140300	0.271	1.9	7.08	21	240	0.7	1	0.77	1	12	120	7770	0.777	3.2	4.52	0.72	553	56	0.8	7	440	65	2.95	16	172	0.12	114	0.5	157		QU04013369	0.06	QU04020684
M75	2751190310	0.002	0.2	9.69	2	1020	1	1	2.94	0.2	6	34	50	0.005	3.34	2.86	1.26	1390	0.5	3.18	3	910	8	0.05	5	473	0.23	89	10	91		QU04013369	0.005	QU04020684
M75	2751240320	0.002	0.2	8.43	10	1020	1	1	2.21	0.2	7	43	34	0.003	2.96	2.78	0.88	1090	0.5	3.14	1	760	5	0.02	2	443	0.2	80	10	65		QU04013369	0.01	QU04020684
M75	2751290330	0.002	0.2	9.65	2	1090	0.9	1	2.97	0.2	5	44	17	0.002	3.15	2.65	1.14	1215	0.5	3.19	1	810	7	0.01	2	555	0.21	79	0.5	66		QU04013369	0.005	QU04020684
M75	2751340340	0.008	0.2	9.06	2	1720	1	1	3.17	0.2	5	38	29	0.003	2.95	2.9	0.95	1100	0.5	2.42	1	790	6	0.03	2	494	0.22	81	0.5	62		QU04013369	0.01	QU04020684
M75	2751390350	0.006	0.2	9.23	2	940	1	1	3.13	0.2	6	27	29	0.003	3.09	3.23	0.98	1155	0.5	2.22	0.5	820	5	0.01	6	446	0.21	86	0.5	61		QU04013369	0.01	QU04020684
M75	2751440360	0.031	0.2	8.94	2	1040	0.9	1	2.83	0.2	5	32	417	0.042	3.25	3.29	0.86	1290	7	2.37	1	810	5	0.16	5	400	0.22	93	0.5	60		QU04013369	0.02	QU04020684
M75	2751470370	0.205	2.8	5.89	18	240	0.5	1	1.04	0.2	10	136	5680	0.568	3.92	3.27	0.49	620	36	0.09	3	380	75	3.65	14	52	0.1	156	0.5	108		QU04013369	0.07	QU04020684
M75	2751470379	0.206	2.7	5.43	26	490	0.5	1	0.96	0.5	10	132	5370	0.537	3.75	3.02	0.46	588	34	0.08	3	370	72	3.53	17	48	0.09	142	0.5	95		QU04013369	0.07	QU04020684
M75	2751500380	0.084	3.5	6.39	162	490	0.6	1	0.99	3.5	8	170	4330	0.433	3.76	3.23	0.46	502	10	0.06	3	440	370	3.9	25	39	0.11	152	10	601		QU04013369	0.25	QU04020684
M75	2751530390	0.06	1.6	7.44	64	190	0.7	1	1.23	0.5	8	134	6230	0.623	3.52	4.29	0.61	553	43	0.13	4	470	16	3.57	14	78	0.13	160	10	102		QU04013369	0.07	QU04020684
M75	2751560400	0.178	1.2	6.81	2	210	0.6	1	0.98	0.2	9	112	5490	0.549	3.53	4.2	0.77	474	8	0.75	2	390	9	3.18	6	162	0.13	166	10	35		QU04013369	0.02	QU04020684
M75	2751590410	0.142	1.6	7.25	2	140	0.7	1	1.12	0.6	10	86	7800	0.780	4.14	4.66	0.64	452	15	0.23	4	480	13	4.22	2	103	0.11	152	10	176		QU04013369	0.04	QU04020684
M75	2751620420	0.038	0.9	6.62	6	160	0.6	1	0.8	0.2	6	97	3660	0.366	3.59	3.64	0.57	318	11	0.14	4	460	11	3.7	2	67	0.11	130	10	39		QU04013369	0.03	QU04020684
M75	2751650430	0.022	0.7	7.7	7	480	0.8	1	2.01	0.2	7	38	2120	0.212	3.57	3.42	0.89	640	5	1.04	1	620	10	2.41	6	160	0.16	110	10	85		QU04013369	0.03	QU04020684
M75	2751680440	0.002	0.2	9.67	2	790	0.9	1	3.02	0.2	6	14	54	0.005	3.35	3.3	1.23	910	0.5	2.3	1	840	5	0.05	2	261	0.24	98	0.5	52		QU04013369	0.02	QU04020684
M75	2751680449	0.002	0.2	9.34	7	780	0.8	1	2.97	0.2	6	13	48	0.005	3.23	3.2	1.2	893	0.5	2.2	3	850	4	0.03	5	250	0.23	95	10	50		QU04013369	0.02	QU04020684
M75	2751710450	0.002	0.2	9.35	7	1980	0.9	1	3.1	0.2	6	22	16	0.002	3.05	2.96	1.14	964	1	2.71	3	840	4	0.05	5	339	0.21	91	0.5	44		QU04013369	0.01	QU04020684
M75	2751740460	0.017	0.2	9.48	2	1100	0.9	1	2.92	0.2	6	29	458	0.046	3.11	3.12	1.09	837	1	2.79	3	870	8	0.48	2	402	0.2	89	0.5	42		QU04013369	0.01	QU04020684
M75	2751770470	0.057	0.2	8.15	2	200	0.8	1	1.53	0.2	8	99	2560	0.256	2.94	4.5	0.69	372	6	1.55	3	700	14	2.57	2	281	0.12	104	10	72		QU04013369	0.04	QU04020684
M75	2751800480	0.087	0.7	6.13	2	190	0.5	1	0.72	1.2	9	91	3630	0.363	3.27	4.94	0.48	232	18	0.37	3	320	14	3.35	5	138	0.09	146	10	286		QU04013369	0.08	QU04020684

DDH	SAMPLE DESCRIPTION	Au ppm	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd ppm	Co ppm	Cr ppm	Cu ppm	Cu Final %(AMEC)	Fe %	K %	Mg %	Mn ppm	Mo ppm	Na %	Ni ppm	P ppm	Pb ppm	S %	Sb ppm	Sr ppm	Ti %	V ppm	W ppm	Zn ppm	Cu OD %	Cert #	Hg ppm	HG Cert #
M75	2751830490	0.041	0.7	6.77	2	180	0.5	1	0.45	0.2	7	102	2920	0.292	2.93	4.93	0.54	219	27	0.32	3	400	15	2.85	2	150	0.09	142	0.5	52		QU04013369	0.03	QU04020684
M75	2751860500	0.053	0.8	5.83	2	190	0.5	1	0.44	0.2	10	121	3690	0.369	3.84	4.39	0.42	144	29	0.15	3	390	9	3.96	2	103	0.09	157	10	15		QU04013369	0.01	QU04020684
M75	2756860500	0.27	1.9	7.24	23	170	0.7	1	0.78	1	12	110	7780	0.778	3.29	4.57	0.73	552	53	0.81	6	460	68	3.04	15	177	0.13	114	10	154		QU04013369	0.05	QU04020684
M75	2751890510	0.053	0.5	6.67	2	210	0.6	1	0.67	0.2	7	88	3030	0.303	2.87	4.47	0.49	188	13	0.37	3	470	5	2.9	2	126	0.09	112	10	14		QU04013369	0.01	QU04020684
M75	2751920520	0.036	0.6	7.72	2	200	0.7	1	1	0.2	9	104	2290	0.229	3.13	4.68	0.7	279	10	0.74	1	660	8	3.02	6	152	0.1	93	10	25		QU04013369	0.01	QU04020684
M75	2751950530	0.034	0.2	7.44	2	210	0.6	1	0.98	0.2	6	93	2250	0.225	2.96	4.94	0.56	240	18	0.69	2	550	7	2.69	2	157	0.1	98	10	14		QU04013369	0.03	QU04020684
M75	2751980540	0.034	0.2	6.99	6	160	0.6	1	0.79	0.2	7	78	2240	0.224	2.9	3.86	0.51	170	11	0.44	3	520	5	2.86	2	92	0.09	92	10	10		QU04013369	0.03	QU04020684
M75	2752010550	0.032	0.6	7.37	2	190	0.7	1	0.73	0.2	9	95	3240	0.324	3.89	4.05	0.46	150	57	0.18	2	560	2	4.14	2	61	0.09	100	10	5		QU04013369	0.02	QU04020684
M75	2752010558	0.029	0.5	7.38	2	160	0.7	1	0.7	0.2	7	83	2880	0.288	3.23	4.02	0.47	142	67	0.19	2	570	4	3.44	2	64	0.09	97	10	5		QU04013369	0.02	QU04020684
M75	2752040560	0.047	0.6	6.83	11	160	0.6	1	0.55	0.2	10	98	1910	0.191	4.38	3.49	0.42	138	20	0.1	3	460	4	4.61	2	42	0.09	116	20	6		QU04013369	0.02	QU04020684
M75	2752070570	0.063	0.5	5.32	2	160	0.2	1	0.87	0.2	7	100	2850	0.285	3.43	3.77	0.52	230	16	0.14	3	300	4	3.29	2	86	0.08	126	10	13		QU04013369	0.02	QU04020684
M75	2752100580	0.149	0.9	6.79	2	160	0.6	1	0.8	0.2	11	121	5770	0.577	3.73	4.12	0.56	189	48	0.16	2	440	5	3.66	2	75	0.1	116	10	12		QU04013369	0.02	QU04020684
M75	2752130590	0.113	0.7	6.67	2	210	0.6	1	0.49	0.2	12	98	4030	0.403	4.3	3.71	0.46	102	10	0.09	4	420	6	4.42	2	51	0.11	178	10	3		QU04013369	0.02	QU04020684
M75	2752160600	0.155	1	6.5	2	180	0.6	1	0.77	0.2	11	104	6810	0.681	3.06	4.67	0.64	176	7	0.19	4	420	4	2.9	2	101	0.1	104	10	13		QU04013369	0.02	QU04020684
M75	2752190610	0.069	0.5	7.17	6	290	0.6	1	0.31	0.2	17	89	2680	0.268	4.05	3.94	0.51	84	9	0.13	2	480	1	4.24	5	68	0.1	136	10	5		QU04013369	0.01	QU04020684
M75	2752220620	0.066	0.2	8.11	2	230	0.7	1	0.82	0.2	10	59	2670	0.267	2.89	5	0.58	154	20	0.59	1	600	6	2.91	2	146	0.09	83	10	9		QU04013369	0.02	QU04020684
M75	2752250630	0.065	0.2	7.44	6	200	0.6	1	0.84	0.2	13	89	1905	0.191	3.11	4.58	0.57	182	32	0.7	0.5	580	8	2.88	2	160	0.09	91	10	11		QU04013369	0.02	QU04020684
M75	2752280640	0.069	0.2	7.74	2	570	0.8	1	1.23	0.2	8	58	1505	0.151	2.99	3.96	0.79	223	4	1.44	2	670	10	2.31	2	245	0.1	78	0.5	21		QU04013369	0.02	QU04020684
M75	2752310650	0.075	0.2	7.88	2	540	0.8	1	1.71	0.2	7	95	1805	0.181	3.19	3.74	0.76	249	10	1.28	2	660	6	2.42	2	287	0.12	87	0.5	21		QU04013369	0.03	QU04020684
M75	2755310650	0.162	1.2	7.85	9	250	0.8	1	0.98	0.2	17	76	3820	0.382	3.64	3.91	0.79	671	114	1.26	5	480	42	2.27	2	172	0.14	100	0.5	111		QU04013369	0.04	QU04020684
M75	2752340660	0.138	1	5.97	38	150	0.5	1	2.41	0.2	13	110	6060	0.606	3.96	2.91	0.37	56	60	0.06	5	410	5	6.33	6	309	0.08	108	10	15		QU04013369	0.02	QU04020684
M75	2752370670	0.071	0.2	5.92	7	140	0.5	1	2.34	0.2	18	146	3370	0.337	4.17	2.83	0.29	65	28	0.06	4	450	3	6.37	2	306	0.07	90	10	1		QU04013369	0.01	QU04020684
M75	2752400680	0.135	1.2	5.92	196	130	0.2	1	2.74	0.2	10	104	6780	0.678	3.03	3.71	0.45	118	309	0.11	3	440	3	5.02	12	333	0.08	104	0.5	56		QU04013369	0.06	QU04020684
M75	2752430690	0.268	0.7	6.09	18	310	0.5	1	2.24	0.2	10	114	7620	0.762	2.94	4.04	0.61	144	11	0.28	4	380	5	4.15	2	238	0.09	97	0.5	20		QU04013369	0.03	QU04020684
M75	2752460700	0.225	2	6.06	39	130	0.5	1	2.51	0.2	8	162	7480	0.748	3.32	3.25	0.38	104	30	0.08	5	460	3	5.5	2	350	0.09	90	0.5	16		QU04013369	0.03	QU04020684
M75	2752490710	0.162	1.2	5.1	16	120	0.2	1	2.35	0.2	8	129	5420	0.542	2.72	3.1	0.35	102	12	0.08	5	310	3	4.59	2	335	0.07	81	0.5	4		QU04013369	0.02	QU04020684
M75	2752520720	0.263	1.4	6.17	12	90	0.6	1	3.24	0.2	10	117	5700	0.570	2.62	3.28	0.4	86	27	0.08	10	540	4	5.34	2	412	0.09	81	0.5	14		QU04013369	0.02	QU04020684
M75	2752520728	0.195	1.4	6.62	11	120	0.6	1	3.3	0.2	8	79	6060	0.606	2.57	3.41	0.42	77	27	0.09	4	560	2	5.39	2	419	0.09	78	0.5	10		QU04013369	0.02	QU04020684
M75	2752550730	0.213	3	6.72	21	130	0.6	1	2.36	0.2	10	124	7910	0.791	3.44	3.19	0.44	83	31	0.07	5	540	4	5.62	2	429	0.09	94	0.5	12		QU04013369	0.03	QU04020684
M75	2752580740	0.291	1.6	7.07	8	100	0.7	2	3.5	0.2	10	65	7040	0.704	2.78	4.04	0.89	143	188	0.71	3	500	5	5.16	2	342	0.13	104	0.5	17		QU04013369	0.03	QU04020684
M75	2752610750	0.225	1.1	6.71	52	90	0.5	1	2.72	0.2	10	145	8300	0.830	3.48	3.68	0.66	118	25	0.15	5	420	10	5.59	2	297	0.1	104	0.5	30		QU04013369	0.04	QU04020684
M75	2752640760	0.184	0.5	6.73	11	170	0.6	1	3	0.2	11	82	6210	0.621	2.96	3.89	0.46	76	17	0.12	4	550	12	5.54	2	343	0.08	90	0.5	21		QU04013369	0.03	QU04020684
M75	2752670770	0.281	1.6	6.07	26	90	0.5	3	2.34	0.2	9	106	6060	0.606	3.13	3.98	0.46	107	19	0.1	4	460	8	5.1	2	361	0.09	100	0.5	15		QU04013369	0.04	QU04020684
M75	2752700780	0.311	1.9	6.22	46	90	0.5	1	2.59	0.2	10	136	7290	0.729	3.09	4.38	0.7	126	40	0.14	5	380	7	5.23	2	309	0.09	96	0.5	30		QU04013369	0.07	QU04020684
M75	2752700789	0.209	1.8	6.03	48	130	0.5	1	2.52	0.2	10	146	7330	0.733	2.98	4.38	0.69	124	38	0.14	5	360	6	5.06	2	308	0.09	97	0.5	32		QU04013369	0.07	QU04020684
M75	2752730790	0.278	2.5	5.71	2	90	0.5	2	2.34	0.2	8	118	8250	0.825	2.58	3.35	0.61	87	47	0.07	7	410	5	4.72	2	314	0.09	96	0.5	9		QU04013369	0.04	QU04020684
M75	2752760800	0.254	1.7	5.69	8	150	0.5	4	2.63	0.2	10	105	5060	0.506	3.13	3.22	0.57	110	58	0.19	14	410	4	5.09	2	338	0.08	90	0.5	20		QU04013369	0.02	QU04020684
M75	2752790810	0.073	0.2	8.36	2	140	0.9	2	2.43	0.2	6	72	1245	0.125	2.87	3.52	0.94	223	8	1.9	4	750	4	2.68	2	375	0.1	70	0.5	20		QU04013369	0.01	QU04020684
M75	2752820820	0.132	0.8	8	2	140	0.7	1	2.91	0.2	7	85	3580	0.358	2.75	4.05	0.88	172	34	1.09	4	670	4	3.68	2	380	0.11	89	0.5	15		QU04013369	0.02	QU04020684
M75	2752850830	0.187	1.7	6.42	31	150	0.5	1	2.45	0.2	12	90	6140	0.614	3.38	3.6	0.64	96	13	0.12	5	410	3	5.5	2	284	0.1	110	0.5	16		QU04013369	0.02	QU04020684
M75	2752880840	0.214	0.5	5.12	2	120	0.2	1	2.35	0.2	8	104	4510	0.451	2.47	2.8	0.55	97	6	0.2	4	360	4	4.13	2	218	0.08	77	0.5	2		QU04013369	0.02	QU04020684
M75	2752910850	0.13	1	6.64	2	110	0.6	1	3	0.2	10	88	6230	0.623	2.5	4.32	0.74	132	6	0.42	5	460	4	4.44	2	430	0.11	116	0.5	12		QU04013369	0.02	QU04020684
M75	2755910850	0.154	1.3	7.7	7	190	0.8	1	0.98	0.2	17	70	3590	0.359	3.58	3.69	0.78	674	99	1.24	4	480	40	2.22	2	170	0.14	96	0.5	98		QU04013369	0.04	QU04020684
M75	2752940860	0.171	1.1	5.88	8	120	0.5	1	2.61	0.2	10	126	6490	0.649	2.34	3.74	0.6	112	17	0.29	6	380	4	4.21	2	309	0.1	93	0.5	11		QU04013369	0.04	QU04020684
M75	2752970870	0.243	0.9	6.31	30	160	0.5	1	3	0.2	13	138	5020	0.502	3.05	3.08	0.44	63	42	0.08	6	460	7	5.77	2	352	0.09	99	0.5	8		QU04013369	0.08	QU04020684
M75	2752970879	0.209	1	5.9	35	130	0.5	1	2.76	0.2	16	138	5160	0.516	3.04	3.1	0.41	59	24	0.08	6	420	6	5.57	2	330	0.09	101	10	12		QU04013369	0.07	QU04020684
M75	2753000880	0.226	1.3	5.9	41	110	0.5	2	2.45	0.2	10	118	4870	0.487	2.72	3.33	0.48	67	19	0.09	5	450	8	4.99	2	299	0.08	90	0.5	20		QU04013369	0.19	QU04020684
M77	2770050010	0.214	0.2	6.83	14	330	0.5	3	0.02	0.2	1	142	397	0.040	5.19	1.86	0.24	68	33	0.07	5	1100	72	0.02	2	35	0.1	151	0.5	14		QU04014264	0.02	QU04020685
M77	2770100020	0.33	0.6	6.8	2	340	0.5	5	0.01	0.2	0.5	107	372	0.037	3.88	1.95	0.28	65	54	0.07	3	380	65	0.02	2	27	0.11	150	0.5	11		QU04014264	0.01	QU04020685
M77	2770150030	0.132	1.7	7.69	2	800	0.6	4	0.01	0.2	0.5	82	634	0.063	4.05	2.91	0.23	55	43	0.18	5	330	65	0.02	2	87	0.15	120	0.5	11		QU04014264	0.005	QU04020685
M77	2770200040	0.217	1.5	7.9	7	890	0.5	3	0.01	0.2	1	71	513	0.051	4.36	3.14	0.23	55	42	0.19	4	340	59	0.02	2	95	0.14	124	0.5	11		QU04014264	0.005	QU04020685
M77	2770250050	0.365	2.3	8.81	2	1040	0.5	4	0.01	0.2	1	81	702	0.070	4.64	3.77	0.27	54	58	0.2	4	410	32	0.02	2	110	0.17	136	0.5	12		QU04014264	0.005	QU04020685
M77	2770250058	0.368	2.5	8.93	7	1040	0.5	3	0.01	0.2	0.5	58	698	0.070	4.67	3.74	0.27	59	57	0.2	3	400	34	0.02	2	112	0.17	135	0.5	12		QU04014264	0.005	QU04020685
M77	2770300060	0.294	5.7	8.53	2	1120	0.5	3	0.01	0.2	0.5	71	731	0.073	4.44	3.99	0.34	68	44	0.2	2	590	62	0.03	2	108	0.14	108	0.5	13		QU04014264	0.01	QU04020685
M77	2770330070	0.258	5	8.52	9	1860	0.7	3	0.02	0.2	1	53	810	0.081	4.4	4.39	0.43	194	76	0.27	2	1450	98	0.04	2	146	0.14	114	0.5	26		QU04014264	0.01	QU04020685

DDH	SAMPLE DESCRIPTION	Au ppm	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd ppm	Co ppm	Cr ppm	Cu ppm	Cu Final %(AMEC)	Fe %	K %	Mg %	Mn ppm	Mo ppm	Na %	Ni ppm	P ppm	Pb ppm	S %	Sb ppm	Sr ppm	Ti %	V ppm	W ppm	Zn ppm	Cu OD %	Hg Cert #	Hg ppm	HG Cert #
M77	2770360080	0.167	2	11.2	9	430	1.2	4	0.02	0.2	7	27	4010	0.401	3.01	3.6	0.25	126	57	0.17	3	350	22	2.16	2	142	0.2	86	0.5	28		QU04014264	0.005	QU04020685
M77	2770390090	0.213	1.7	6.8	7	280	0.7	3	0.03	0.2	10	113	8090	0.809	3.5	4.27	0.63	249	62	0.34	5	670	26	3.51	2	127	0.12	91	0.5	53		QU04014264	0.005	QU04020685
M77	2770420100	0.155	1.3	7.45	5	260	1	3	0.05	0.2	10	92	4740	0.474	3.37	4.47	0.86	290	24	0.52	5	1080	28	3.21	2	146	0.12	91	0.5	94		QU04014264	0.005	QU04020685
M77	2770450110	0.222	2.1	5.45	5	270	0.5	3	0.04	0.2	8	148	5810	0.581	3.86	3.75	0.62	260	32	0.26	3	610	30	3.72	2	103	0.1	122	0.5	86		QU04014264	0.005	QU04020685
M77	2775450110	0.154	1.1	7.64	10	500	0.8	3	0.99	0.2	16	69	3550	0.355	3.74	3.89	0.79	689	98	1.21	4	490	44	2.18	2	174	0.14	98	0.5	107		QU04014264	0.04	QU04020685
M77	2770480120	0.177	1.7	6.6	5	270	0.7	3	0.16	0.2	8	142	3790	0.379	4.24	4.18	0.86	272	37	0.69	3	480	33	4.21	2	141	0.12	111	10	77		QU04014264	0.005	QU04020685
M77	2770510130	0.154	1.6	6.4	2	300	0.7	3	0.21	0.2	9	120	3500	0.350	4.01	3.94	0.81	268	17	0.8	2	580	26	3.83	2	142	0.12	115	0.5	53		QU04014264	0.005	QU04020685
M77	2770540140	0.195	1.8	6.47	2	310	0.7	3	0.21	0.2	8	149	3740	0.374	4.43	3.92	0.87	249	26	0.73	4	560	20	4.27	2	142	0.12	104	0.5	49		QU04014264	0.005	QU04020685
M77	2770570150	0.193	1.6	6.49	8	340	0.7	3	0.33	0.2	7	87	3400	0.340	3.79	3.89	0.87	288	22	0.81	3	550	17	3.3	2	148	0.13	120	0.5	58		QU04014264	0.005	QU04020685
M77	2770570159	0.177	1.8	6.58	5	280	0.7	3	0.34	0.2	7	85	3440	0.344	3.95	3.91	0.88	291	23	0.83	2	550	15	3.45	2	152	0.13	122	10	61		QU04014264	0.005	QU04020685
M77	2770600160	0.158	1.9	6.23	9	240	0.7	3	0.21	0.2	10	79	3800	0.380	4.47	3.68	0.92	309	19	0.59	2	430	18	4.25	2	124	0.12	152	0.5	37		QU04014264	0.005	QU04020685
M77	2770630170	0.13	2	7.35	7	190	0.9	3	0.53	0.2	9	112	3520	0.352	4.51	4.22	1.08	248	26	1.09	3	520	16	4.06	2	197	0.14	114	0.5	29		QU04014264	0.005	QU04020685
M77	2770660180	0.129	2.1	7.3	6	170	0.8	5	0.59	0.5	10	124	3690	0.369	5.14	3.97	1.02	271	19	0.89	3	570	40	4.95	2	162	0.13	135	0.5	89		QU04014264	0.005	QU04020685
M77	2770690190	0.135	2.1	6.98	9	180	0.8	4	0.77	1	8	120	3330	0.333	4.89	3.62	0.93	508	26	0.94	3	530	69	4.64	2	151	0.13	118	0.5	182		QU04014264	0.005	QU04020685
M77	2770720200	0.12	1.8	8.02	12	170	0.8	3	1.1	0.2	8	98	2910	0.291	4.83	4.02	0.99	543	24	1.18	3	730	42	4.6	2	189	0.15	117	0.5	77		QU04014264	0.005	QU04020685
M77	2770750210	0.42	2.4	6.68	12	170	0.7	3	0.75	0.2	13	132	4850	0.485	6.51	3.63	1.08	498	26	0.71	7	520	38	6.13	2	114	0.14	202	10	106		QU04014264	0.005	QU04020685
M77	2770780220	0.122	2	7.33	8	140	0.8	4	1.27	0.2	9	126	4290	0.429	5.03	3.78	0.88	401	55	0.92	3	680	26	5.08	2	187	0.12	128	0.5	50		QU04014264	0.005	QU04020685
M77	2770810230	0.103	1.2	7.47	22	150	0.8	5	1.52	1	9	112	2270	0.227	4.84	2.93	0.93	400	16	1.28	7	680	16	4.96	2	263	0.16	142	0.5	229		QU04014264	0.01	QU04020685
M77	2770840240	0.029	0.2	8.74	66	120	0.9	4	2.75	0.2	8	55	401	0.040	3.91	1.59	1.28	317	1	2.34	3	900	17	4.27	2	578	0.17	105	0.5	85		QU04014264	0.005	QU04020685
M77	2770870250	0.019	0.2	9.37	77	110	1	4	3.1	0.2	8	79	483	0.048	3.99	1.7	1.4	305	2	2.38	3	960	14	4.34	2	598	0.19	110	0.5	44		QU04014264	0.005	QU04020685
M77	2770870258	0.02	0.2	9.22	72	190	1	2	3.01	0.2	8	64	478	0.048	3.99	1.7	1.36	287	2	2.34	4	950	12	4.37	2	593	0.19	109	0.5	42		QU04014264	0.005	QU04020685
M77	2770900260	0.012	0.2	9.92	46	240	1	3	3.39	0.2	9	51	433	0.043	4.46	2	1.36	448	1	2.3	2	1010	12	4.92	2	578	0.18	112	0.5	56		QU04014264	0.005	QU04020685
M77	2770930270	0.037	0.5	8.72	8	150	0.7	4	1.12	0.2	9	86	1570	0.157	4.31	3.52	0.87	399	29	0.69	3	840	8	3.83	2	102	0.12	116	0.5	22		QU04014264	0.005	QU04020685
M77	2770960280	0.006	0.2	9.49	6	810	0.9	3	3.04	0.2	7	18	72	0.007	3.36	2.95	1.35	1065	0.5	2.6	3	870	7	0.18	2	331	0.24	95	0.5	64		QU04014264	0.005	QU04020685
M77	2770990290	0.062	1.2	7.32	18	300	0.8	4	0.49	0.2	9	100	3870	0.387	4.72	3.32	0.81	157	30	0.13	3	640	17	4.85	2	29	0.09	132	0.5	20		QU04014264	0.005	QU04020685
M77	2771020300	0.06	1.1	9.57	7	280	0.9	2	1.46	0.2	9	99	2790	0.279	5.18	3.36	1.02	300	22	0.89	4	930	13	5.37	2	140	0.12	117	10	19		QU04014264	0.005	QU04020685
M77	2771050310	0.073	1.9	8.42	17	250	0.6	4	0.43	0.2	7	78	5150	0.515	5.35	3.41	0.71	162	86	0.13	2	790	30	5.55	6	28	0.09	114	10	64		QU04014264	0.01	QU04020685
M77	2771080320	0.119	1.4	7.23	7	170	0.7	3	0.92	15.4	8	127	3350	0.335	3.92	3.11	0.91	344	11	0.28	4	660	58	4.18	2	40	0.1	132	0.5	2960		QU04014264	0.1	QU04020685
M77	2771110330	0.077	1.3	6.79	9	190	0.6	4	0.41	0.2	9	142	3560	0.356	5.9	3.16	0.61	162	21	0.08	5	680	29	6.13	2	18	0.09	154	10	28		QU04014264	0.005	QU04020685
M77	2771140340	0.098	1.7	6.09	7	190	0.6	4	0.34	0.2	8	172	4070	0.407	5.12	2.97	0.56	159	19	0.07	4	430	18	5.18	5	26	0.08	154	10	18		QU04014264	0.005	QU04020685
M77	2771140349	0.104	1.6	6.09	10	210	0.6	3	0.35	0.2	7	162	4040	0.404	5.23	2.95	0.57	160	18	0.07	3	420	20	5.27	2	26	0.09	152	10	19		QU04014264	0.005	QU04020685
M77	2771170350	0.098	1.4	7.74	5	290	0.7	4	0.59	0.2	8	106	4010	0.401	5.26	3.54	0.71	223	32	0.1	4	740	32	5.53	2	29	0.1	132	10	70		QU04014264	0.005	QU04020685
M77	2771200360	0.062	1	7.81	2	320	0.7	3	0.66	0.2	8	104	2720	0.272	4.89	3.48	0.72	225	14	0.16	5	740	31	5.06	2	31	0.09	138	10	32		QU04014264	0.005	QU04020685
M77	2771230370	0.091	1.4	7.15	11	180	0.7	1	1.38	0.5	9	60	3200	0.320	3.98	3.29	0.56	430	23	0.15	1	580	27	4.07	2	34	0.09	116	10	117		QU04014264	0.01	QU04020685
M77	2775230370	0.157	1.3	8.14	5	180	0.8	3	1.06	0.2	15	67	3730	0.373	4	4.01	0.84	728	94	1.3	4	510	52	2.31	2	186	0.15	101	0.5	106		QU04014264	0.04	QU04020685
M77	2771260380	0.198	1.5	7.65	7	190	0.7	3	1.96	0.2	11	126	5340	0.534	4.17	4.19	0.85	773	44	0.34	4	650	23	3.98	2	87	0.14	130	0.5	65		QU04014264	0.005	QU04020685
M77	2771290390	0.055	0.7	8.15	2	180	0.8	3	1.54	0.2	8	102	2720	0.272	4.58	3.99	0.8	438	25	0.35	3	770	6	4.74	2	56	0.09	124	10	19		QU04014264	0.005	QU04020685
M77	2771320400	0.067	1.3	6.83	2	140	0.7	3	0.7	0.2	8	116	3990	0.399	4.12	3.26	0.55	241	15	0.06	6	510	8	4.43	2	27	0.08	144	10	9		QU04014264	0.005	QU04020685
M77	2771350410	0.071	1.1	7.51	2	210	0.7	1	0.53	0.2	8	105	4140	0.414	5.04	3.53	0.67	156	16	0.1	6	670	6	5.54	2	29	0.08	134	10	6		QU04014264	0.005	QU04020685
M77	2771380420	0.077	1.1	6.79	2	150	0.6	3	0.43	0.2	7	100	4080	0.408	4.27	3.13	0.66	178	43	0.07	5	510	6	4.6	2	28	0.08	134	10	6		QU04014264	0.005	QU04020685
M77	2771410430	0.084	1.3	6.53	2	130	0.6	1	0.45	0.2	8	123	6500	0.650	4.36	3.35	0.61	191	42	0.09	5	390	8	4.75	2	42	0.07	130	10	20		QU04014264	0.005	QU04020685
M77	2771440440	0.086	0.9	6.97	2	130	0.6	3	0.62	0.2	9	111	3660	0.366	3.98	3.44	0.7	207	15	0.27	4	570	8	4.2	2	58	0.09	124	10	11		QU04014264	0.005	QU04020685
M77	2771470450	0.076	1.4	7.34	2	140	0.6	3	0.75	0.2	8	112	4710	0.471	3.87	3.87	0.79	238	20	0.33	5	600	8	4.06	2	107	0.08	132	10	17		QU04014264	0.005	QU04020685
M77	2771500460	0.1	2.3	6.79	2	160	0.6	3	0.6	0.2	7	120	6040	0.604	3.93	3.52	0.78	242	30	0.15	5	520	10	4.06	2	62	0.09	154	0.5	20		QU04014264	0.005	QU04020685
M77	2771530470	0.107	1.6	6.31	2	130	0.5	3	0.64	0.2	9	121	7000	0.700	3.67	3.6	0.6	236	34	0.09	6	360	8	3.94	2	68	0.07	130	10	17		QU04014264	0.01	QU04020685
M77	2771530478	0.066	0.9	7.34	2	130	0.7	3	1.06	0.2	7	108	5060	0.506	3.64	3.63	0.87	317	81	0.46	6	590	8	3.69	7	122	0.09	127	10	19		QU04014264	0.005	QU04020685
M77	2771560480	0.064	0.8	7.49	2	100	0.7	2	1.14	0.2	8	101	4630	0.463	3.56	3.67	0.9	338	48	0.5	4	630	8	3.52	2	132	0.09	124	0.5	23		QU04014264	0.01	QU04020685
M77	2771590490	0.082	2	7.05	13	130	0.6	2	0.71	0.2	9	119	5820	0.582	4.12	3.32	0.72	253	32	0.07	5	540	9	4.49	12	48	0.07	140	10	20		QU04014264	0.01	QU04020685
M77	2771620500	0.103	1.4	5.68	11	110	0.5	4	0.39	0.2	8	135	4560	0.456	3.66	2.78	0.54	176	44	0.06	5	370	11	3.88	7	39	0.07	134	10	53		QU04014264	0.01	QU04020685
M77	2771650510	0.123	1.7	6.04	7	120	0.5	3	0.52	0.2	11	112	7510	0.751	3.46	3.63	0.55	240	16	0.11	6	390	14	3.67	7	75	0.07	136	0.5	70		QU04014264	0.01	QU04020685
M77	2771680520	0.092	1.5	6.9	2	150	0.7	2	0.68	0.8	10	92	4220	0.422	4.41	4.13	0.57	274	44	0.21	3	500	15	4.81	2	77	0.08	134	10	134		QU04014264	0.01	QU04020685
M77	2771710530	0.057	0.7	7.6	2	150	0.8	2	1.08	0.7	11	98	3150	0.315	4.57	3.97	0.73	403	17	0.36	3	630	13	4.95	2	79	0.08	146	0.5	125		QU04014264	0.01	QU04020685
M77	2771710539	0.06	0.7	7.27	2	210	0.7	2	1.02	0.7	10	97	3000	0.300	4.4	3.83	0.69	369	16	0.34	3	600	12	4.76	2	78	0.08	140	0.5	124		QU04014264	0.01	QU04020685
M77	2771740540	0.091	1.7	5.78	8	150	0.5	2	0.75	2.3	9	103	4950	0.495	4.08	3.32	0.53	305	28	0.28	3	410	17	4.53	5	66	0.08	140	10	426		QU04014264	0.02	QU04020685
M77	2771770550	0.091	1.4	6.53	2	140	0.5	2	0.84	0.2	9	55	5380	0.538	4.27	3.73	0.63	393	32	0.38	4	470	12	4.74	2	89	0.08	148	10	45		QU04014264	0.005	QU04020685

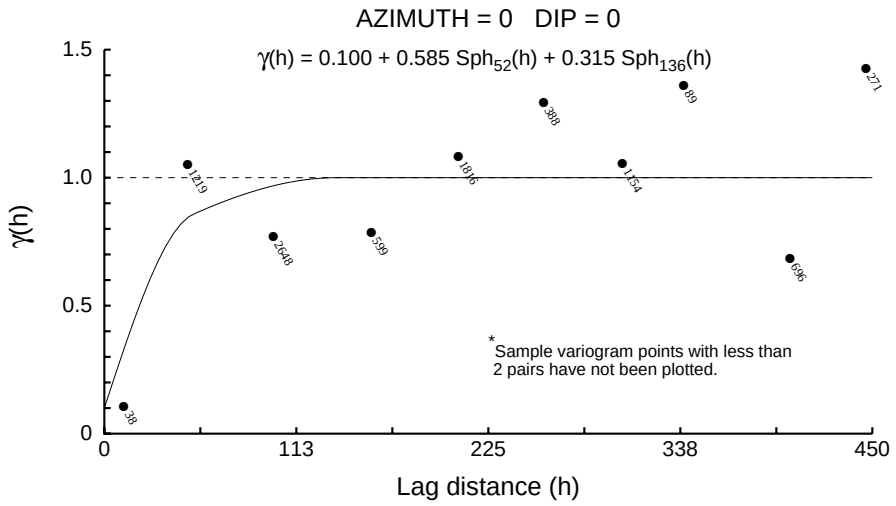
DDH	SAMPLE	Au	Ag	Al	As	Ba	Be	Bi	Ca	Cd	Co	Cr	Cu	Cu Final	Fe	K	Mg	Mn	Mo	Na	Ni	P	Pb	S	Sb	Sr	Ti	V	W	Zn	Cu OD	Hg	
	DESCRIPTION	ppm	ppm	%	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	%(AMEC)	%	%	%	ppm	ppm	%	ppm	ppm	ppm	%	ppm	ppm	%	ppm	ppm	ppm	%	Cert #	ppm	HG Cert #
M77	2771800560	0.067	1.2	6.83	2	110	0.6	3	0.7	0.2	8	116	5370	0.537	3.38	3.93	0.78	257	19	0.55	4	560	11	3.6	2	99	0.09	142	10	33		QU04014264	0.005	QU04020685
M77	2771830570	0.112	1.1	6.37	2	130	0.5	2	0.92	0.2	9	110	5220	0.522	3.76	3.67	0.68	288	29	0.58	5	510	11	4.06	2	112	0.08	138	10	25		QU04014264	0.005	QU04020685
M77	2771860580	0.072	1.4	6.85	5	130	0.6	2	0.65	0.2	9	99	6410	0.641	3.96	4.01	0.74	214	26	0.42	5	540	10	4.29	2	97	0.09	142	10	22		QU04014264	0.01	QU04020685
M77	2776860580	0.278	1.9	7.17	18	130	0.6	1	0.76	0.8	12	99	7650	0.765	3.12	4.38	0.71	536	62	0.78	6	430	68	2.89	14	170	0.12	105	0.5	144		QU04014264	0.05	QU04020685
M77	2771890590	0.084	1.2	5.71	26	140	0.2	3	0.32	0.2	10	111	6460	0.646	3.57	3.25	0.54	132	27	0.1	5	360	5	3.77	2	54	0.07	141	10	16		QU04014264	0.01	QU04020685
M77	2771920600	0.104	1.3	6.75	5	150	0.5	1	0.62	0.2	11	106	6390	0.639	3.3	3.99	0.76	226	20	0.36	5	520	9	3.45	2	92	0.09	146	0.5	26		QU04014264	0.01	QU04020685
M77	2771950610	0.067	1.2	6.85	2	150	0.5	3	0.81	0.2	8	95	5840	0.584	3.07	4.15	0.88	320	30	0.42	4	540	11	3.2	2	112	0.09	147	10	28		QU04014264	0.01	QU04020685
M77	2771980620	0.06	1	7.48	2	120	0.7	2	1.14	0.2	9	96	5290	0.529	3.58	3.98	0.87	353	35	0.42	4	610	9	3.75	2	99	0.1	138	0.5	32		QU04014264	0.03	QU04020685
M77	2772010630	0.084	1.3	7.17	9	130	0.6	2	0.38	0.2	9	130	7240	0.724	4.02	3.13	0.76	149	26	0.09	6	560	7	4.32	2	36	0.11	162	10	21		QU04014264	0.02	QU04020685
M77	2772010638	0.096	1.1	7.14	15	130	0.6	5	0.35	0.2	10	97	8080	0.808	3.98	3.24	0.77	148	33	0.09	4	560	9	4.26	2	35	0.11	175	10	21		QU04014264	0.02	QU04020685
M77	2772040640	0.083	1.4	6.44	10	110	0.6	2	0.57	0.2	7	75	8250	0.825	3.52	3.1	0.69	183	24	0.09	4	520	7	3.77	2	35	0.08	144	10	30		QU04014264	0.01	QU04020685
M77	2772070650	0.155	2.6	6.56	65	120	0.5	2	0.47	0.2	9	116	7880	0.788	4.19	3.14	0.67	239	22	0.08	5	470	8	4.57	6	50	0.08	158	10	29		QU04014264	0.03	QU04020685
M77	2772100660	0.284	1.8	6.66	2	170	0.5	2	1.1	0.2	11	128	7750	0.775	3.16	4.2	0.67	472	36	0.19	3	480	8	2.89	2	112	0.09	138	0.5	26		QU04014264	0.01	QU04020685
M77	2772130670	0.146	1.8	6.63	6	170	0.5	1	0.9	0.2	12	108	6790	0.679	3.7	4.38	0.65	445	35	0.28	5	430	13	3.65	10	113	0.1	148	10	23		QU04014264	0.02	QU04020685
M77	2772160680	0.155	7.1	6.03	159	160	0.5	10	0.55	2.1	8	108	7610	0.761	3.95	3.62	0.56	568	44	0.12	5	420	62	4.26	35	82	0.09	140	10	395		QU04014264	0.11	QU04020685
M77	2775160680	0.155	1.2	7.9	7	140	0.8	3	0.99	0.2	16	64	3450	0.345	3.73	3.65	0.79	695	109	1.24	5	460	43	2.31	6	178	0.13	92	0.5	99		QU04014264	0.04	QU04020685
M77	2772190690	0.065	1.4	6.51	9	130	0.6	2	0.74	0.2	8	92	6680	0.668	3.66	4.05	0.69	353	21	0.19	4	500	19	3.86	5	93	0.09	138	10	88		QU04014264	0.02	QU04020685
M77	2772220700	0.05	1.1	6.12	6	150	0.5	3	0.51	0.2	8	100	6460	0.646	3.83	3.89	0.61	275	49	0.14	4	370	14	4.06	2	85	0.09	142	10	30		QU04014264	0.01	QU04020685
M77	2772250710	0.07	4.2	6.08	193	160	0.5	3	0.61	1.4	10	149	7070	0.707	4.42	3.89	0.63	625	23	0.11	4	430	63	4.8	18	77	0.09	147	10	205		QU04014264	0.12	QU04020685
M77	2772280720	0.062	1.5	5.79	126	260	0.5	4	0.45	0.2	9	146	5120	0.512	3.37	3.78	0.63	254	21	0.1	4	390	10	3.59	11	73	0.09	150	10	39		QU04014264	0.05	QU04020685
M77	2772310730	0.102	1.2	6.11	25	140	0.5	4	0.51	0.2	9	132	6680	0.668	4.12	3.83	0.66	292	14	0.12	5	440	14	4.36	2	84	0.1	140	10	36		QU04014264	0.02	QU04020685
M77	2772310739	0.09	1.4	6.29	25	160	0.6	2	0.52	0.2	10	138	6850	0.685	4.25	3.91	0.68	299	12	0.13	5	450	13	4.52	5	86	0.09	144	10	37		QU04014264	0.02	QU04020685
M77	2772340740	0.043	0.8	5.49	5	140	0.5	2	0.6	0.5	9	128	4800	0.480	3.97	3.7	0.57	403	22	0.17	4	430	22	4.26	5	81	0.1	156	10	69		QU04014264	0.02	QU04020685
M77	2772370750	0.066	2.3	6.16	20	130	0.6	4	0.67	3.3	10	142	4960	0.496	4.24	3.47	0.62	760	132	0.08	5	510	168	4.58	18	61	0.09	140	0.5	646		QU04014264	0.12	QU04020685
M77	2772400760	0.051	1.8	5.96	40	160	0.6	1	0.55	1	8	150	3810	0.381	3.83	3.62	0.55	767	29	0.08	4	500	87	4.14	18	67	0.08	133	10	195		QU04014264	0.07	QU04020685
M77	2772430770	0.346	3.2	6.15	273	200	0.5	2	0.7	1.4	11	130	4530	0.453	5.38	4.35	0.48	775	25	0.12	3	460	194	5.86	16	99	0.09	163	10	245		QU04014264	0.12	QU04020685
M77	2772460780	0.04	1	7.05	17	100	0.7	2	1.14	0.2	8	93	3770	0.377	3.85	4.43	0.7	461	26	0.4	6	580	9	3.8	6	154	0.1	144	10	18		QU04014264	0.02	QU04020685
M77	2772490790	0.048	1	6.39	24	170	0.5	3	0.73	0.2	9	116	4580	0.458	4.35	4.35	0.6	673	15	0.11	4	490	25	4.63	10	98	0.1	142	10	38		QU04014264	0.03	QU04020685
M77	2772520800	0.063	0.2	6.76	6	120	0.5	2	0.88	0.2	9	110	2370	0.237	3.98	4.58	0.63	514	22	0.23	4	580	13	3.62	2	127	0.1	138	0.5	15		QU04014264	0.01	QU04020685
M77	2772550810	0.066	0.7	6.68	75	150	0.5	2	0.9	0.2	8	103	3800	0.380	4.27	4.16	0.66	480	38	0.17	4	550	16	4.36	8	114	0.09	152	10	24		QU04014264	0.07	QU04020685
M77	2772580820	0.226	4.5	5.18	373	170	0.5	5	0.31	18.5	8	129	3550	0.355	9.99	2.39	0.41	321	24	0.03	4	460	787	10	26	27	0.07	132	0.5	4190		QU04014264	2.46	QU04020685
M77	2772610830	0.076	1.5	6.43	126	220	0.5	3	0.65	5	9	85	3260	0.326	5.87	3.24	0.62	547	22	0.06	3	550	655	6.54	16	67	0.07	134	0.5	1130		QU04014264	1.36	QU04020685
M77	2772640840	0.036	0.2	7.23	8	250	0.6	2	0.85	0.2	11	69	3130	0.313	4.22	5	0.65	366	22	0.18	3	610	13	4.46	2	115	0.1	153	10	87		QU04014264	0.07	QU04020685
M77	2772640848	0.039	0.5	8.02	2	270	0.6	2	0.94	0.5	8	80	2980	0.298	4.75	4.85	0.75	409	26	0.19	3	710	10	4.99	2	132	0.1	150	10	72		QU04014264	0.07	QU04020685
M77	2772670850	0.043	0.8	5.77	2	160	0.2	2	0.59	0.2	10	65	4910	0.491	3.5	4.54	0.45	249	32	0.12	3	380	11	3.69	2	118	0.07	121	10	6		QU04014264	0.02	QU04020685
M77	2772700860	0.039	1.6	6.29	30	160	0.5	3	0.76	0.2	10	64	4480	0.448	4.03	4.11	0.56	291	17	0.08	3	470	9	4.34	12	87	0.08	144	10	28		QU04014264	0.08	QU04020685
M77	2772730870	0.056	1.1	7.24	27	100	0.7	4	1.04	0.2	8	67	2680	0.268	3.61	3.32	0.47	321	19	0.39	2	590	3	3.67	15	58	0.09	99	0.5	14		QU04014264	0.05	QU04020685
M77	2772760880	0.046	0.2	7.69	6	140	0.8	1	2.39	0.2	8	95	1870	0.187	2.99	3.81	0.51	646	28	0.73	3	550	6	2.4	5	87	0.13	88	10	15		QU04014264	0.02	QU04020685
M77	2772790890	0.04	0.2	8.09	8	260	1	3	3.05	0.2	4	29	1390	0.139	2.02	3.39	0.4	657	37	0.99	3	500	4	1.06	2	64	0.15	65	0.5	11		QU04014264	0.01	QU04020685
M77	2772820900	0.031	0.2	7.51	9	180	0.9	2	3.14	0.2	7	48	1660	0.166	2.29	3.52	0.35	603	35	0.85	3	510	5	1.62	2	75	0.13	79	10	8		QU04014264	0.01	QU04020685
M77	2772820909	0.032	0.2	8.11	7	220	0.9	2	3.3	0.2	6	49	1680	0.168	2.48	3.45	0.36	635	37	0.89	4	550	7	1.78	6	78	0.13	78	10	8		QU04014264	0.01	QU04020685
M77	2772850910	0.039	0.6	7.24	5	220	0.9	2	1.32	0.2	11	48	2680	0.268	4.26	4.31	0.4	242	11	0.14	2	690	6	4.44	5	73	0.09	133	10	9		QU04014264	0.01	QU04020685
M77	2772880920	0.055	0.6	7.33	2	150	0.8	2	1.86	0.2	9	59	3060	0.306	3.53	4.98	0.38	384	12	0.29	3	570	10	3.55	2	112	0.1	107	0.5	9		QU04014264	0.01	QU04020685
M77	2772910930	0.046	0.5	7.67	9	150	1.1	3	1.96	0.2	10	69	2790	0.279	3.51	4.83	0.36	305	24	0.3	4	570	7	3.67	2	80	0.11	91	10	4		QU04014264	0.01	QU04020685
M77	2772940940	0.038	0.2	6.93	2	170	0.9	4	2.22	0.2	10	60	3540	0.354	2.96	4.72	0.31	348	26	0.29	3	540	2	2.97	2	97	0.1	89	10	2		QU04014264	0.01	QU04020685
M77	2772970950	0.032	0.2	7.95	6	270	1	1	3.39	0.2	6	39	1175	0.118	2.05	3.79	0.33	593	31	1.41	3	480	14	1.32	5	133	0.14	67	0.5	79		QU04014264	0.12	QU04020685
M77	2773000960	0.056	0.5	9.14	106	120	1.2	3	2.97	0.2	8	44	846	0.085	3.94	3	0.58	573	3	2.51	3	880	13	3.12	5	275	0.24	109	0.5	23		QU04014264	0.06	QU04020685
M77	2775000960	0.157	1.1	8.09	2	130	0.8	4	1.13	0.2	16	62	3580	0.358	3.9	3.66	0.81	686	116	1.3	3	500	41	2.42	5	190	0.14	95	0.5	99		QU04014264	0.05	QU04020685
M80	2800050010	0.242	1.3	7.19	14	400	0.5	1	0.01	0.2	0.5	112	187	0.019	2.26	2.75	0.34	42	42	0.08	6	300	10	0.02	2	22	0.12	110	10	9		QU04014806	0.03	QU04020686
M80	2800100020	0.36	0.6	7.6	19	460	0.6	1	0.01	0.2	1	61	347	0.035	3.47	2.67	0.37	37	55	0.08	2	600	12	0.02	2	26	0.13	124	0.5	7		QU04014806	0.03	QU04020686
M80	2800150030	0.238	0.6	7.79	21	510	0.5	1	0.01	0.2	1	75	547	0.055	4.33	2.71	0.3	41	41	0.11	4	510	10	0.03	2	35	0.16	138	10	8		QU04014806	0.02	QU04020686
M80	2800200040	0.194	0.2	7.49	7	750	0.5	1	0.01	0.2	1	76	421	0.042	3.77	2.61	0.31	42	24	0.13	2	580	12	0.02	2	50	0.15	122	0.5	6		QU04014806	0.01	QU04020686
M80	2800250050	0.294	0.6	7.37	10	830	0.5	1	0.01	0.2	0.5	103	561	0.056	3.91	3.05	0.27	39	28	0.18	3	460	16	0.02	2	70	0.15	124	0.5	6		QU04014806	0.01	QU04020686
M80	2800300060	0.32	0.6	8.29	23	790	0.5	1	0.01	0.2	0.5	58	371	0.037	3.53	3.49	0.29	35	44	0.16	3	330	21	0.02	2	64	0.14	131	0.5	6		QU04014806	0.02	QU04020686
M80	2800350070	0.27	1	7.83	10	810	0.5	1	0.01	0.2	1	66	401	0.040	4.13	3.54	0.39	31	100	0.13	3	250	10	0.02	2	42	0.11	126	0.5	5		QU04014806	0.01	QU04020686

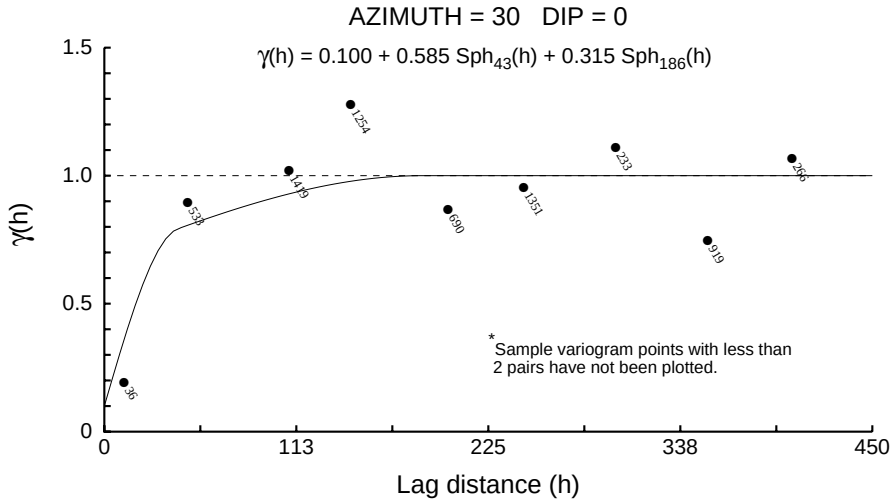
DDH	SAMPLE DESCRIPTION	Au ppm	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd ppm	Co ppm	Cr ppm	Cu ppm	Cu Final %(AMEC)	Fe %	K %	Mg %	Mn ppm	Mo ppm	Na %	Ni ppm	P ppm	Pb ppm	S %	Sb ppm	Sr ppm	Ti %	V ppm	W ppm	Zn ppm	Cu OD %	Cert #	Hg ppm	HG Cert #
M80	2800350079	0.235	0.9	7.46	11	770	0.5	1	0.01	0.2	1	59	383	0.038	3.98	3.41	0.37	30	100	0.13	4	230	9	0.02	2	40	0.11	120	0.5	4		QU04014806	0.01	QU04020686
M80	2800400080	0.086	2.3	6.81	132	1020	0.2	1	0.02	0.2	1	86	307	0.031	4.6	2.99	0.3	44	52	0.11	3	200	7	0.05	12	20	0.09	106	0.5	3		QU04014806	0.08	QU04020686
M80	2800450090	0.2	6.1	5.24	449	1000	0.2	1	0.02	0.2	2	130	918	0.092	4.37	2.3	0.31	66	45	0.05	4	160	13	0.35	128	19	0.09	99	0.5	4		QU04014806	0.35	QU04020686
M80	2800500100	0.158	4	5.59	516	3470	0.2	1	0.02	0.2	0.5	97	547	0.055	4.33	2.47	0.28	54	32	0.08	5	150	7	0.16	112	17	0.08	94	0.5	2		QU04014806	0.32	QU04020686
M80	2800530110	0.167	4.4	5.83	337	650	0.2	1	0.02	0.2	4	63	2230	0.223	4	2.84	0.3	47	49	0.09	3	110	11	1.57	33	34	0.08	96	0.5	20		QU04014806	0.31	QU04020686
M80	2800550120	0.17	3.9	6.53	330	390	0.2	1	0.02	0.2	9	67	8120	0.812	3.62	2.99	0.38	60	30	0.06	4	80	11	3.01	48	25	0.11	111	0.5	63		QU04014806	0.3	QU04020686
M80	2805550120	0.16	1	7.13	8	640	0.7	1	0.97	0.2	15	68	3320	0.332	3.49	3.59	0.74	667	102	1.14	4	450	38	2.02	2	164	0.13	88	0.5	101		QU04014806	0.04	QU04020686
M80	2800570130	0.131	2.2	5.92	273	370	0.2	1	0.03	0.2	14	100	>10000	1.48	4	2.77	0.31	52	37	0.07	5	80	12	4.38	53	20	0.1	106	0.5	75	1.48	QU04014806	0.25	QU04020686
M80	2800590140	0.233	2.7	5.58	360	310	0.2	1	0.02	0.2	15	108	>10000	2.02	4.18	2.78	0.33	64	28	0.08	4	90	14	4.59	64	31	0.11	124	0.5	85	2.02	QU04014806	0.32	QU04020686
M80	2800610150	0.16	3.5	6.1	289	410	0.2	1	0.02	0.5	14	88	>10000	1.17	3.62	3.07	0.35	56	23	0.09	5	90	14	3.95	118	41	0.11	95	0.5	108	1.17	QU04014806	0.37	QU04020686
M80	2800630160	0.234	1.7	6.61	159	470	0.2	1	0.02	0.2	17	60	>10000	1.56	4.41	3.5	0.36	49	30	0.11	4	140	13	4.49	33	40	0.1	113	0.5	51	1.56	QU04014806	0.16	QU04020686
M80	2800650170	0.255	1.5	5.86	84	460	0.2	1	0.02	0.2	16	106	>10000	1.68	3.69	3.63	0.3	44	102	0.15	11	130	10	4.02	18	67	0.08	118	0.5	34	1.68	QU04014806	0.12	QU04020686
M80	2800670180	0.181	3.5	6.44	355	390	0.2	1	0.02	0.5	11	41	>10000	1.17	3.63	3.25	0.38	53	27	0.09	5	180	10	4.01	146	37	0.09	96	0.5	106	1.17	QU04014806	0.35	QU04020686
M80	2800670188	0.204	3.2	6.46	335	450	0.5	1	0.02	0.5	10	64	>10000	1.21	3.58	3.25	0.39	50	24	0.09	5	190	8	3.98	138	38	0.09	96	10	98	1.21	QU04014806	0.33	QU04020686
M80	2800690190	0.159	4.4	5.81	546	300	0.2	1	0.03	0.8	9	44	>10000	1.05	3.7	2.92	0.35	67	52	0.08	4	170	10	4.04	202	38	0.08	80	0.5	164	1.05	QU04014806	0.56	QU04020686
M80	2800710200	0.221	2.4	5.94	416	330	0.2	1	0.02	0.2	12	108	9800	0.980	3.62	3.62	0.33	62	58	0.13	6	230	10	3.87	106	62	0.1	96	10	102		QU04014806	0.36	QU04020686
M80	2800730210	0.159	2.6	6.74	519	430	0.5	1	0.02	0.5	17	80	>10000	1.17	5.37	3.95	0.4	91	41	0.12	6	230	7	5.71	82	52	0.09	103	0.5	118	1.17	QU04014806	0.36	QU04020686
M80	2800760220	0.174	2.4	6.07	353	210	0.2	1	0.02	0.5	11	126	7910	0.791	3.58	3.32	0.34	76	23	0.08	7	280	9	3.67	44	41	0.08	97	0.5	106		QU04014806	0.31	QU04020686
M80	2800790230	0.162	2.8	5.3	530	320	0.2	1	0.02	0.7	12	69	8150	0.815	4.75	2.9	0.32	73	37	0.08	3	220	8	4.95	120	39	0.08	85	0.5	134		QU04014806	0.4	QU04020686
M80	2800820240	0.243	3	6.3	448	330	0.2	1	0.02	0.7	13	41	7570	0.757	4.34	3.36	0.35	60	57	0.1	3	360	10	4.54	75	48	0.09	99	0.5	132		QU04014806	0.4	QU04020686
M80	2800820248	0.228	2.9	6.21	447	350	0.2	1	0.02	0.7	14	69	7270	0.727	4.28	3.35	0.35	71	61	0.1	5	380	10	4.45	164	48	0.1	103	10	136		QU04014806	0.38	QU04020686
M80	2800850250	0.163	2.7	6.8	375	440	0.5	1	0.04	0.7	12	69	5640	0.564	4	3.42	0.4	74	31	0.08	5	510	12	4.12	150	44	0.11	98	10	128		QU04014806	0.36	QU04020686
M80	2800880260	0.136	1.9	6.87	328	460	0.5	2	0.08	0.7	14	61	4020	0.402	4.42	3.39	0.4	72	30	0.12	11	490	11	4.58	110	46	0.12	112	0.5	105		QU04014806	0.3	QU04020686
M80	2800910270	0.158	1.2	5.89	206	430	0.2	1	0.05	0.2	11	59	5090	0.509	3.43	3.9	0.28	66	24	0.16	5	380	12	3.45	30	92	0.1	104	0.5	73		QU04014806	0.2	QU04020686
M80	2800940280	0.166	2.4	6.12	379	380	0.2	2	0.05	1	10	71	5190	0.519	3.85	3.42	0.32	70	14	0.12	5	360	10	4.01	110	54	0.11	114	10	121		QU04014806	0.4	QU04020686
M80	2800970290	0.161	1.5	5.79	273	360	0.2	1	0.05	0.6	13	108	4930	0.493	4.58	3.18	0.32	138	17	0.09	5	380	14	4.65	28	48	0.11	110	10	75		QU04014806	0.24	QU04020686
M80	2806970290	0.265	2	6.78	21	400	0.6	1	0.76	0.8	12	108	7620	0.762	3.12	4.49	0.7	534	51	0.75	6	430	64	2.72	11	166	0.12	104	0.5	160		QU04014806	0.05	QU04020686
M80	2801000300	0.092	1.8	6.16	168	360	0.5	1	0.11	0.2	11	90	6790	0.679	4.75	3.56	0.32	791	29	0.12	4	440	10	4.31	23	61	0.11	120	0.5	58		QU04014806	0.16	QU04020686
M80	2801030310	0.078	0.6	5.27	15	260	0.2	1	0.05	0.2	10	94	2260	0.226	3.18	3.43	0.25	80	47	0.13	4	410	8	3.14	2	80	0.09	105	10	7		QU04014806	0.02	QU04020686
M80	2801060320	0.068	0.8	5.23	10	220	0.2	1	0.03	0.2	10	56	3710	0.371	3.31	2.99	0.25	56	78	0.1	3	250	5	3.32	2	55	0.08	110	0.5	3		QU04014806	0.01	QU04020686
M80	2801090330	0.13	1	5.59	10	240	0.2	1	0.03	0.2	12	90	3380	0.338	3.5	3.53	0.28	56	32	0.12	4	330	9	3.44	2	80	0.11	140	0.5	10		QU04014806	0.01	QU04020686
M80	2801090339	0.138	0.9	5.71	9	380	0.2	1	0.03	0.2	13	78	3420	0.342	3.64	3.55	0.28	43	28	0.12	4	340	8	3.61	2	81	0.12	140	10	11		QU04014806	0.01	QU04020686
M80	2801120340	0.088	0.9	5.27	20	220	0.2	1	0.03	0.2	13	44	2410	0.241	4.65	2.63	0.27	47	27	0.07	4	420	11	4.7	2	30	0.1	132	0.5	8		QU04014806	0.02	QU04020686
M80	2801150350	0.125	1.9	5.67	38	200	0.2	1	0.06	0.2	16	76	3090	0.309	5.12	2.61	0.31	55	160	0.06	5	470	9	5.22	10	15	0.08	132	10	22		QU04014806	0.02	QU04020686
M80	2801180360	0.096	0.8	6.04	30	380	0.2	1	0.1	0.2	15	47	3200	0.320	3.33	3.79	0.3	37	58	0.14	6	740	12	3.33	2	87	0.1	115	0.5	46		QU04014806	0.02	QU04020686
M80	2801210370	0.133	1	4.8	42	180	0.2	1	0.11	0.2	11	86	3790	0.379	3.47	2.87	0.22	94	20	0.11	5	390	8	3.38	7	64	0.07	105	0.5	23		QU04014806	0.03	QU04020686
M80	2801240380	0.093	1.4	3.87	86	180	0.2	1	0.08	0.2	12	51	3670	0.367	3.01	2.35	0.2	74	12	0.08	2	300	6	2.99	7	56	0.06	93	0.5	21		QU04014806	0.04	QU04020686
M80	2801270390	0.144	0.8	3.95	48	260	0.2	1	0.1	0.2	10	102	2790	0.279	3.98	2.18	0.23	348	20	0.06	4	240	6	3.72	2	45	0.08	116	0.5	7		QU04014806	0.02	QU04020686
M80	2801300400	0.15	0.9	3.02	40	150	0.2	1	0.3	0.2	9	59	2310	0.231	3.35	1.69	0.26	478	16	0.06	2	220	6	3.23	2	41	0.06	92	0.5	7		QU04014806	0.02	QU04020686
M80	2801330410	0.291	0.5	3.57	26	170	0.2	1	0.23	0.2	6	53	1810	0.181	3.64	2.23	0.39	807	9	0.1	3	230	4	2.59	2	64	0.08	102	0.5	11		QU04014806	0.01	QU04020686
M80	2801360420	0.113	0.9	4.24	18	170	0.2	1	0.56	0.2	10	105	3140	0.314	4.19	2.4	0.38	780	48	0.08	4	420	4	3.61	2	57	0.07	112	0.5	8		QU04014806	0.01	QU04020686
M80	2801390430	0.119	0.7	4.01	7	220	0.2	1	0.47	0.2	12	60	3750	0.375	3.82	2.34	0.35	699	12	0.07	3	400	5	3.42	2	46	0.07	93	0.5	4		QU04014806	0.01	QU04020686
M80	2801420440	0.074	0.2	6.02	10	230	0.5	1	0.79	0.2	9	90	1680	0.168	3.96	3.1	0.52	1060	36	0.09	5	570	6	3.29	2	58	0.09	103	0.5	10		QU04014806	0.005	QU04020686
M80	2801420448	0.073	0.5	5.93	10	360	0.5	1	0.79	0.2	9	92	1685	0.169	3.91	3.09	0.52	1040	39	0.09	4	570	6	3.24	2	57	0.09	106	0.5	10		QU04014806	0.005	QU04020686
M80	2801450450	0.111	2.1	4.63	13	480	0.2	1	0.6	3.8	16	71	3940	0.394	5.52	2.81	0.42	1305	174	0.11	3	400	47	5.28	2	67	0.07	94	0.5	725		QU04014806	0.11	QU04020686
M80	2801480460	0.059	1.2	4.08	5	150	0.2	1	0.54	0.2	11	81	3340	0.334	3.38	1.99	0.33	348	13	0.05	4	410	14	3.29	2	28	0.07	75	0.5	8		QU04014806	0.005	QU04020686
M80	2801510470	0.073	0.6	8.09	8	230	0.8	1	2.31	1.8	8	42	1555	0.156	2.98	3.86	0.78	1080	159	0.62	2	730	13	2.43	2	88	0.11	67	0.5	389		QU04014806	0.04	QU04020686
M80	2801540480	0.081	0.9	8.26	15	230	0.8	1	1.82	0.2	9	43	1900	0.190	3.1	4.24	0.79	796	7	1.16	3	780	58	2.41	2	170	0.12	71	0.5	85		QU04014806	0.01	QU04020686
M80	2801570490	0.074	0.2	8.7	9	280	0.9	1	2.03	0.2	8	37	1650	0.165	2.96	3.81	0.85	821	28	1.64	2	840	12	1.66	2	207	0.15	76	0.5	36		QU04014806	0.02	QU04020686
M80	2805570490	0.155	1.3	7.97	7	210	0.8	1	1.07	0.5	15	68	3470	0.347	3.92	3.78	0.83	724	92	1.26	4	500	42	2.22	2	180	0.14	95	0.5	106		QU04014806	0.04	QU04020686
M80	2801600500	0.066	0.6	7.92	8	230	0.8	1	2.06	0.2	11	50	2060	0.206	2.98	3.94	0.59	825	134	0.76	2	750	11	2.6	2	111	0.11	71	0.5	48		QU04014806	0.01	QU04020686
M80	2801630510	0.06	0.7	7.74	10	200	0.8	1	1.66	0.2	11	32	2010	0.201	3.29	3.87	0.61	797	54	0.39	2	730	9	3.01	2	74	0.1	67	0.5	12		QU04014806	0.01	QU04020686
M80	2801660520	0.068	0.7	7.68	34	230	0.9	1	1.84	0.2	7	42	1360	0.136	3	3.81	0.79	1615	22	0.11	2	690	15	2.64	8	54	0.11	62	0.5	19		QU04014806	0.01	QU04020686
M80	2801690530	0.07	2	7.92	69	270	0.9	1	1.62	1.1	8	31	1290	0.129	2.73	4	0.8	1865	31	0.07	1	720	78	2.34	45	61	0.14	67	0.5	221		QU04014806	0.07	QU04020686
M80	2801720540	0.055	0.8	8.14	16	290	0.9	1	1.7	4.3	12	53	2900	0.290	3.6	4.18	0.81	1790	35	0.08	4	680	376	3.3	8	49	0.13	80	0.5	851		QU04014806	0.13	QU04020686

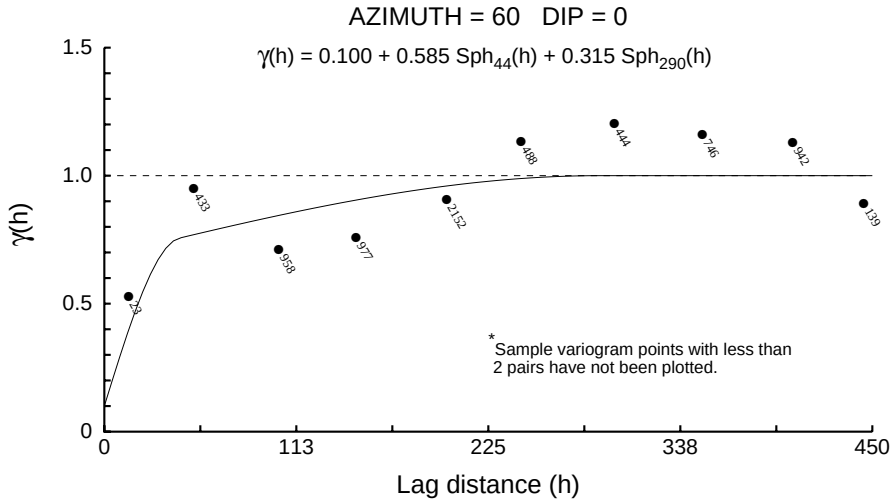
DDH	SAMPLE DESCRIPTION	Au ppm	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd ppm	Co ppm	Cr ppm	Cu ppm	Cu Final %(AMEC)	Fe %	K %	Mg %	Mn ppm	Mo ppm	Na %	Ni ppm	P ppm	Pb ppm	S %	Sb ppm	Sr ppm	Ti %	V ppm	W ppm	Zn ppm	Cu OD %	Cert #	Hg ppm	HG Cert #
M80	2801750550	0.047	0.7	7.77	20	220	0.8	1	1.48	0.2	8	57	2110	0.211	2.97	4.04	0.68	1130	29	0.09	6	580	32	2.77	14	60	0.08	57	0.5	71		QU04014806	0.04	QU04020686
M80	2801750559	0.041	0.7	7.6	21	250	0.8	1	1.45	0.2	7	51	2110	0.211	2.86	4.09	0.66	1090	25	0.09	4	580	34	2.68	13	59	0.08	58	0.5	80		QU04014806	0.04	QU04020686
M80	2801780560	0.036	0.7	8.02	19	290	0.8	1	1.26	0.2	6	29	1885	0.189	2.54	4.22	0.66	852	415	0.1	2	570	12	2.38	19	62	0.07	54	0.5	16		QU04014806	0.03	QU04020686
M80	2801810570	0.052	0.6	8.01	12	410	0.8	1	1.34	0.2	9	50	1995	0.200	2.99	4.13	0.64	921	13	0.1	3	590	17	2.87	10	59	0.07	53	0.5	11		QU04014806	0.02	QU04020686
M80	2801840580	0.068	3.8	7.2	95	420	0.7	2	0.62	1	6	43	2210	0.221	3.75	3.48	0.52	718	25	0.07	1	530	58	3.86	49	29	0.08	58	10	133		QU04014806	0.11	QU04020686
M80	2801870590	0.058	1.5	7.18	34	390	0.6	1	1.03	1.3	6	35	1470	0.147	3.44	3.04	0.53	897	15	0.08	1	480	146	3.52	21	34	0.07	55	0.5	219		QU04014806	0.09	QU04020686
M80	2801900600	0.041	6.5	7.9	158	340	0.7	1	0.36	12.6	10	57	2530	0.253	3.53	3.59	0.51	523	55	0.08	2	600	960	3.75	110	20	0.08	66	0.5	2530		QU04014806	0.54	QU04020686
M80	2801930610	0.057	1.8	8.66	52	430	0.8	1	1.08	0.2	13	43	2680	0.268	4.9	3.83	0.67	529	89	0.1	3	710	50	4.86	30	31	0.08	66	0.5	35		QU04014806	0.06	QU04020686
M80	2801960620	0.056	0.7	7.72	28	300	0.7	1	1.22	0.2	10	59	1965	0.197	4.52	3.67	0.64	562	56	0.11	6	630	13	4.44	2	32	0.12	91	0.5	10		QU04014806	0.01	QU04020686
M80	2801990630	0.047	0.7	7.8	30	320	0.8	1	1.5	0.2	9	34	1145	0.115	5.03	3.2	0.67	414	55	0.71	7	700	11	4.93	2	65	0.14	106	0.5	20		QU04014806	0.01	QU04020686
M80	2802020640	0.054	0.2	7.32	12	230	0.8	1	1.24	0.2	8	44	1750	0.175	3.63	3.34	0.57	291	23	0.87	3	550	8	3.3	2	121	0.1	65	0.5	16		QU04014806	0.01	QU04020686
M80	2802020648	0.051	0.5	7.87	15	210	0.8	1	1.38	0.2	8	49	1810	0.181	3.72	3.37	0.62	310	38	0.97	3	590	8	3.34	2	139	0.1	65	0.5	16		QU04014806	0.005	QU04020686
M80	2802050650	0.043	0.7	7.93	15	350	0.8	1	1.58	0.2	9	56	1630	0.163	3.41	3.63	0.58	323	158	1.01	3	590	10	3.11	2	172	0.09	63	0.5	25		QU04014806	0.01	QU04020686
M80	2802080660	0.072	0.7	7.16	14	420	0.7	1	1.14	0.2	11	58	2220	0.222	3.88	3.53	0.61	292	23	0.85	2	620	18	3.66	2	148	0.1	74	0.5	25		QU04014806	0.01	QU04020686
M80	2802110670	0.045	0.5	7.88	23	290	0.9	1	1.32	0.2	8	54	1425	0.143	3.33	3.71	0.63	256	10	1.36	3	600	9	3.2	2	232	0.09	60	0.5	20		QU04014806	0.02	QU04020686
M80	2802140680	0.059	0.7	8.3	68	230	0.8	1	1.09	0.2	8	73	1995	0.200	3.67	3.75	0.63	372	19	0.99	0.5	570	13	3.72	2	138	0.09	69	0.5	32		QU04014806	0.04	QU04020686
M80	2802170690	0.073	1	7.62	41	100	0.8	1	1.34	0.2	7	76	3450	0.345	3.1	3.93	0.72	392	15	1.07	3	560	11	2.96	5	189	0.11	90	0.5	22		QU04014806	0.02	QU04020686
M80	2802200700	0.083	0.8	9.43	21	140	1	1	2.87	0.2	1	47	2440	0.244	4.13	2.22	1.18	476	11	2.08	2	840	10	3.17	2	491	0.18	108	0.5	30		QU04014806	0.01	QU04020686
M80	2802230710	0.06	0.2	8.62	34	220	0.9	1	2.57	0.2	6	59	1255	0.126	3.9	2.71	0.9	533	47	1.48	2	710	7	2.82	2	353	0.15	83	0.5	27		QU04014806	0.02	QU04020686
M80	2802260720	0.058	0.7	7.93	32	210	0.8	1	1.34	0.2	5	65	2290	0.229	3.2	3.51	0.65	294	10	1.14	1	630	12	3.19	2	194	0.1	65	0.5	16		QU04014806	0.03	QU04020686
M80	2802290730	0.063	0.6	8.14	43	120	0.9	1	1.02	0.2	9	56	1950	0.195	3.82	3.68	0.61	287	99	0.78	3	570	11	3.99	2	130	0.08	68	0.5	16		QU04014806	0.04	QU04020686
M80	2802290739	0.061	0.5	8.15	40	120	0.9	1	1.03	0.2	7	51	1985	0.199	3.61	3.6	0.61	289	71	0.79	1	540	7	3.71	2	132	0.08	68	0.5	16		QU04014806	0.03	QU04020686
M80	2802320740	0.068	0.8	8.14	67	130	0.8	1	1.74	0.2	9	50	2120	0.212	3.52	3.79	0.59	403	22	0.65	0.5	580	9	3.69	5	116	0.07	67	0.5	23		QU04014806	0.04	QU04020686
M80	2802350750	0.086	0.7	7.88	63	120	0.7	1	1.29	0.5	8	56	2470	0.247	2.64	4.11	0.54	287	126	1.21	8	520	23	2.72	6	220	0.08	69	0.5	55		QU04014806	0.05	QU04020686
M80	2802380760	0.069	0.2	8.42	25	90	0.9	1	2.05	0.2	8	47	1410	0.141	3.59	2.96	0.83	301	10	2.09	4	750	11	3.45	5	390	0.13	98	0.5	30		QU04014806	0.03	QU04020686
M80	2802410770	0.057	0.5	8.37	30	160	0.8	1	2.21	0.2	9	54	810	0.081	5.08	2.69	0.75	397	13	1.44	5	740	25	5.64	6	222	0.13	104	0.5	45		QU04014806	0.02	QU04020686
M80	2802440780	0.114	0.2	8.52	31	160	0.9	1	1.25	1.6	8	52	1395	0.140	3.85	3.8	0.49	212	52	1.06	0.5	650	25	4.18	2	217	0.09	73	0.5	249		QU04014806	0.05	QU04020686
M80	2802470790	0.099	0.2	8.32	17	210	0.9	1	1.1	0.2	8	70	1015	0.102	5.57	3.39	0.46	123	15	1.19	4	680	10	6.18	2	214	0.09	72	10	10		QU04014806	0.02	QU04020686
M80	2806470790	0.276	1.9	6.9	19	110	0.6	1	0.74	0.9	11	102	7790	0.779	3.05	4.41	0.69	514	54	0.79	2	430	73	2.81	12	160	0.12	106	0.5	132		QU04014806	0.005	QU04020686
M80	2802500800	0.08	0.2	7.9	18	190	0.8	1	0.98	0.2	9	46	1045	0.105	6.28	3.58	0.42	121	20	1.08	3	660	6	7	2	203	0.09	88	10	11		QU04014806	0.03	QU04020686
M80	2802530810	0.059	0.2	8.27	22	180	0.9	1	1.29	0.2	8	58	1045	0.105	6.23	3.51	0.41	117	18	1.44	3	610	10	7	2	269	0.08	73	10	11		QU04014806	0.03	QU04020686
M80	2802560820	0.042	0.2	8.7	24	160	0.9	1	1.36	0.2	6	50	929	0.093	4.9	3.49	0.44	166	20	1.31	2	620	8	5.49	2	241	0.09	72	10	12		QU04014806	0.03	QU04020686
M80	2802590830	0.044	0.2	8.04	9	100	0.8	1	1.18	0.2	10	61	915	0.092	4.48	3.2	0.42	140	25	1.14	3	540	7	4.98	2	226	0.08	71	10	12		QU04014806	0.02	QU04020686
M80	2802590838	0.045	0.2	8.18	14	140	0.8	1	1.24	0.2	10	46	999	0.100	4.62	3.35	0.43	140	30	1.18	2	570	6	5.13	2	236	0.08	71	10	11		QU04014806	0.02	QU04020686
M80	2802620840	0.048	0.2	8.16	15	150	0.8	1	1.46	0.2	10	62	853	0.085	5.03	3.11	0.37	130	29	1.38	3	570	8	5.7	5	273	0.08	66	10	10		QU04014806	0.02	QU04020686
M80	2802650850	0.052	0.2	8.02	16	120	0.9	1	1.48	0.2	6	50	791	0.079	5.35	3.01	0.47	197	41	1.4	0.5	590	13	5.86	2	278	0.09	67	10	16		QU04014806	0.02	QU04020686
M80	2802680860	0.067	0.2	7.92	10	170	0.8	1	1.34	0.2	8	61	1340	0.134	4.17	3.62	0.41	158	86	1.44	0.5	510	11	4.59	2	280	0.07	61	10	9		QU04014806	0.01	QU04020686
M80	2802710870	0.052	0.2	8.67	11	170	0.9	1	1.54	0.2	7	64	684	0.068	4.77	3.51	0.41	163	26	1.56	2	590	7	5.36	2	280	0.08	73	10	9		QU04014806	0.01	QU04020686
M80	2802740880	0.032	0.2	8.29	12	190	0.9	1	1.54	0.2	9	49	801	0.080	4.43	3.49	0.45	142	60	1.74	2	600	15	5.02	5	349	0.09	65	0.5	21		QU04014806	0.02	QU04020686
M80	2802770890	0.034	0.2	8.51	16	90	0.9	1	1.6	0.2	12	62	1360	0.136	3.05	3.65	0.5	167	29	1.63	1	640	8	3.32	2	320	0.09	66	10	11		QU04014806	0.02	QU04020686
M80	2802770899	0.036	0.2	8.48	9	100	0.9	1	1.59	0.2	11	64	1365	0.137	3.06	3.65	0.49	163	29	1.62	3	630	9	3.34	2	319	0.09	64	0.5	11		QU04014806	0.02	QU04020686
M80	2802800900	0.046	0.2	8.77	12	210	0.8	1	1.24	0.2	10	63	1045	0.105	3.66	3.91	0.49	158	25	1.42	3	670	12	4	2	288	0.08	68	0.5	8		QU04014806	0.01	QU04020686
M80	2802830910	0.046	0.2	8.02	5	120	0.8	1	1.18	0.2	8	68	1400	0.140	2.74	3.92	0.5	209	7	1.32	2	630	10	2.71	2	290	0.1	78	0.5	11		QU04014806	0.01	QU04020686
M80	2802860920	0.029	0.2	8.44	10	110	0.9	1	1.38	0.2	7	59	743	0.074	2.72	3.43	0.5	195	37	1.78	3	710	12	2.96	2	348	0.1	77	10	17		QU04014806	0.01	QU04020686
M80	2802890930	0.036	0.2	8.05	16	110	0.8	1	1.14	0.2	8	57	1095	0.110	2.52	3.67	0.46	162	15	1.7	1	610	14	2.7	5	324	0.09	67	0.5	14		QU04014806	0.02	QU04020686
M80	2802920940	0.045	0.2	6.7	12	120	0.6	1	0.87	0.2	13	64	1130	0.113	3.14	3.15	0.42	118	34	1.26	0.5	520	9	3.48	2	212	0.08	71	0.5	9		QU04014806	0.01	QU04020686
M80	2802950950	0.092	0.2	8.1	54	130	0.8	1	2.91	0.2	9	43	416	0.042	3.34	2.88	0.75	1010	52	1.82	5	690	16	2.01	2	387	0.18	82	0.5	47		QU04014806	0.03	QU04020686
M80	2802980960	0.108	0.2	9.31	78	380	0.9	1	3.69	0.2	6	25	50	0.005	3.05	2.87	0.95	1305	0.5	2.31	2	800	13	0.76	7	467	0.22	88	0.5	63		QU04014806	0.03	QU04020686
M80	2805980960	0.158	1.1	7.79	9	140	0.8	1	0.99	0.6	15	66	3480	0.348	3.63	3.59	0.78	654	109	1.22	2	450	39	2.21	2	168	0.14	94	0.5	102		QU04014806	0.05	QU04020686
M80	2803000970	0.06	0.5	8.74	13	330	0.9	1	2.44	1.1	9	48	1620	0.162	2.76	3.14	0.71	596	39	1.92	0.5	710	31	1.72	5	378	0.15	80	0.5	162		QU04014806	0.05	QU04020686

APPENDIX B VARIOGRAPHY

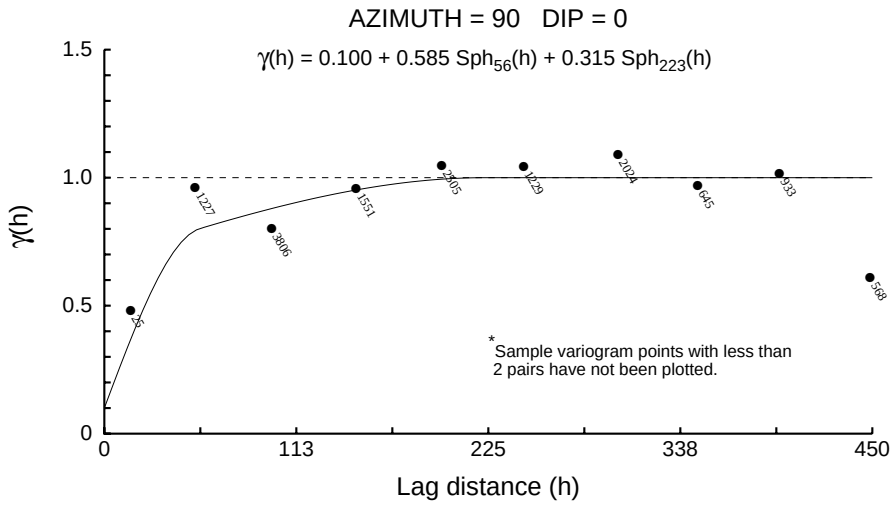
Cu - All Zones

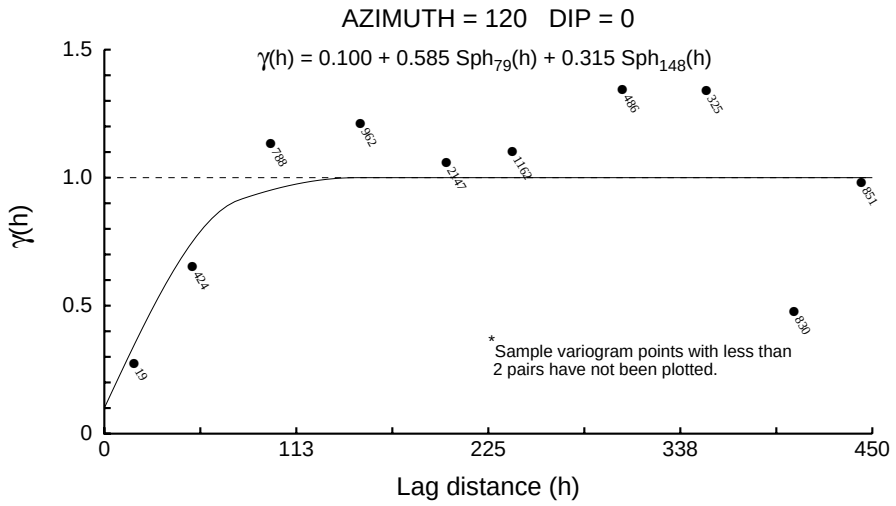

AZIMUTH = 0 DIP = 0
γ(h) = 0.100 + 0.585 Sph52(h) + 0.315 Sph136(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
38
1219
2648
599
1816
388
1554
89
271
696
*Sample variogram points with less than
2 pairs have not been plotted.

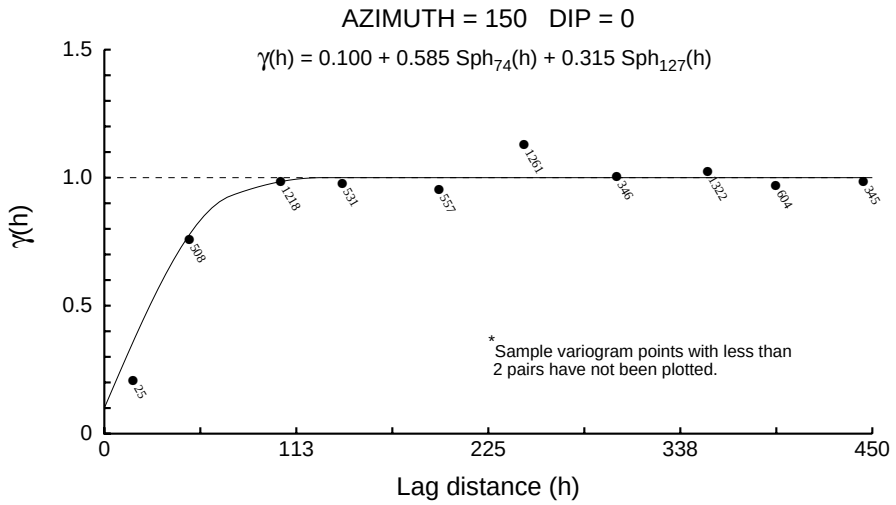

AZIMUTH = 30 DIP = 0
γ(h) = 0.100 + 0.585 Sph43(h) + 0.315 Sph186(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
36
539
1419
1254
690
1351
233
919
265
*Sample variogram points with less than
2 pairs have not been plotted.


AZIMUTH = 60 DIP = 0
γ(h) = 0.100 + 0.585 Sph44(h) + 0.315 Sph290(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
23
433
958
977
2152
488
444
746
942
139
*Sample variogram points with less than
2 pairs have not been plotted.

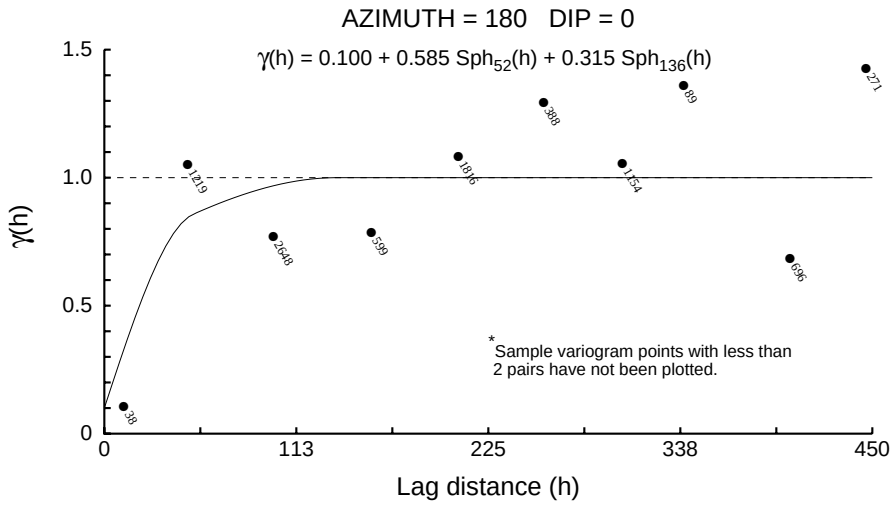
Cu - All Zones

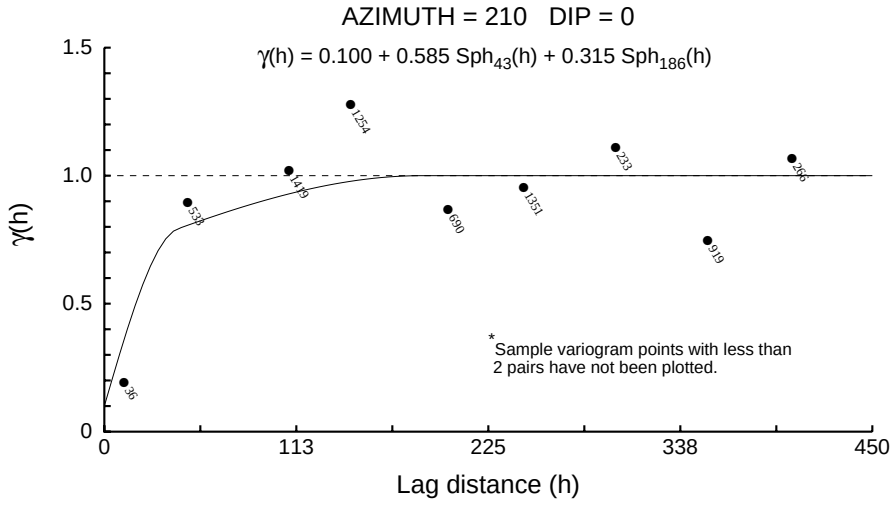

AZIMUTH = 90 DIP = 0
γ(h) = 0.100 + 0.585 Sph56(h) + 0.315 Sph223(h)
γ(h)
1.5
1.0
0.5
0
0
113
225
338
450
Lag distance (h)
55
1227
3806
1551
2005
1229
2024
645
933
568
*Sample variogram points with less than 2 pairs have not been plotted.

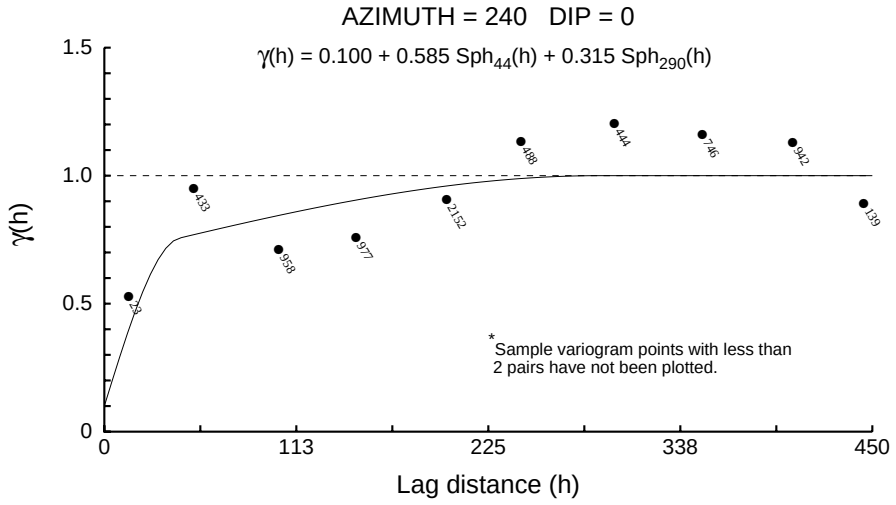

AZIMUTH = 120 DIP = 0
γ(h) = 0.100 + 0.585 Sph79(h) + 0.315 Sph148(h)
γ(h)
1.5
1.0
0.5
0
0
113
225
338
450
Lag distance (h)
19
424
788
962
2147
1162
406
325
851
830
*Sample variogram points with less than 2 pairs have not been plotted.


AZIMUTH = 150 DIP = 0
γ(h) = 0.100 + 0.585 Sph74(h) + 0.315 Sph127(h)
γ(h)
1.5
1.0
0.5
0
0
113
225
338
450
Lag distance (h)
25
308
1218
531
557
1261
346
1322
604
345
*Sample variogram points with less than 2 pairs have not been plotted.

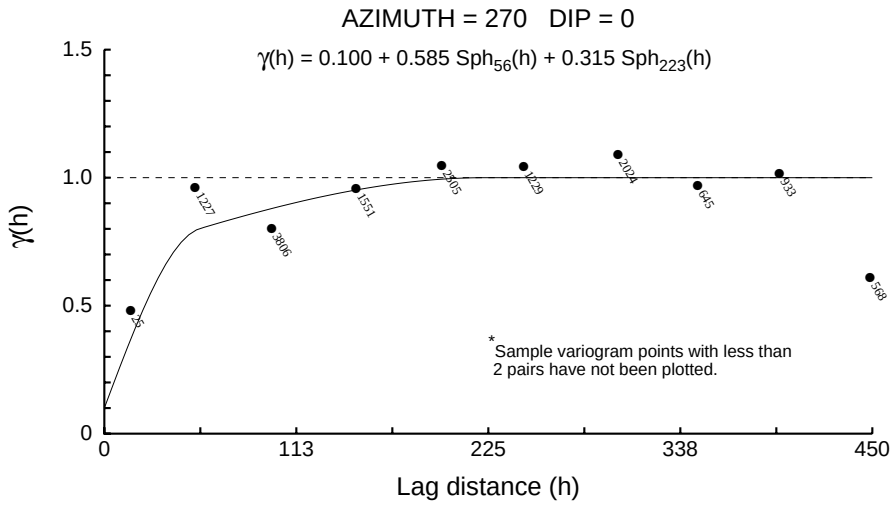
Cu - All Zones

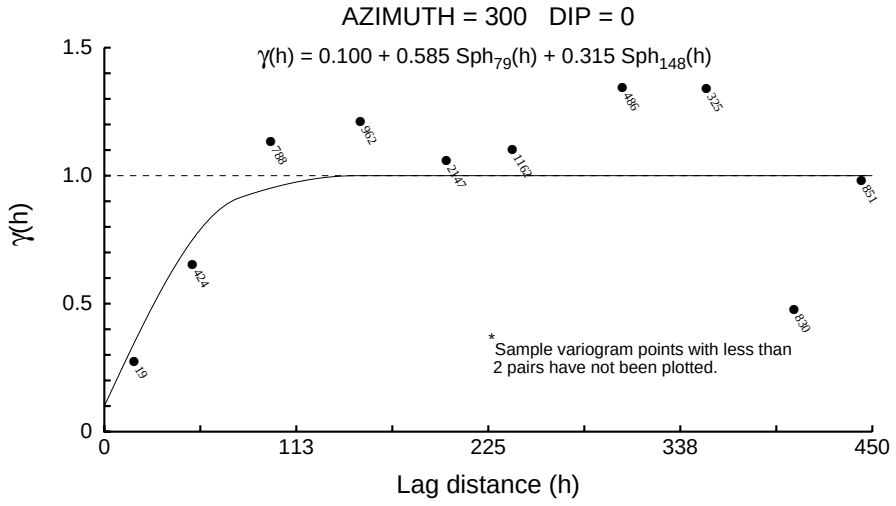

AZIMUTH = 180 DIP = 0
γ(h) = 0.100 + 0.585 Sph52(h) + 0.315 Sph136(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
38
1219
2648
599
1816
388
1554
89
271
696
*Sample variogram points with less than 2 pairs have not been plotted.

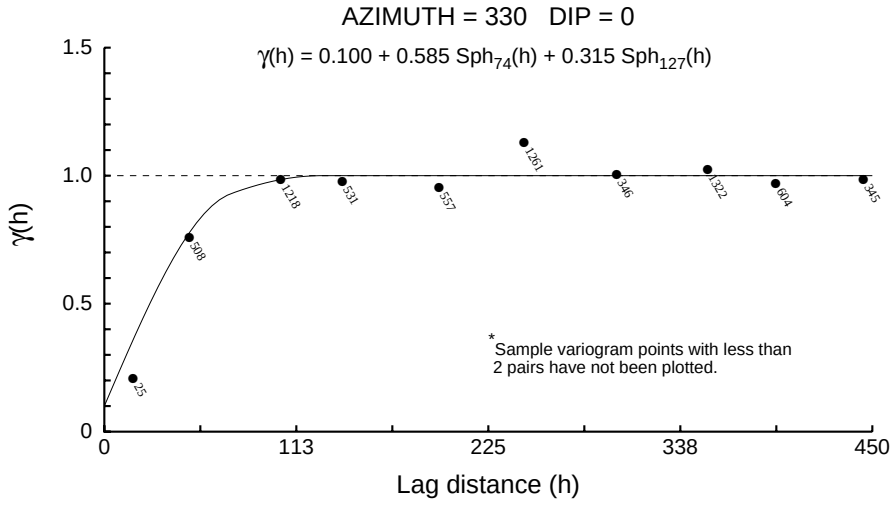

AZIMUTH = 210 DIP = 0
γ(h) = 0.100 + 0.585 Sph43(h) + 0.315 Sph186(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
36
539
1419
1254
690
1351
233
919
265
*Sample variogram points with less than 2 pairs have not been plotted.


AZIMUTH = 240 DIP = 0
γ(h) = 0.100 + 0.585 Sph44(h) + 0.315 Sph290(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
23
433
958
977
2152
488
444
746
942
139
*Sample variogram points with less than 2 pairs have not been plotted.

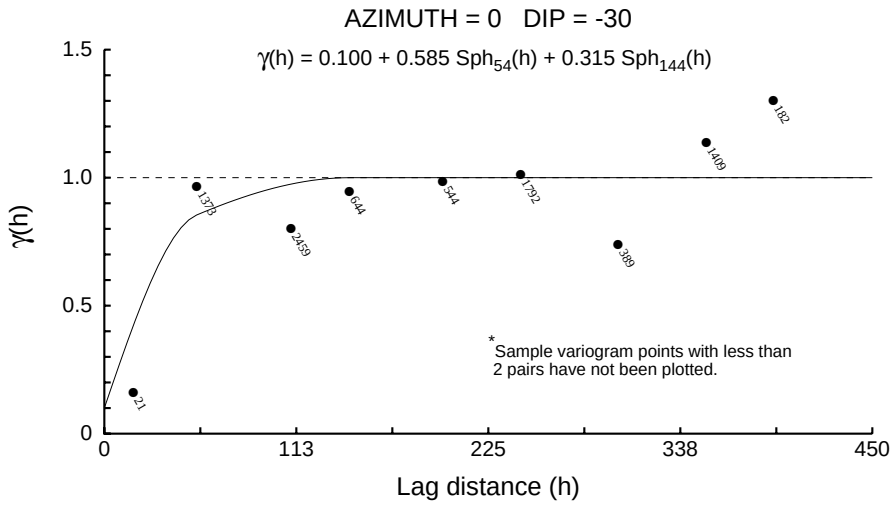
Cu - All Zones

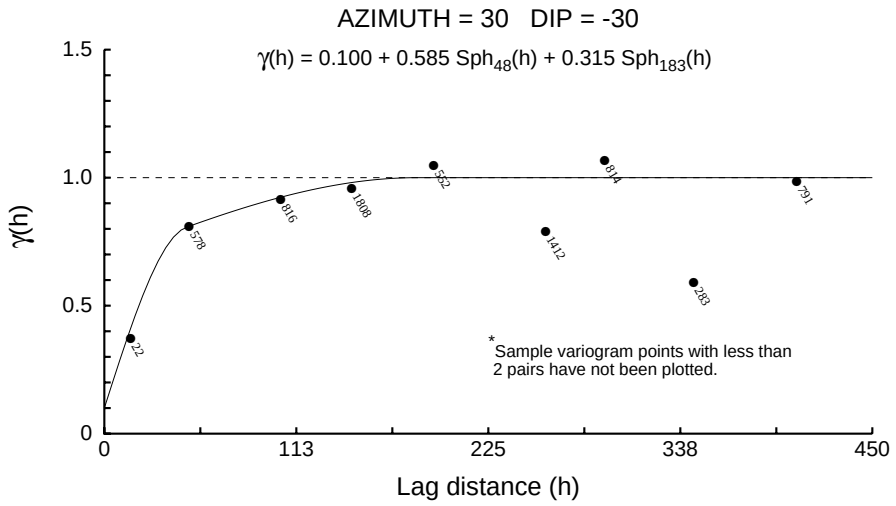

AZIMUTH = 270 DIP = 0
γ(h) = 0.100 + 0.585 Sph56(h) + 0.315 Sph223(h)
γ(h)
1.5
1.0
0.5
0
0
113
225
338
450
Lag distance (h)
35
1227
3806
1551
2005
1229
2024
645
933
568
*Sample variogram points with less than 2 pairs have not been plotted.

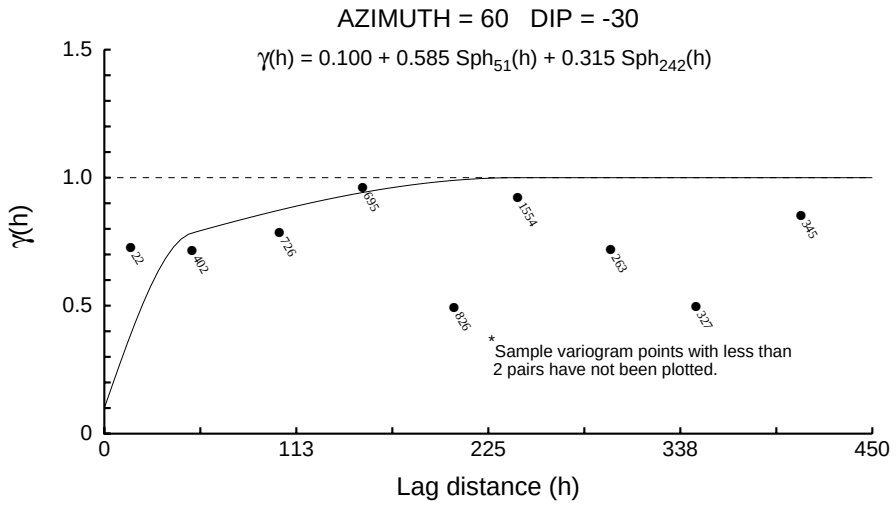

AZIMUTH = 300 DIP = 0
γ(h) = 0.100 + 0.585 Sph79(h) + 0.315 Sph148(h)
γ(h)
1.5
1.0
0.5
0
0
113
225
338
450
Lag distance (h)
19
424
788
962
2147
1162
406
325
851
830
*Sample variogram points with less than 2 pairs have not been plotted.


AZIMUTH = 330 DIP = 0
γ(h) = 0.100 + 0.585 Sph74(h) + 0.315 Sph127(h)
γ(h)
1.5
1.0
0.5
0
0
113
225
338
450
Lag distance (h)
25
308
1218
531
557
1261
346
1322
604
345
*Sample variogram points with less than 2 pairs have not been plotted.

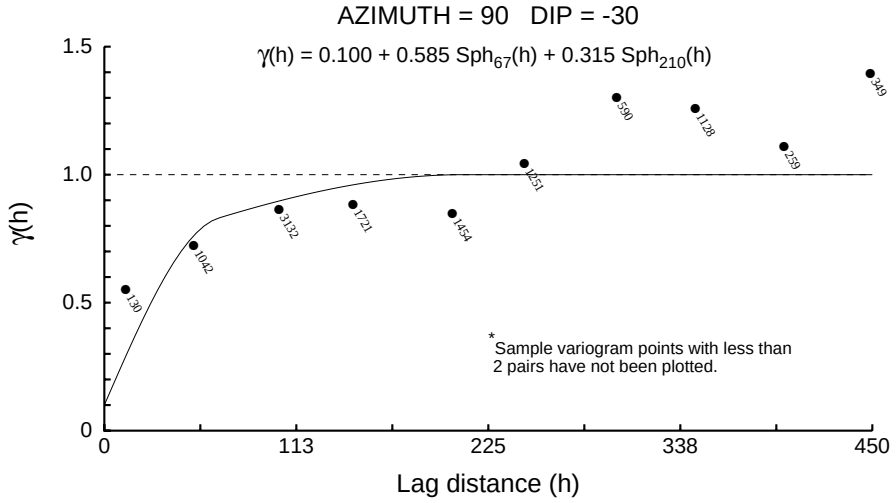
Cu - All Zones

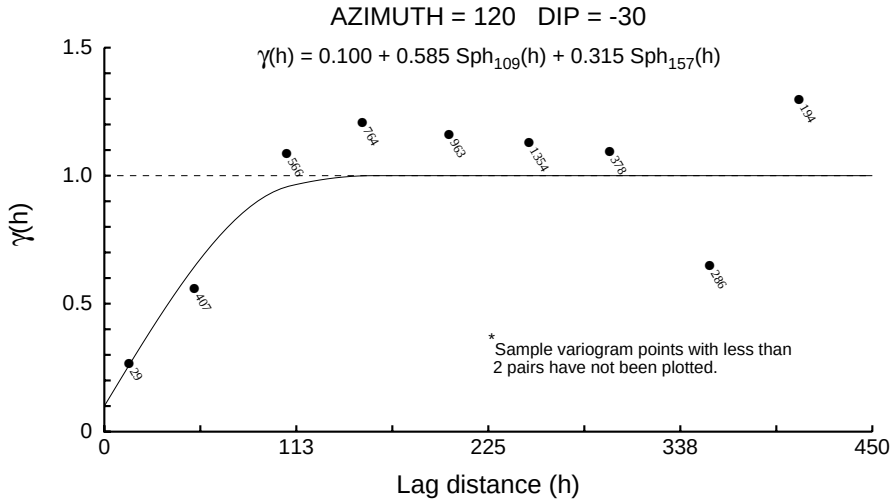

AZIMUTH = 0 DIP = -30
γ(h) = 0.100 + 0.585 Sph54(h) + 0.315 Sph144(h)
γ(h)
1.5
1.0
0.5
0
0
113
225
338
450
Lag distance (h)
21
1378
2459
644
544
1792
389
1409
182
*Sample variogram points with less than
2 pairs have not been plotted.

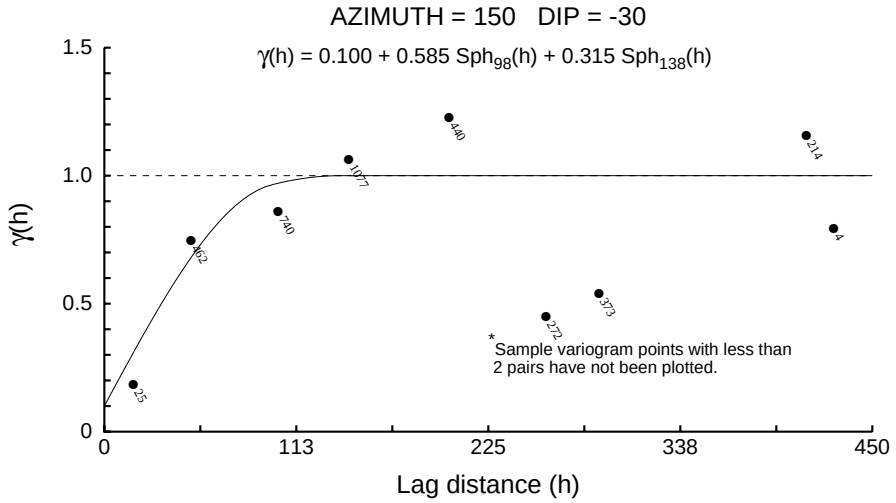

AZIMUTH = 30 DIP = -30
γ(h) = 0.100 + 0.585 Sph48(h) + 0.315 Sph183(h)
γ(h)
1.5
1.0
0.5
0
0
113
225
338
450
Lag distance (h)
22
578
816
1808
552
1412
283
814
791
*Sample variogram points with less than
2 pairs have not been plotted.


AZIMUTH = 60 DIP = -30
γ(h) = 0.100 + 0.585 Sph51(h) + 0.315 Sph242(h)
γ(h)
1.5
1.0
0.5
0
0
113
225
338
450
Lag distance (h)
22
402
726
895
826
1554
263
327
345
*Sample variogram points with less than
2 pairs have not been plotted.

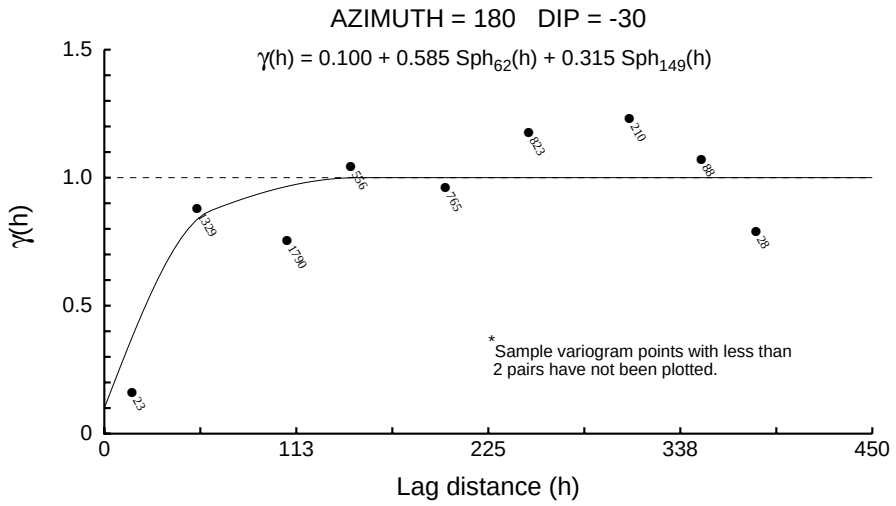
Cu - All Zones

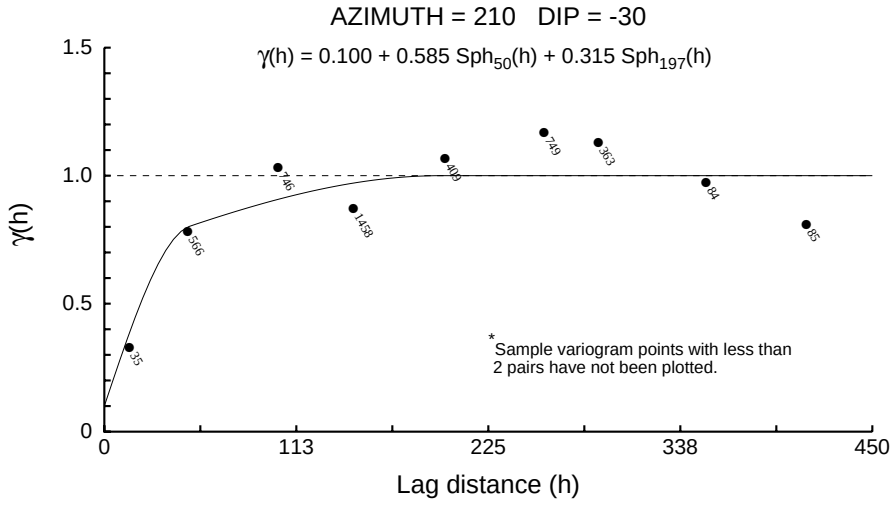

AZIMUTH = 90 DIP = -30
γ(h) = 0.100 + 0.585 Sph67(h) + 0.315 Sph210(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
130
1042
3132
1721
1454
1251
590
1128
259
349
*Sample variogram points with less than 2 pairs have not been plotted.

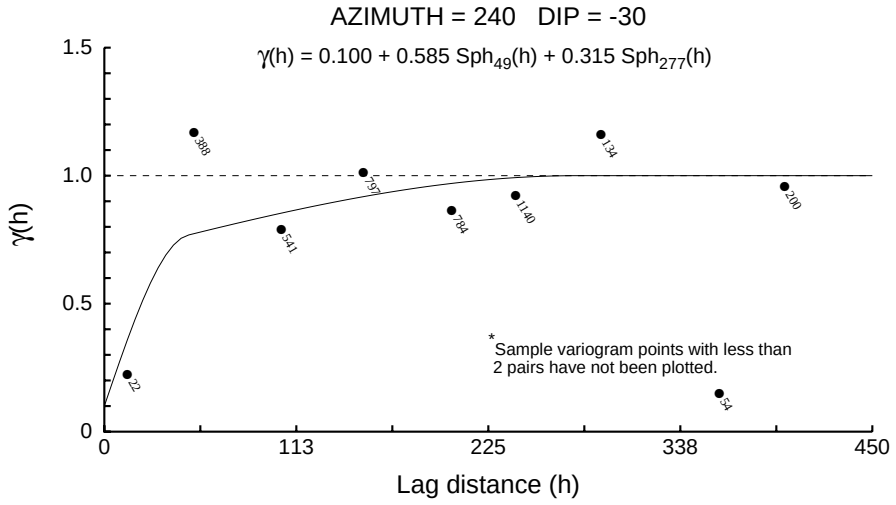

AZIMUTH = 120 DIP = -30
γ(h) = 0.100 + 0.585 Sph109(h) + 0.315 Sph157(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
29
407
906
764
963
1354
378
286
194
*Sample variogram points with less than 2 pairs have not been plotted.


AZIMUTH = 150 DIP = -30
γ(h) = 0.100 + 0.585 Sph98(h) + 0.315 Sph138(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
25
362
740
1077
440
272
373
214
74
*Sample variogram points with less than 2 pairs have not been plotted.

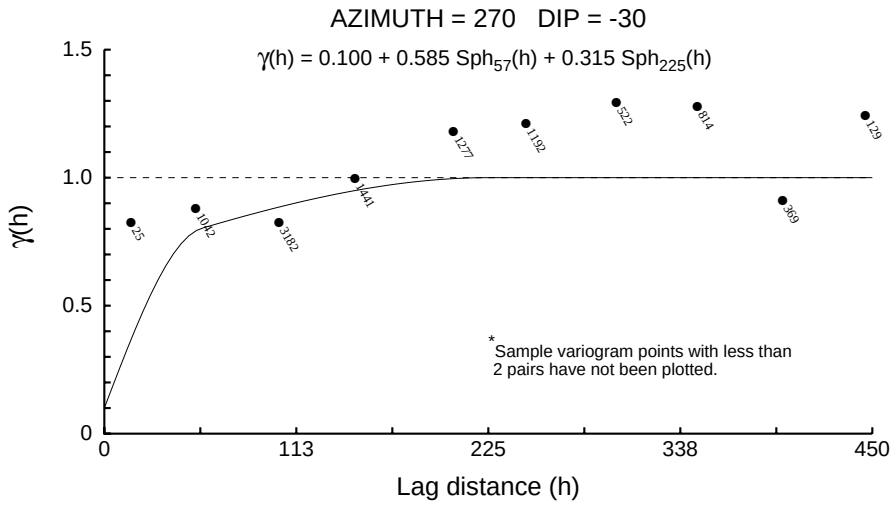
Cu - All Zones

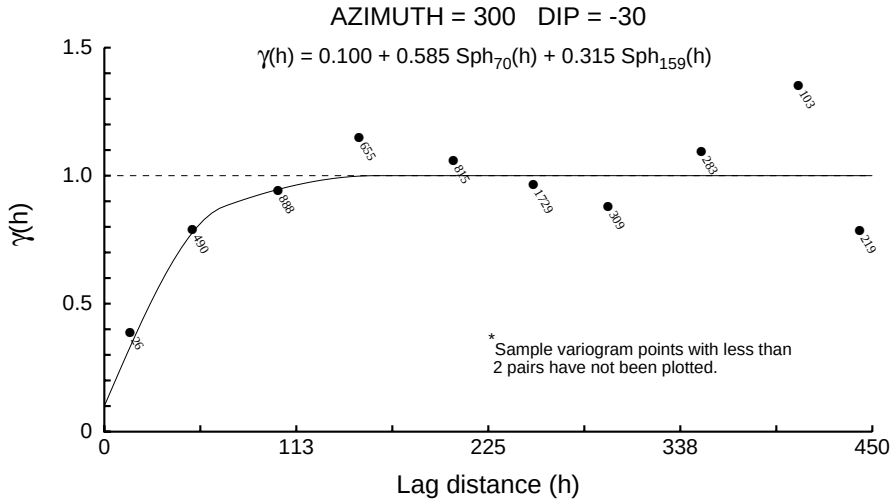

AZIMUTH = 180 DIP = -30
γ(h) = 0.100 + 0.585 Sph62(h) + 0.315 Sph149(h)
γ(h)
1.5
1.0
0.5
0
0
113
225
338
450
Lag distance (h)
23
329
1790
556
755
823
210
88
28
*Sample variogram points with less than 2 pairs have not been plotted.

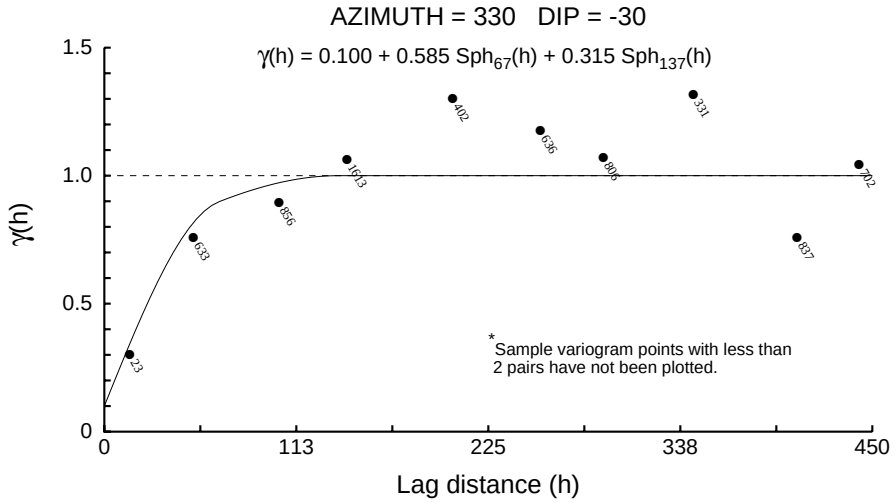

AZIMUTH = 210 DIP = -30
γ(h) = 0.100 + 0.585 Sph50(h) + 0.315 Sph197(h)
γ(h)
1.5
1.0
0.5
0
0
113
225
338
450
Lag distance (h)
35
566
746
1439
409
749
363
84
85
*Sample variogram points with less than 2 pairs have not been plotted.


AZIMUTH = 240 DIP = -30
γ(h) = 0.100 + 0.585 Sph49(h) + 0.315 Sph277(h)
γ(h)
1.5
1.0
0.5
0
0
113
225
338
450
Lag distance (h)
22
388
541
797
704
1140
134
200
54
*Sample variogram points with less than 2 pairs have not been plotted.

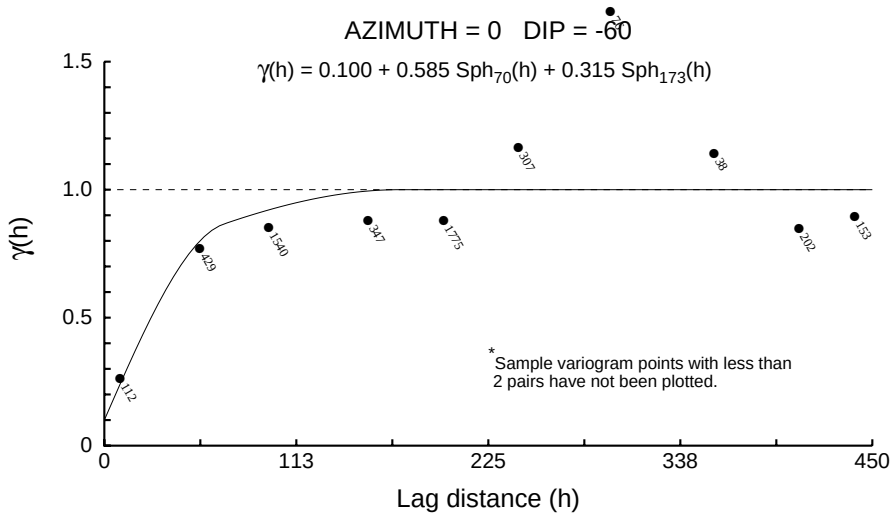
Cu - All Zones

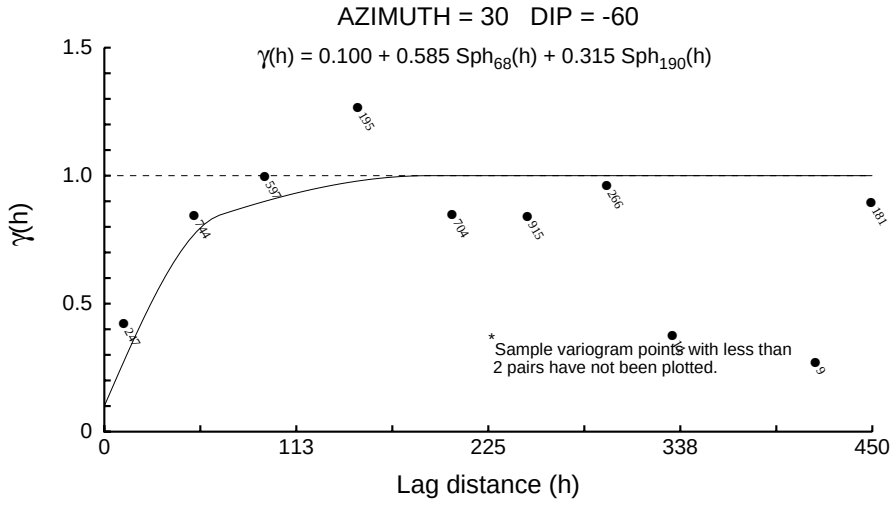

AZIMUTH = 270 DIP = -30
γ(h) = 0.100 + 0.585 Sph57(h) + 0.315 Sph225(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
25
1042
3182
9441
1277
1192
522
814
129
369
*Sample variogram points with less than
2 pairs have not been plotted.

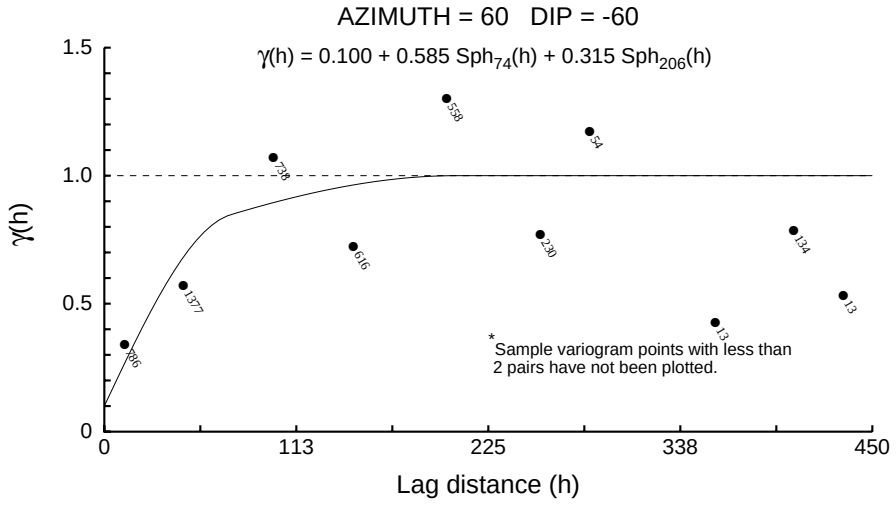

AZIMUTH = 300 DIP = -30
γ(h) = 0.100 + 0.585 Sph70(h) + 0.315 Sph159(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
26
490
888
6555
1075
1729
309
283
103
219
*Sample variogram points with less than
2 pairs have not been plotted.


AZIMUTH = 330 DIP = -30
γ(h) = 0.100 + 0.585 Sph67(h) + 0.315 Sph137(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
23
633
856
1613
402
636
806
331
702
837
*Sample variogram points with less than
2 pairs have not been plotted.

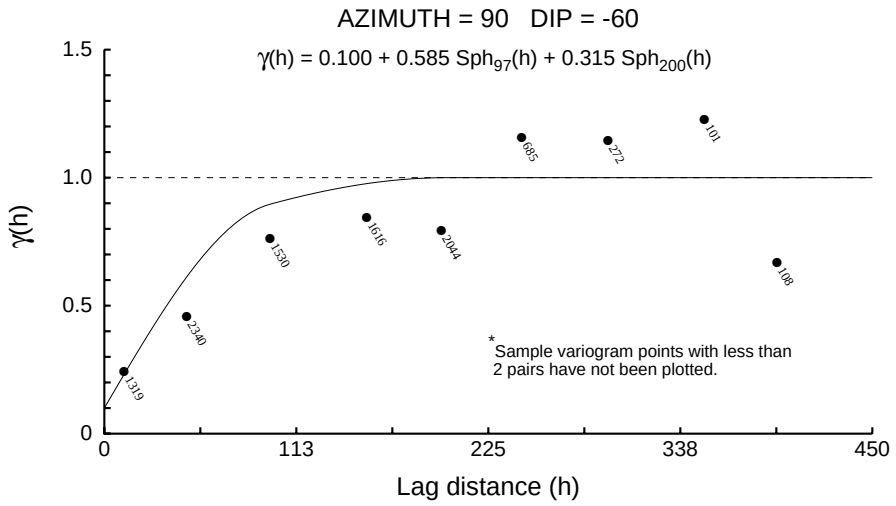
Cu - All Zones

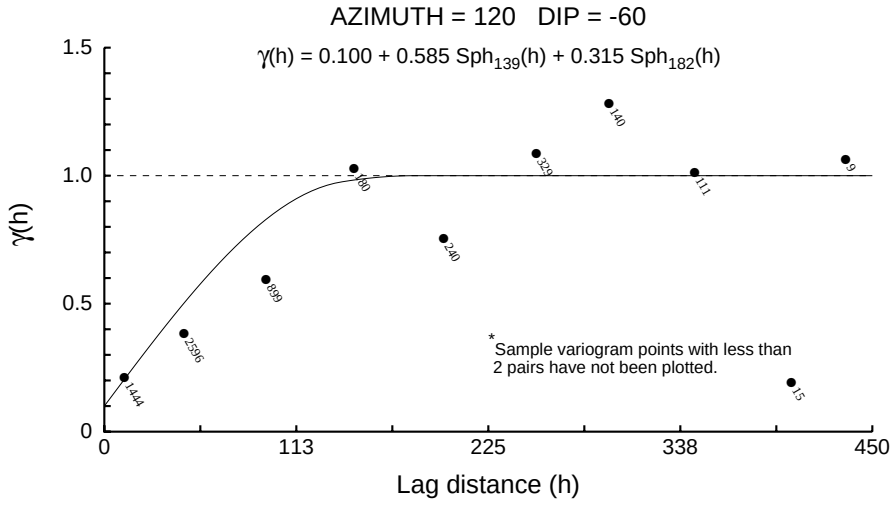

AZIMUTH = 0 DIP = -60
γ(h) = 0.100 + 0.585 Sph70(h) + 0.315 Sph173(h)
γ(h)
1.5
1.0
0.5
0
0
113
225
338
450
Lag distance (h)
307
38
1540
347
1775
429
202
153
112
*Sample variogram points with less than 2 pairs have not been plotted.

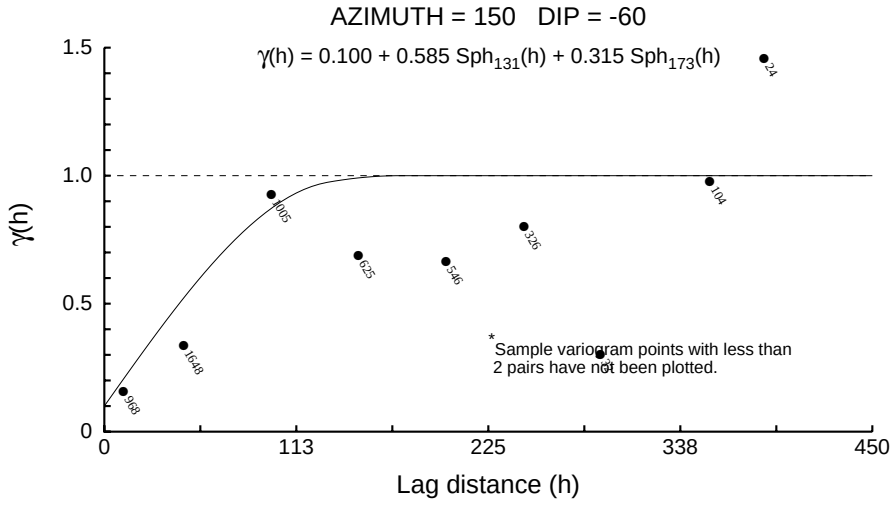

AZIMUTH = 30 DIP = -60
γ(h) = 0.100 + 0.585 Sph68(h) + 0.315 Sph190(h)
γ(h)
1.5
1.0
0.5
0
0
113
225
338
450
Lag distance (h)
195
597
744
704
915
266
181
242
*Sample variogram points with less than 2 pairs have not been plotted.


AZIMUTH = 60 DIP = -60
γ(h) = 0.100 + 0.585 Sph74(h) + 0.315 Sph206(h)
γ(h)
1.5
1.0
0.5
0
0
113
225
338
450
Lag distance (h)
558
54
738
616
230
134
1377
13
886
*Sample variogram points with less than 2 pairs have not been plotted.

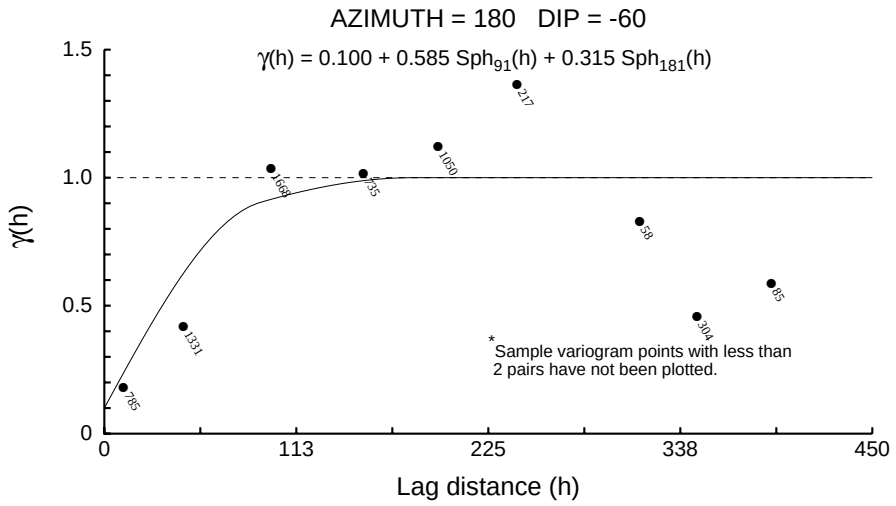
Cu - All Zones

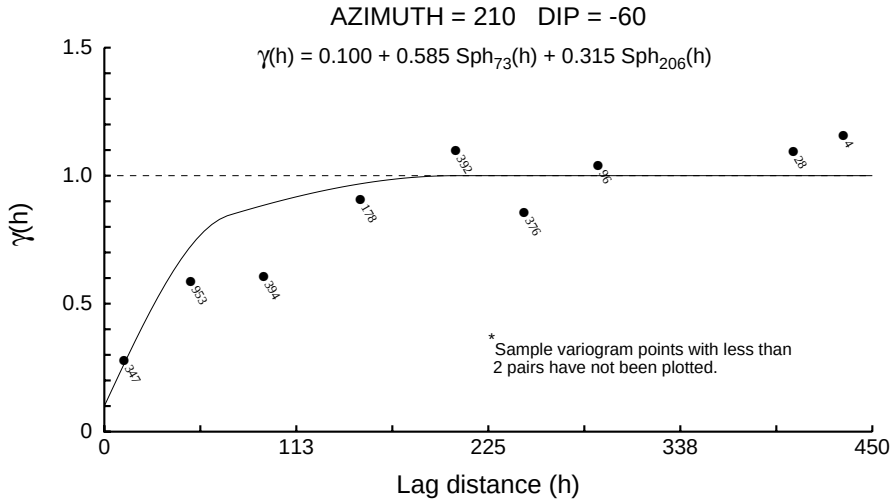

AZIMUTH = 90 DIP = -60
γ(h) = 0.100 + 0.585 Sph97(h) + 0.315 Sph200(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
1319
2340
1530
1616
2044
685
272
101
108
*Sample variogram points with less than 2 pairs have not been plotted.

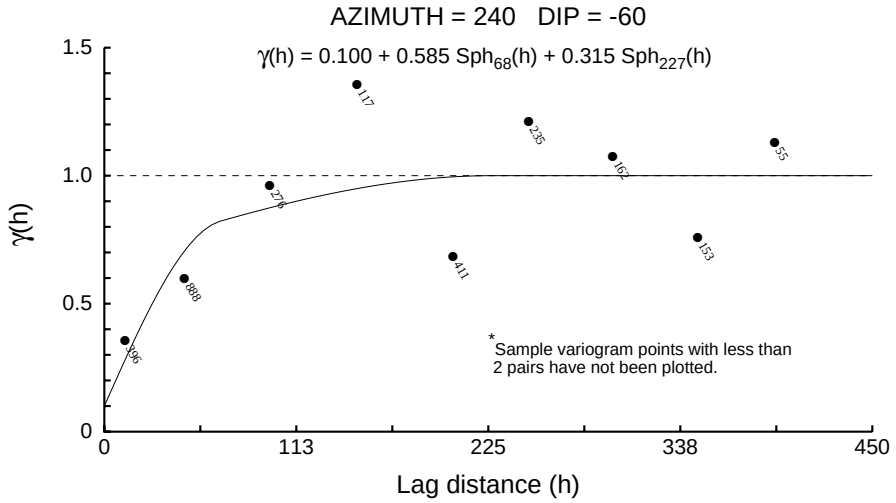

AZIMUTH = 120 DIP = -60
γ(h) = 0.100 + 0.585 Sph139(h) + 0.315 Sph182(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
1444
2596
899
1000
2240
140
329
111
9
15
*Sample variogram points with less than 2 pairs have not been plotted.


AZIMUTH = 150 DIP = -60
γ(h) = 0.100 + 0.585 Sph131(h) + 0.315 Sph173(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
968
1648
1005
625
546
326
104
24
*Sample variogram points with less than 2 pairs have not been plotted.

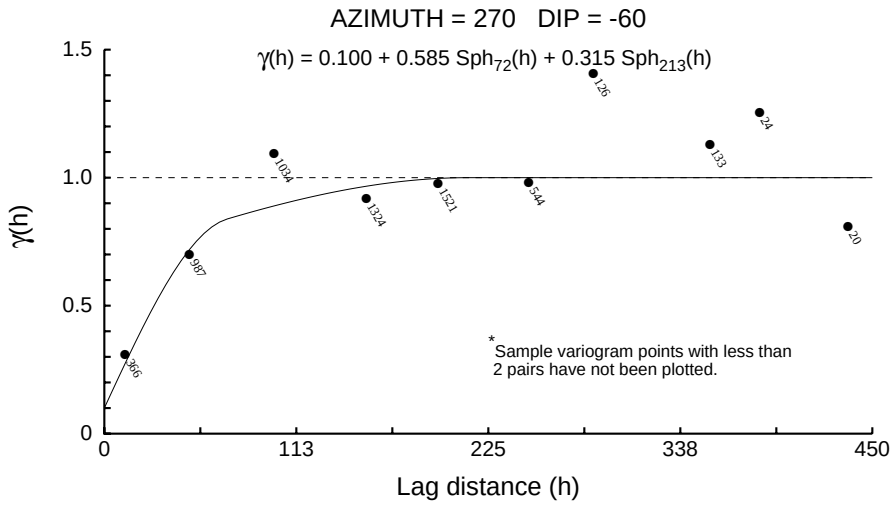
Cu - All Zones

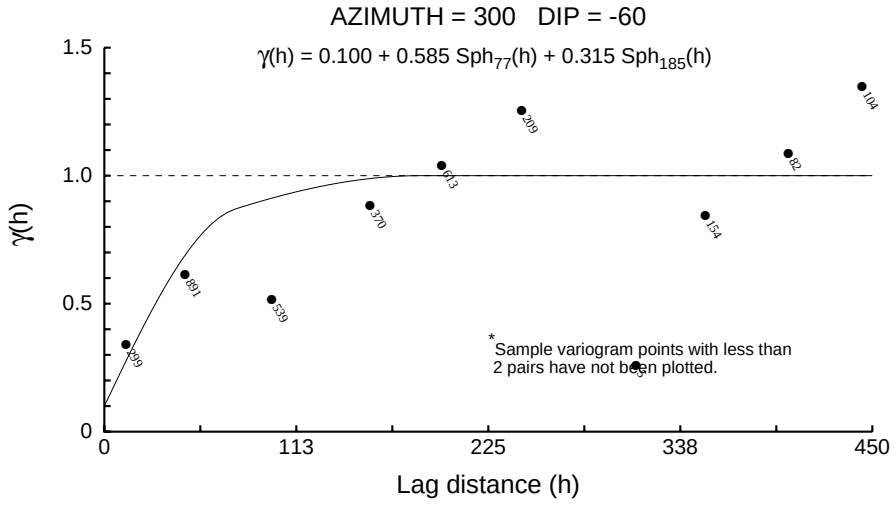

AZIMUTH = 180 DIP = -60
γ(h) = 0.100 + 0.585 Sph91(h) + 0.315 Sph181(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
217
1050
1668
735
58
85
304
1331
785
*Sample variogram points with less than 2 pairs have not been plotted.

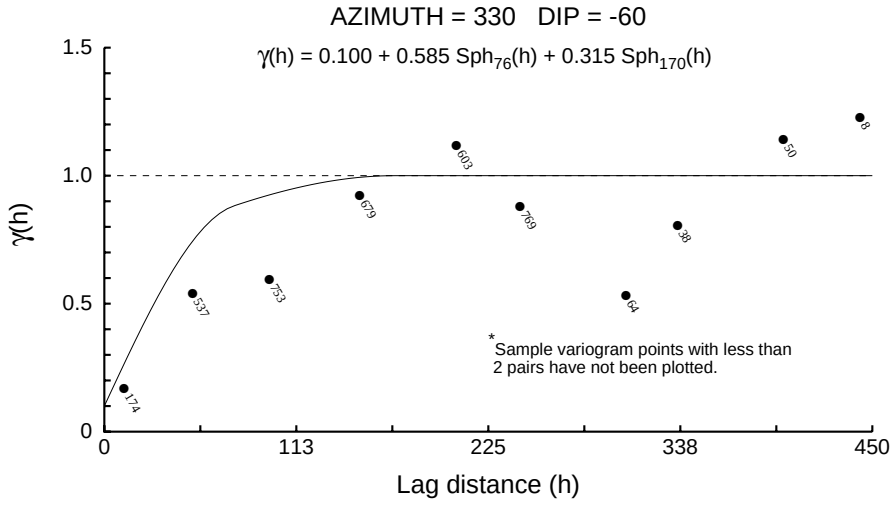

AZIMUTH = 210 DIP = -60
γ(h) = 0.100 + 0.585 Sph73(h) + 0.315 Sph206(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
4
392
96
29
178
376
953
394
347
*Sample variogram points with less than 2 pairs have not been plotted.


AZIMUTH = 240 DIP = -60
γ(h) = 0.100 + 0.585 Sph68(h) + 0.315 Sph227(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
117
235
55
162
276
411
153
888
196
*Sample variogram points with less than 2 pairs have not been plotted.

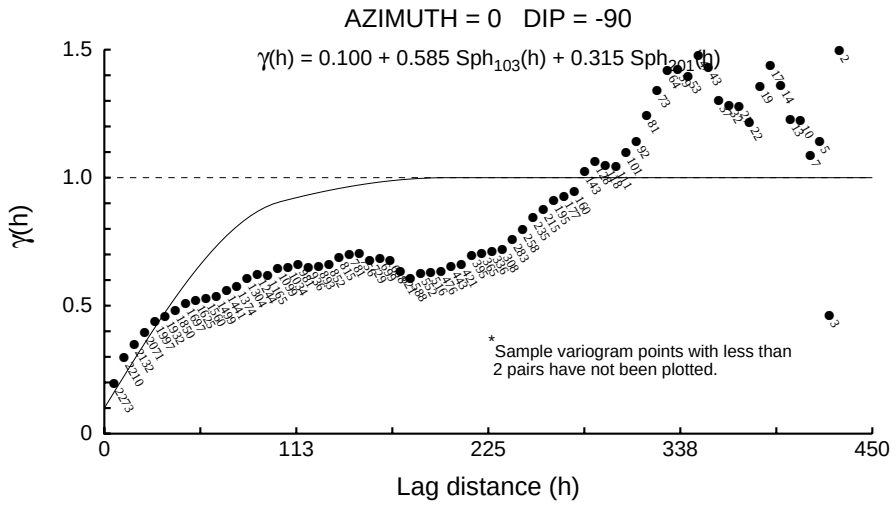
Cu - All Zones


AZIMUTH = 270 DIP = -60
γ(h) = 0.100 + 0.585 Sph72(h) + 0.315 Sph213(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
366
987
1034
1324
1521
544
126
133
24
20
*Sample variogram points with less than 2 pairs have not been plotted.


AZIMUTH = 300 DIP = -60
γ(h) = 0.100 + 0.585 Sph77(h) + 0.315 Sph185(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
299
891
539
370
613
209
154
82
104
*Sample variogram points with less than 2 pairs have not been plotted.


AZIMUTH = 330 DIP = -60
γ(h) = 0.100 + 0.585 Sph76(h) + 0.315 Sph170(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
174
537
753
679
603
769
64
38
50
8
*Sample variogram points with less than 2 pairs have not been plotted.

Cu - All Zones


AZIMUTH = 0 DIP = -90
γ(h) = 0.100 + 0.585 Sph103(h) + 0.315 Sph2010(h)
γ(h)
Lag distance (h)
0
0.5
1.0
1.5
0
113
225
338
450
*Sample variogram points with less than
2 pairs have not been plotted.

Cu - All Zones

User Defined Rotation Conventions

Nugget ==> 0.100
C1 ==> 0.585
C2 ==> 0.315

First Structure -- Spherical

RH Rotation about the Z axis ==> -42
RH Rotation about the Y' axis ==> -36
RH Rotation about the Z' axis ==> -89
Range along the Z' axis ==> 150 Azimuth ==> 312 Dip ==> 54
Range along the Y' axis ==> 72 Azimuth ==> 131 Dip ==> 35
Range along the X' axis ==> 43 Azimuth ==> 221 Dip ==> 0

Second Structure -- Spherical

RH Rotation about the Z axis ==> 16
RH Rotation about the Y' axis ==> -10
RH Rotation about the Z' axis ==> 8
Range along the Z' axis ==> 200 Azimuth ==> 254 Dip ==> 81
Range along the Y' axis ==> 126 Azimuth ==> 336 Dip ==> -1
Range along the X' axis ==> 301 Azimuth ==> 65 Dip ==> 9

Modeling Criteria

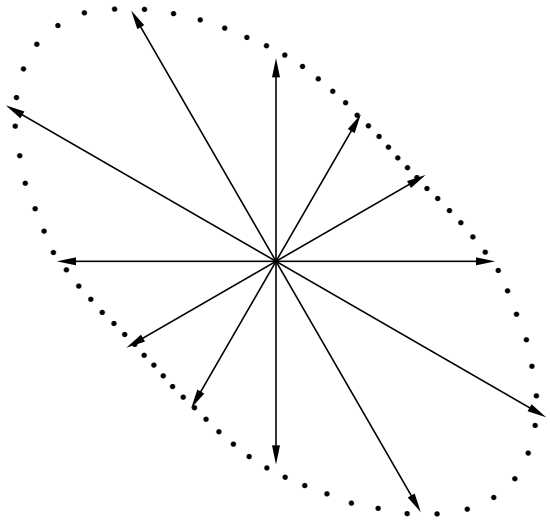
Minimum number pairs req'd ==> 2
Sample variogram points weighted by # pairs

Cu - All Zones

Structure Number 1

Rose Diagram of Ranges Dipping 0 Degrees
Scale:

100 Units

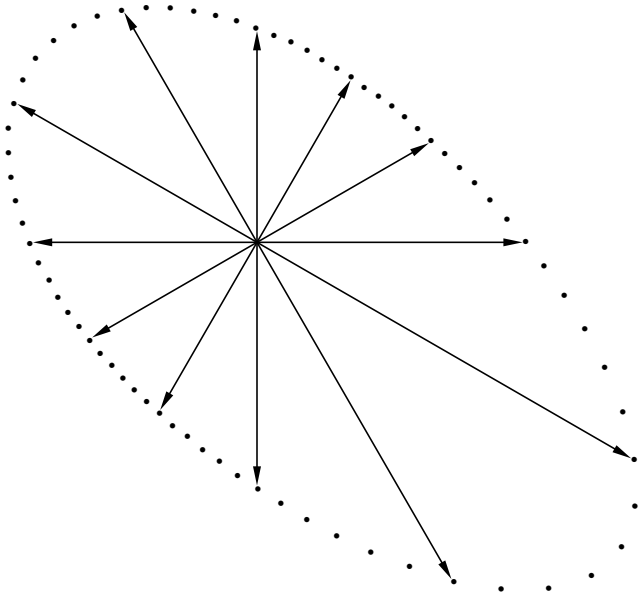


Cu - All Zones

Structure Number 1

Rose Diagram of Ranges Dipping 30 Degrees
Scale:

100 Units

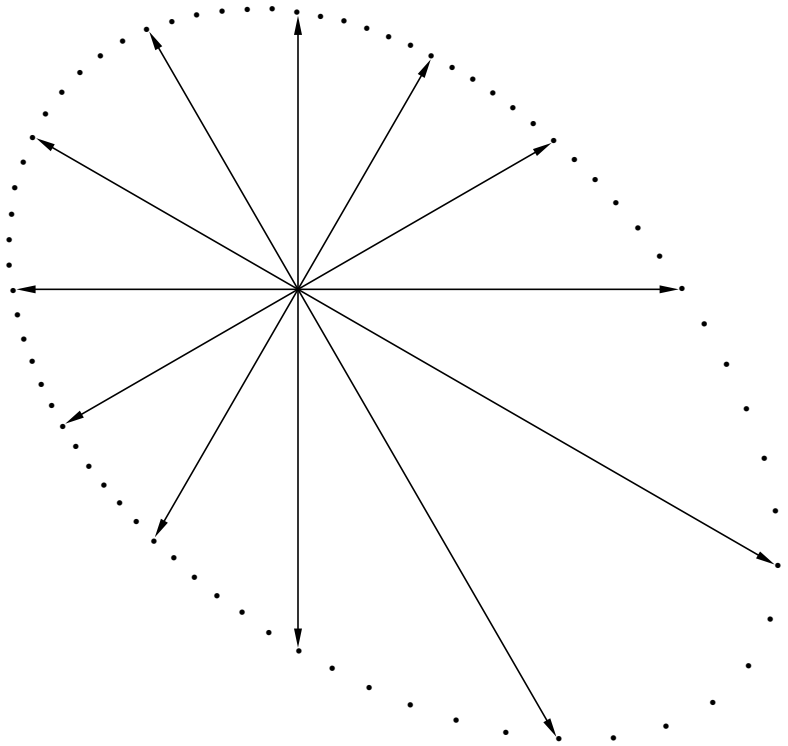


Cu - All Zones

Structure Number 1

Rose Diagram of Ranges Dipping 60 Degrees
Scale:

100 Units

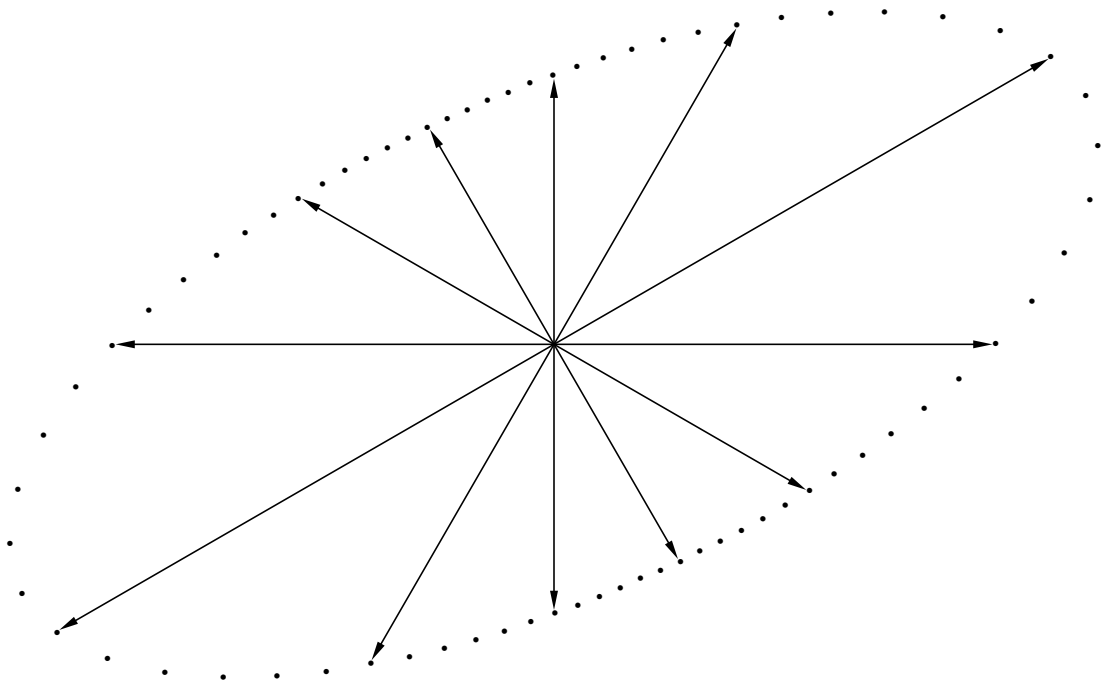


Cu - All Zones

Structure Number 2

Rose Diagram of Ranges Dipping 0 Degrees
Scale:

300 Units

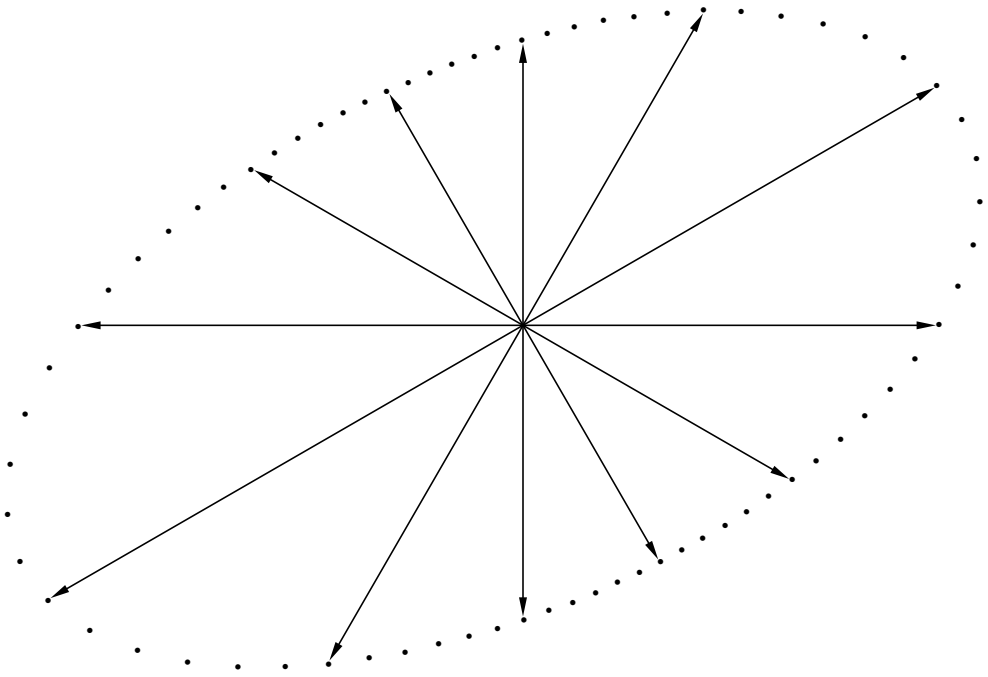


Cu - All Zones

Structure Number 2

Rose Diagram of Ranges Dipping 30 Degrees
Scale:

300 Units

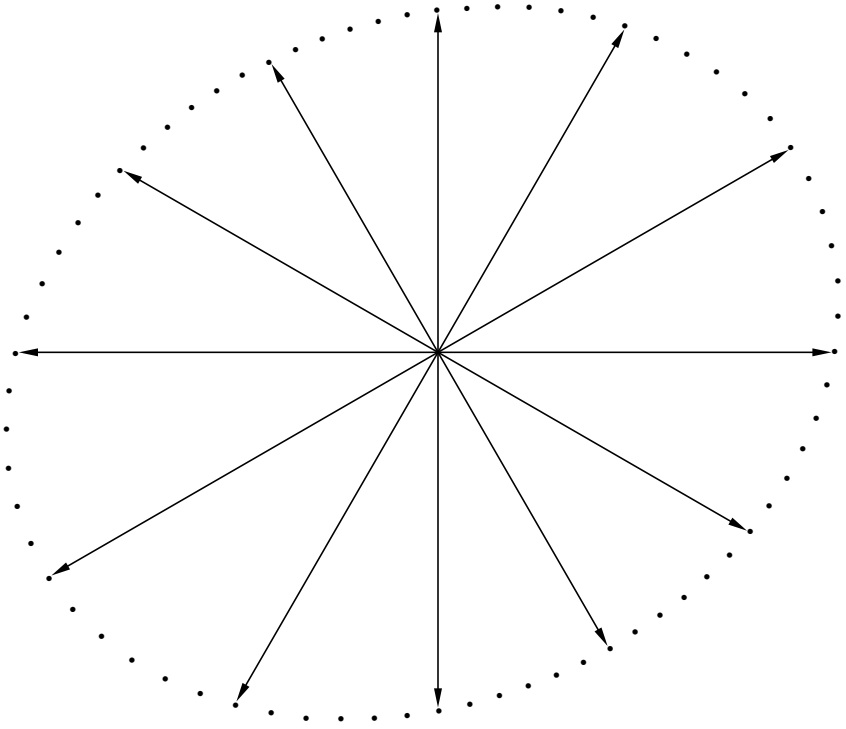


Cu - All Zones

Structure Number 2

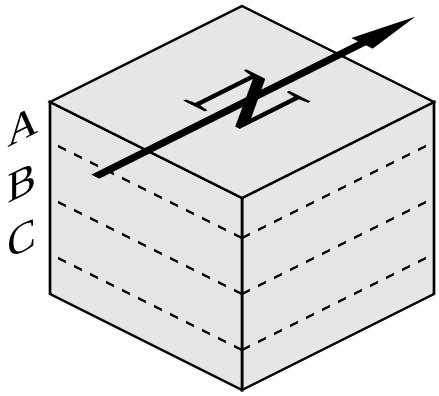
Rose Diagram of Ranges Dipping 60 Degrees
Scale:

300 Units

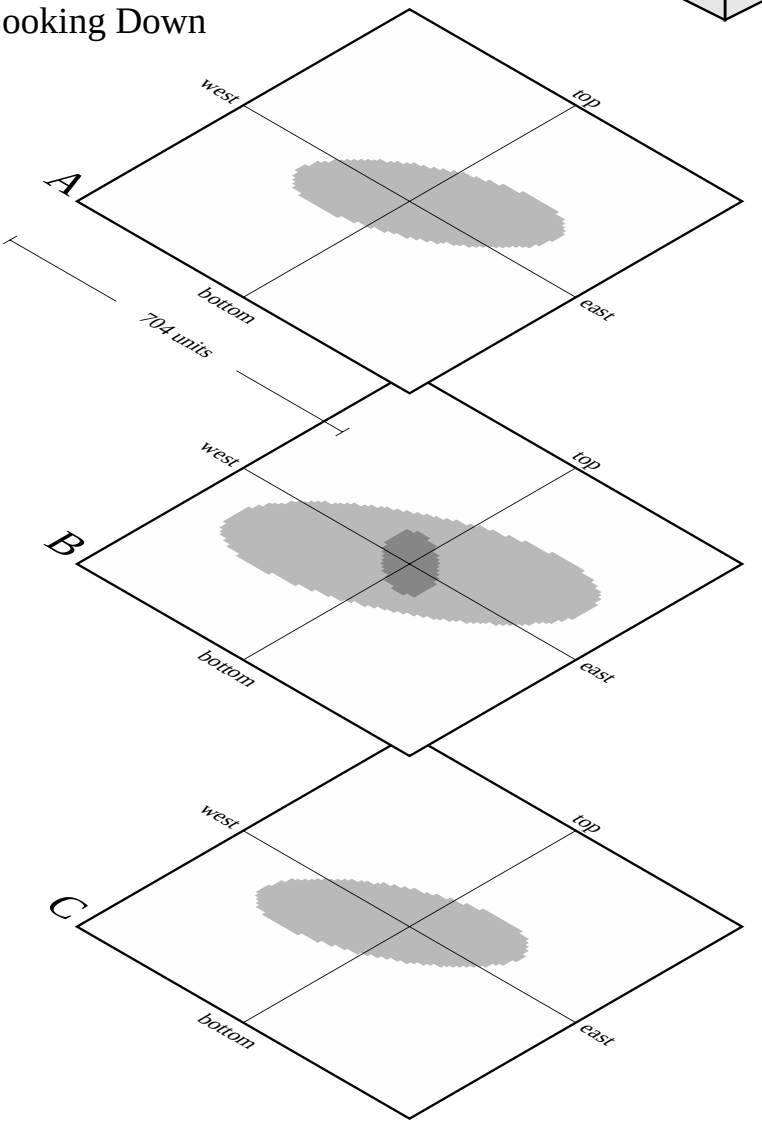


Horizontal Slices Through the Ellipsoids

Reference Cube



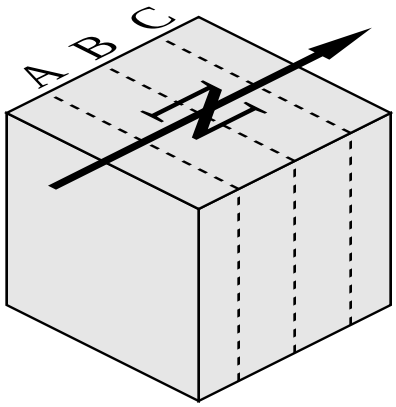
X-Y Planes Looking Down



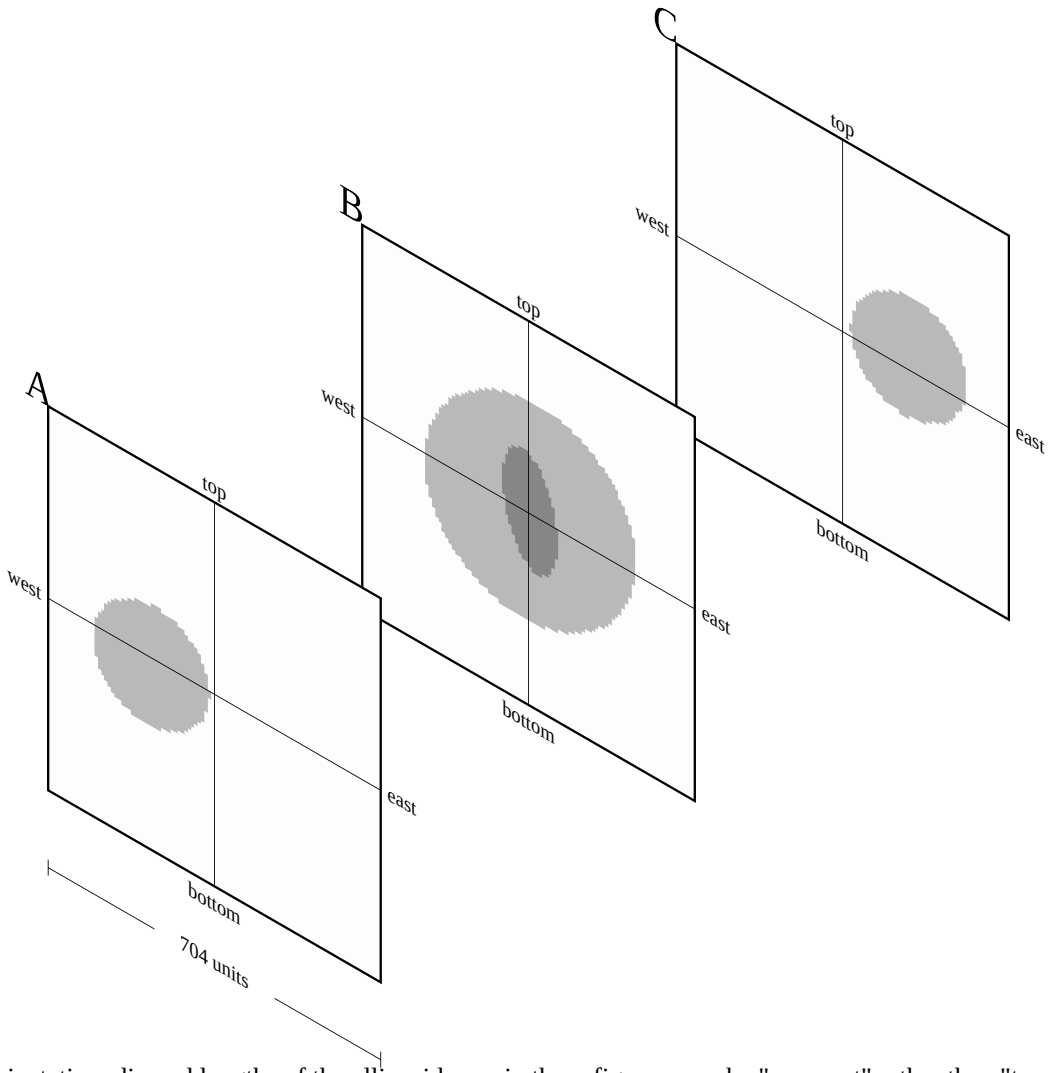
Note -- the orientation, dip and lengths of the ellipsoid axes in these figures may be "apparent" rather than "true".

Cross Section Views Through the Ellipsoids

Reference Cube



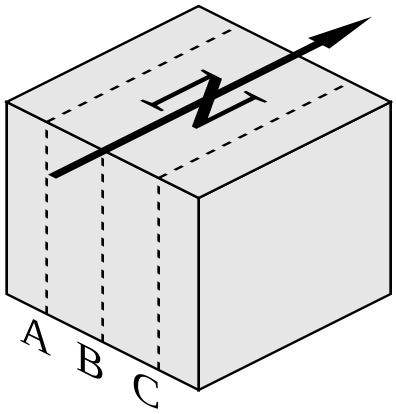
X-Z Planes Looking North



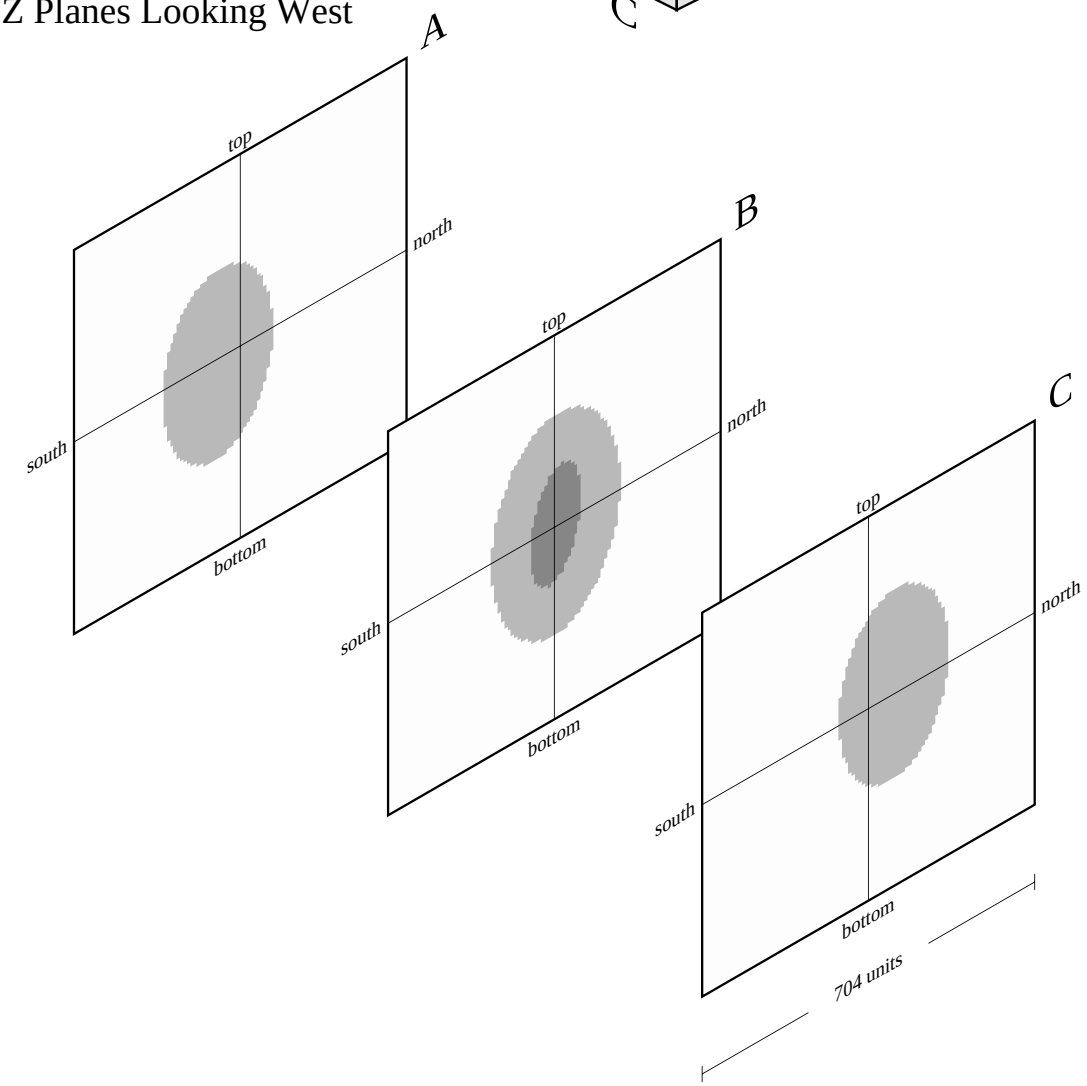
Note -- the orientation, dip and lengths of the ellipsoid axes in these figures may be "apparent" rather than "true".

Long Section Views Through the Ellipsoids

Reference Cube

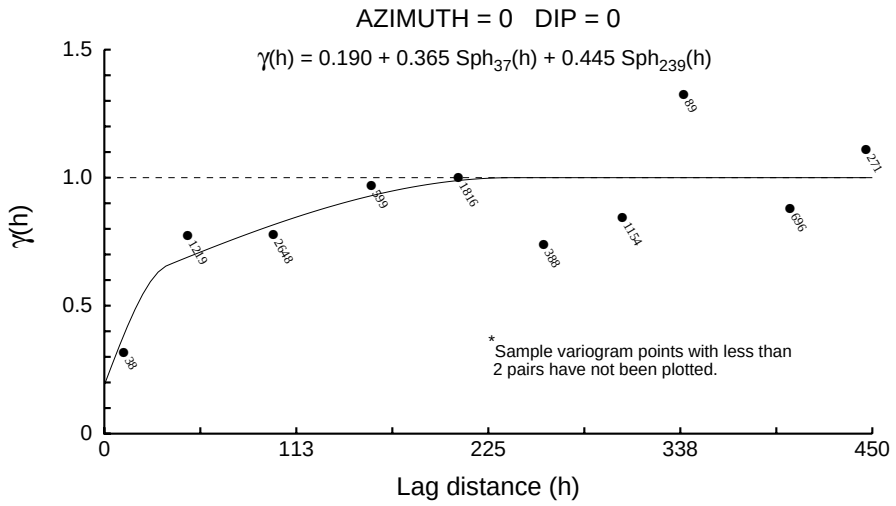


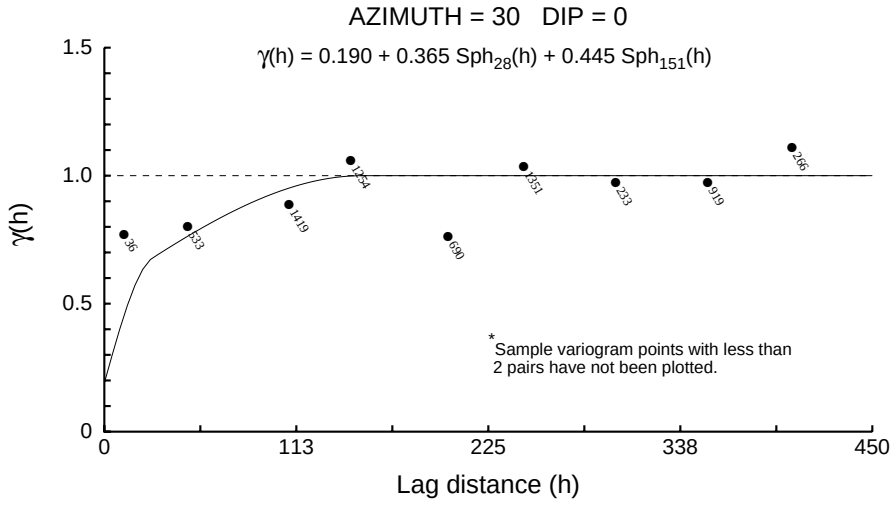
Y-Z Planes Looking West

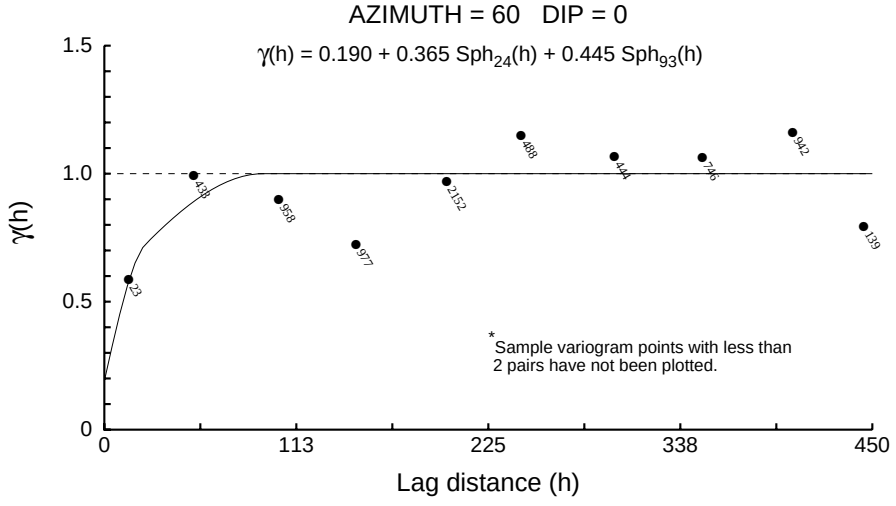


Note -- the orientation, dip and lengths of the ellipsoid axes in these figures may be "apparent" rather than "true".

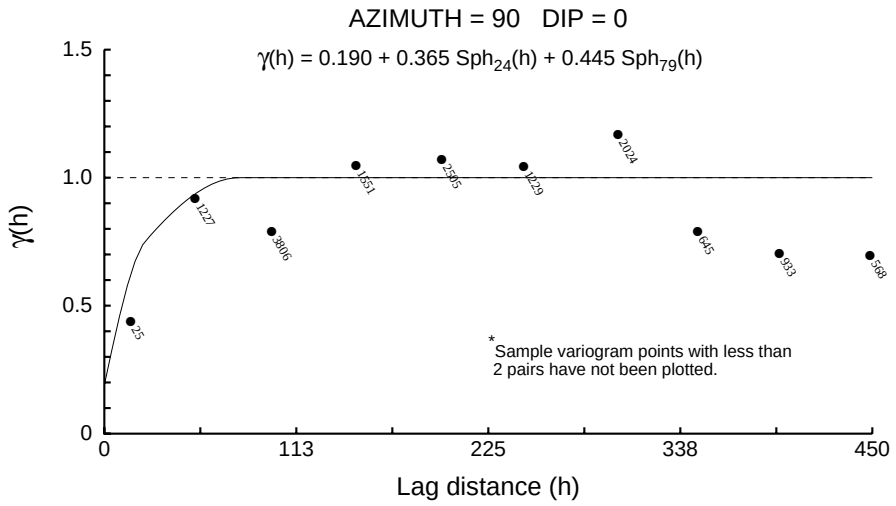
Uncapped Au - All Zones

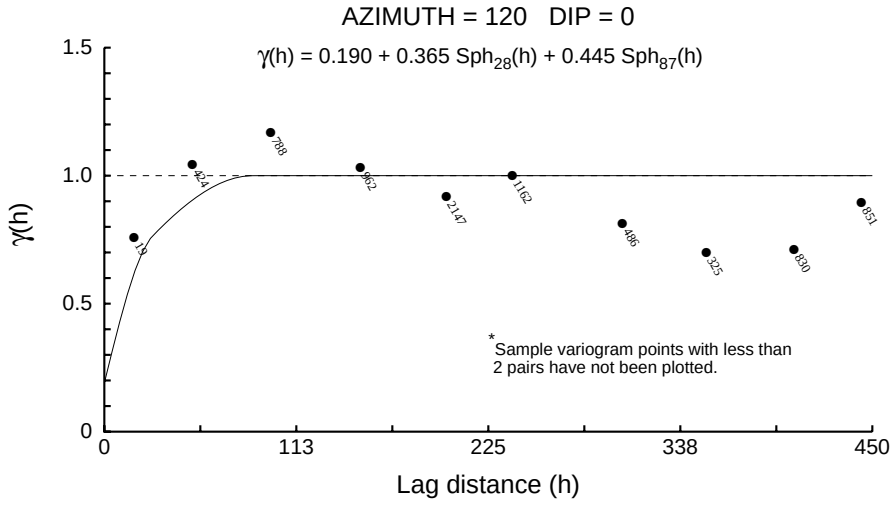


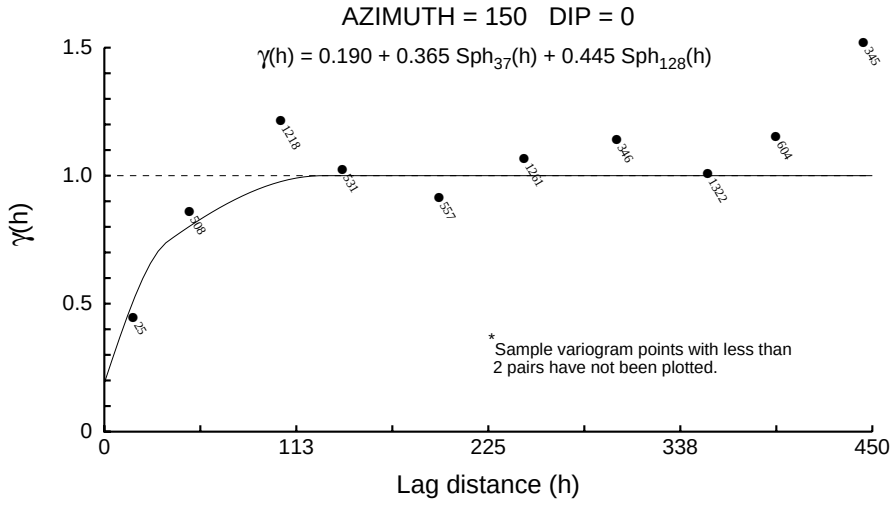




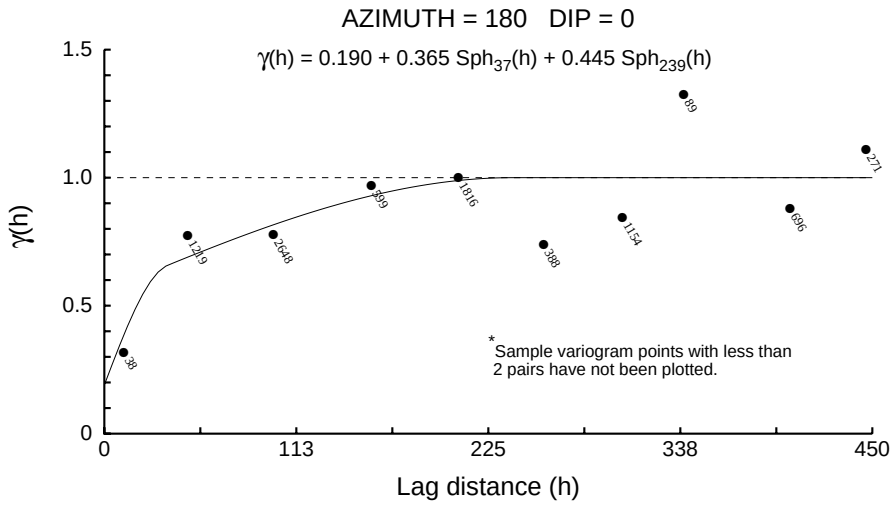
Uncapped Au - All Zones

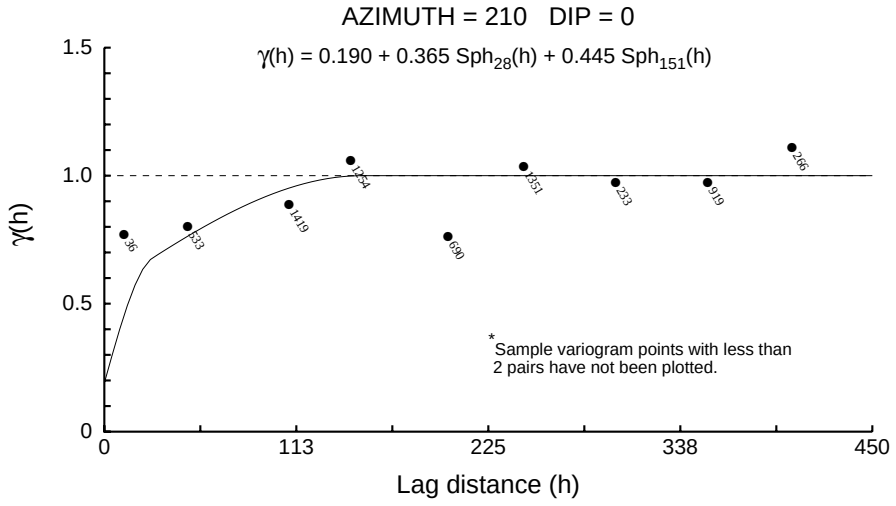


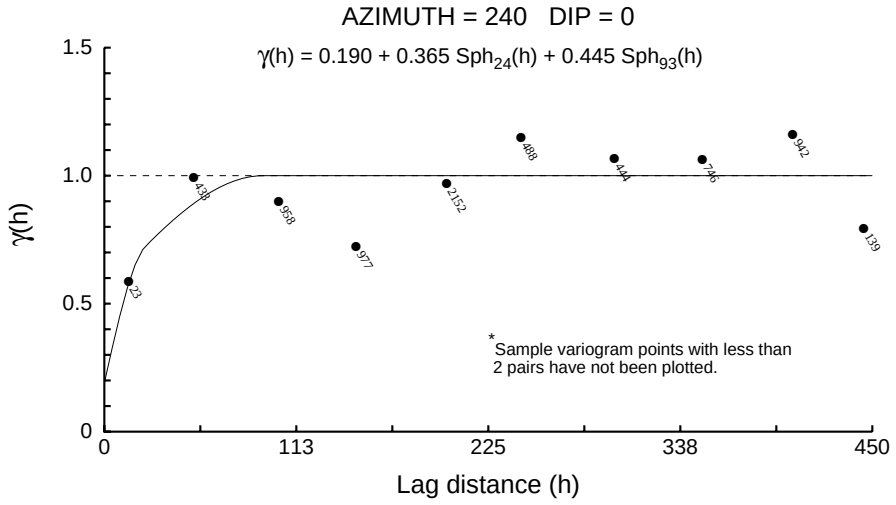




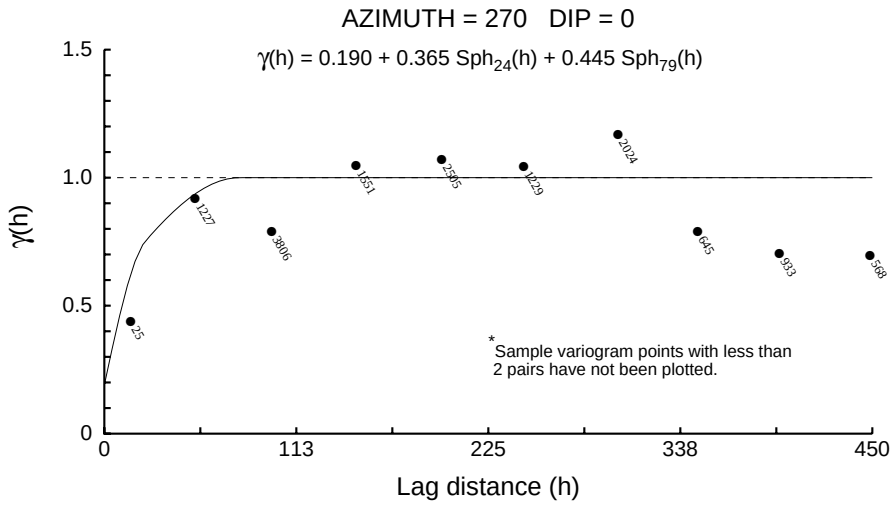
Uncapped Au - All Zones

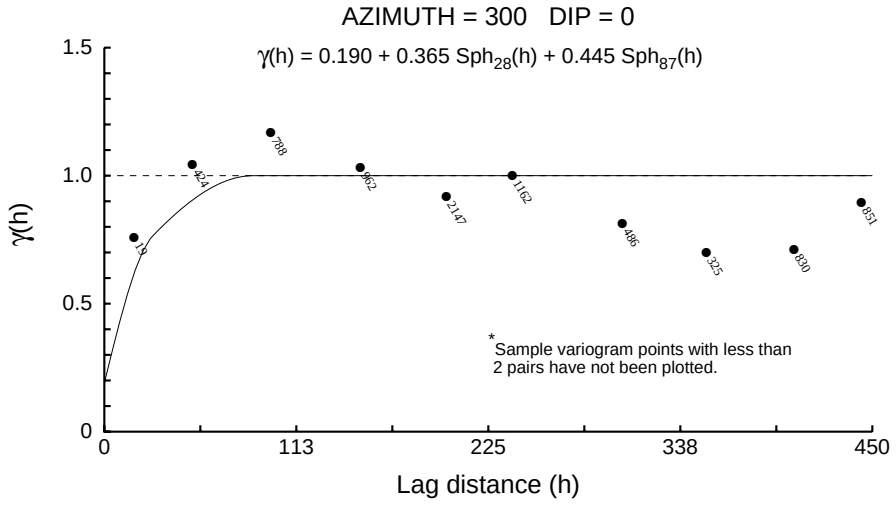


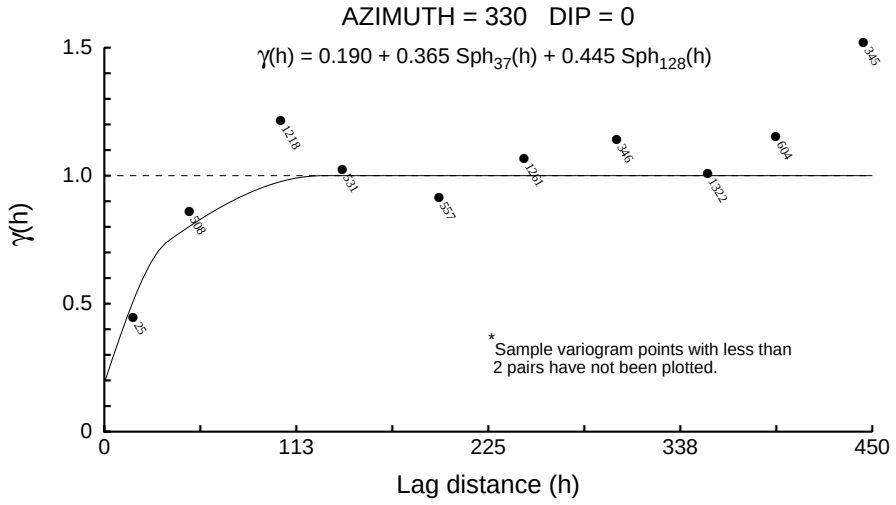




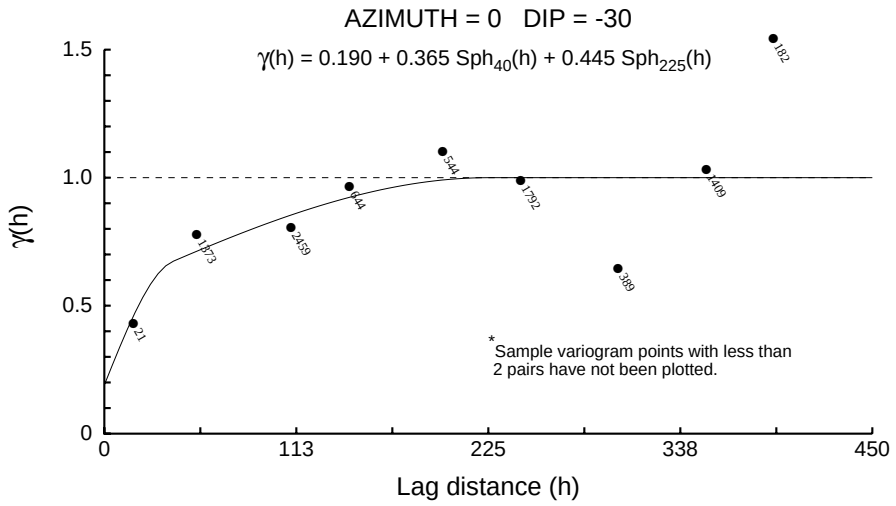
Uncapped Au - All Zones

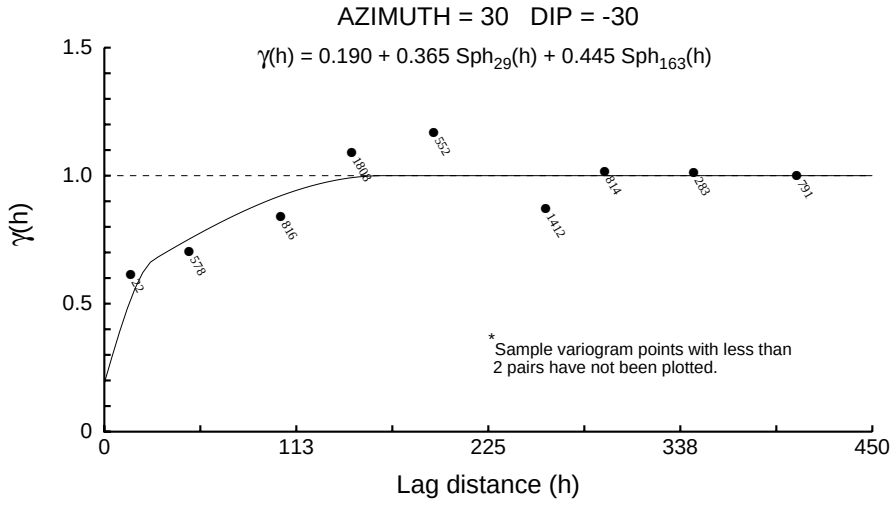


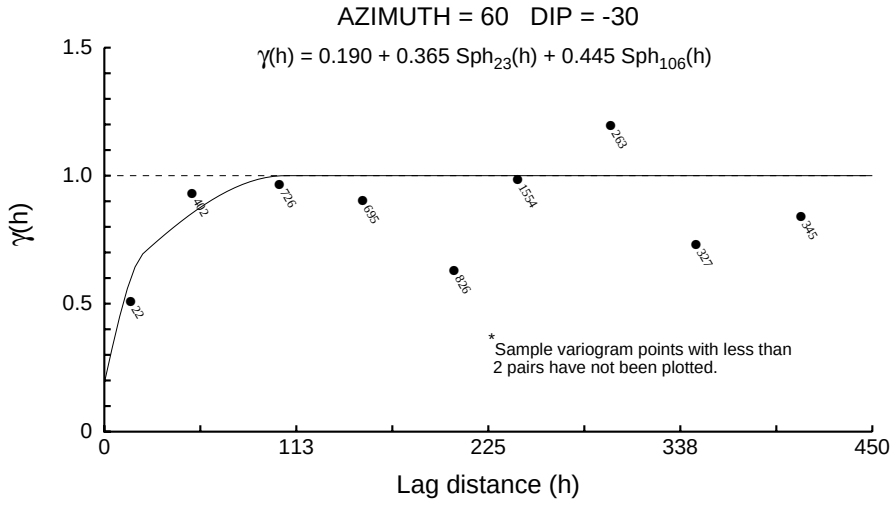




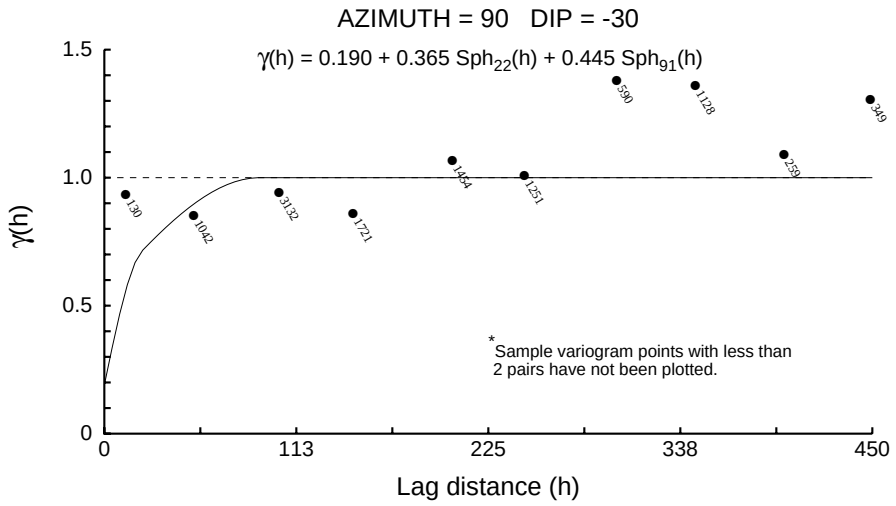
Uncapped Au - All Zones

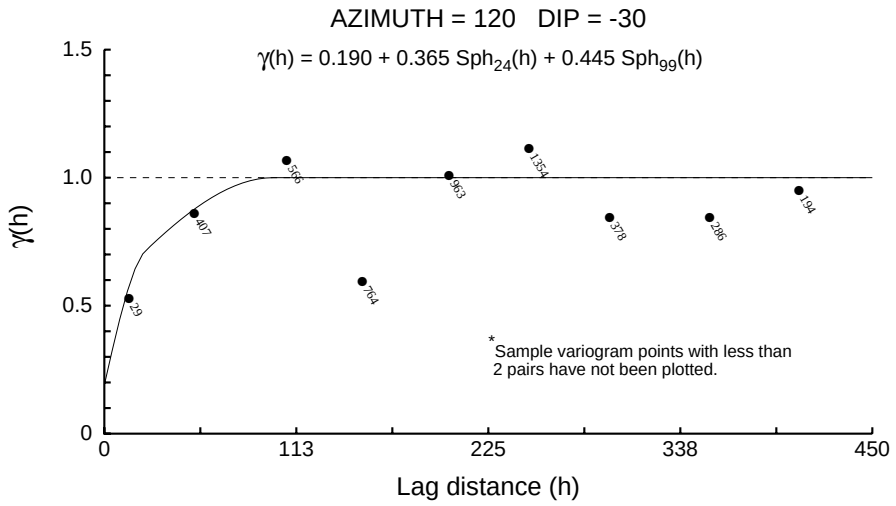


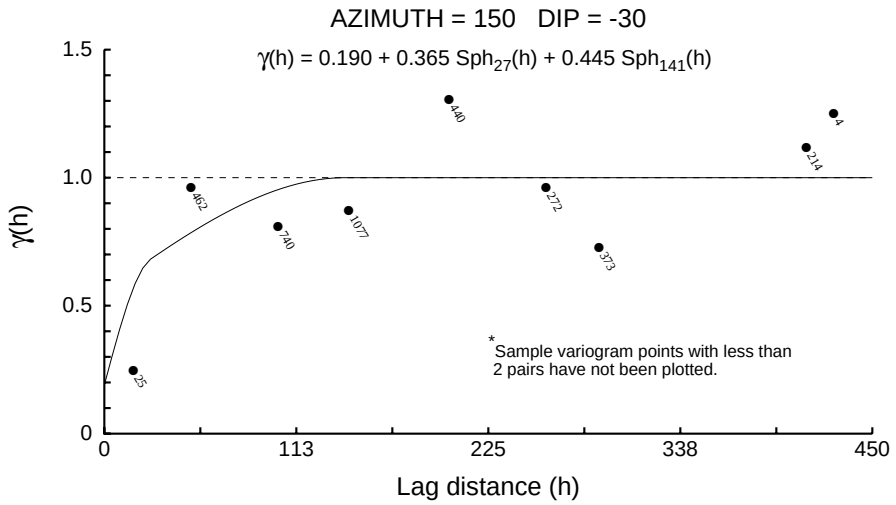




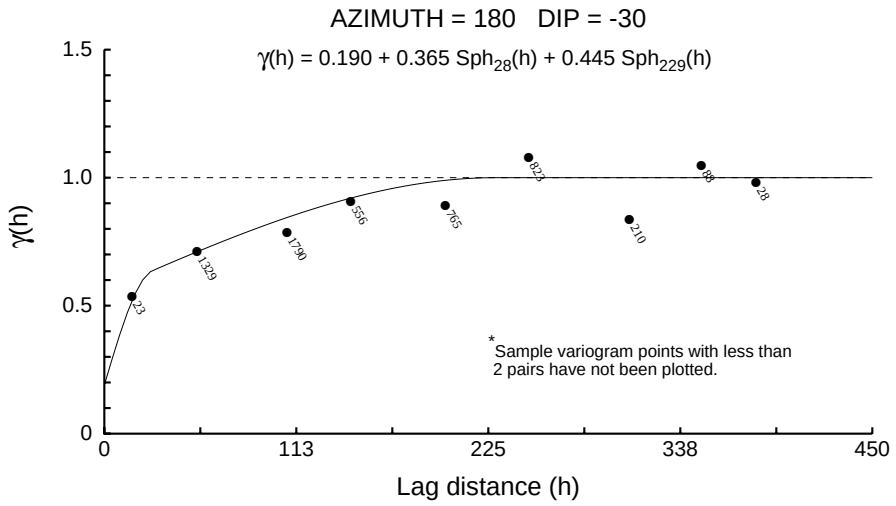
Uncapped Au - All Zones

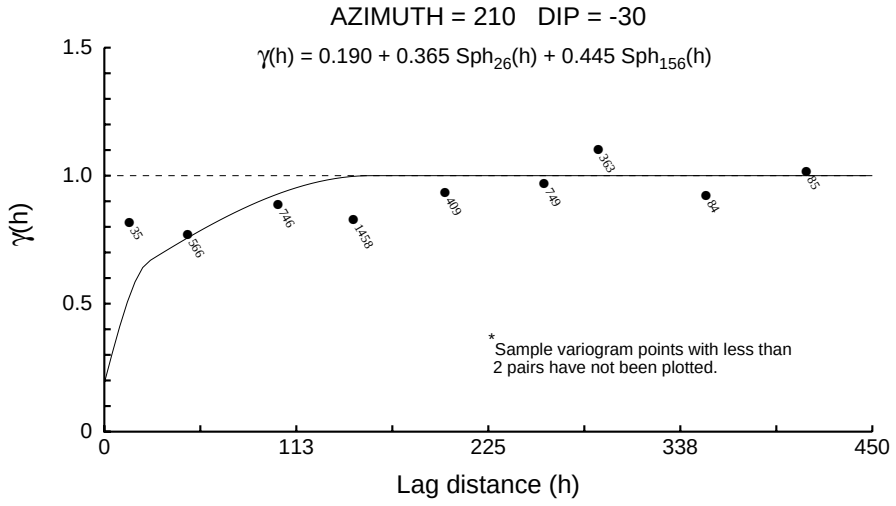


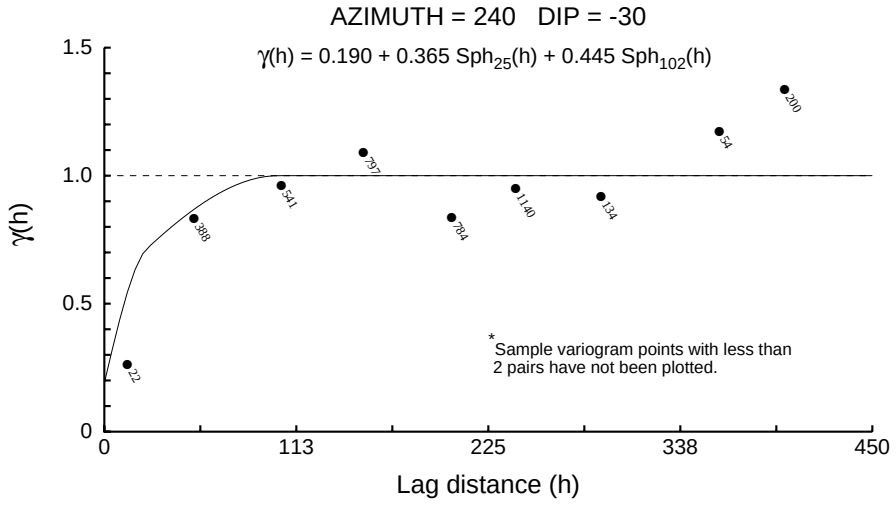




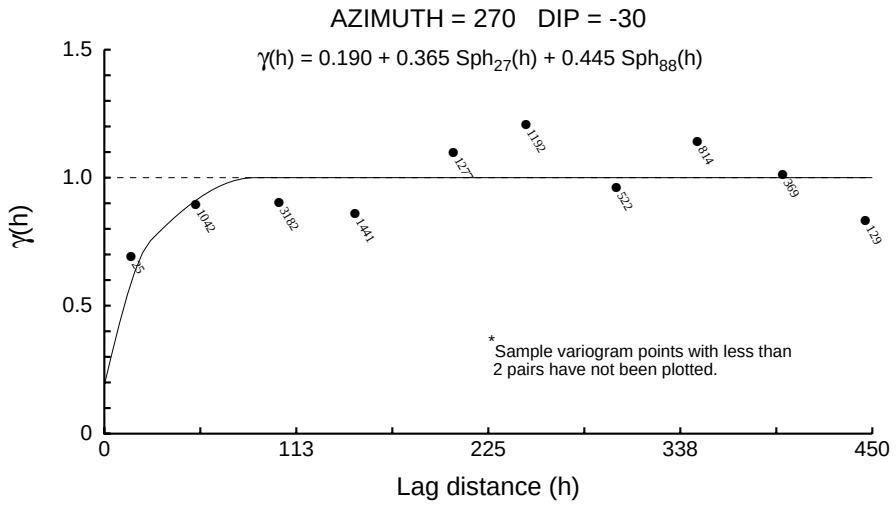
Uncapped Au - All Zones

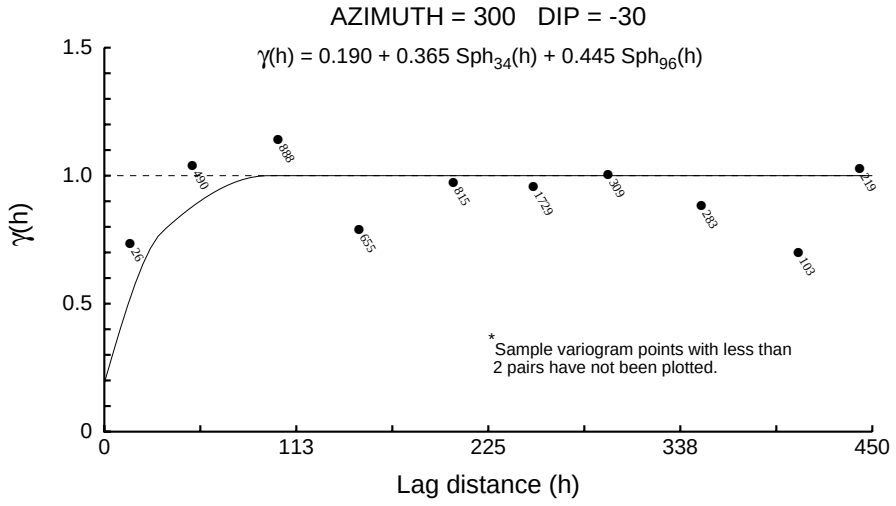


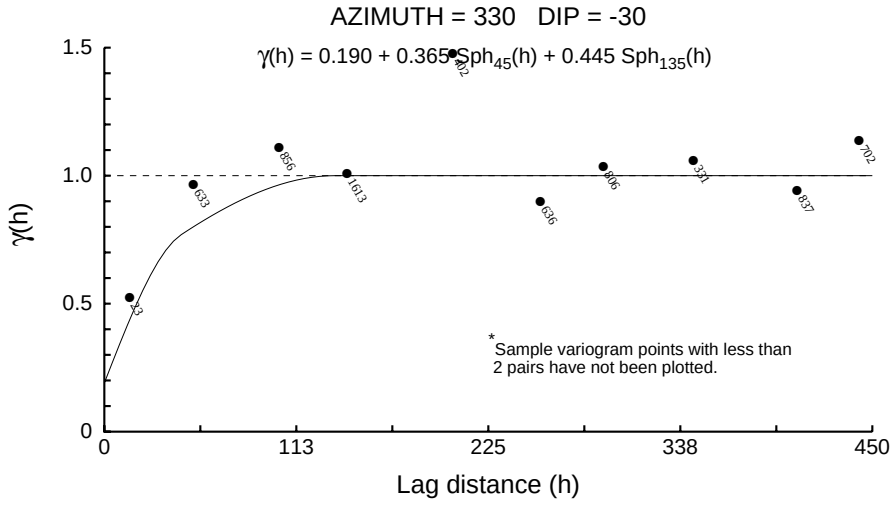




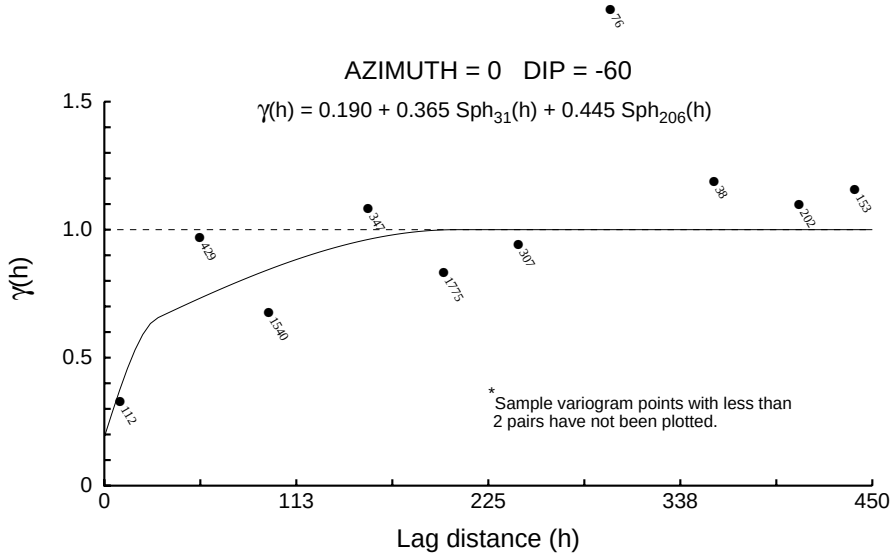
Uncapped Au - All Zones

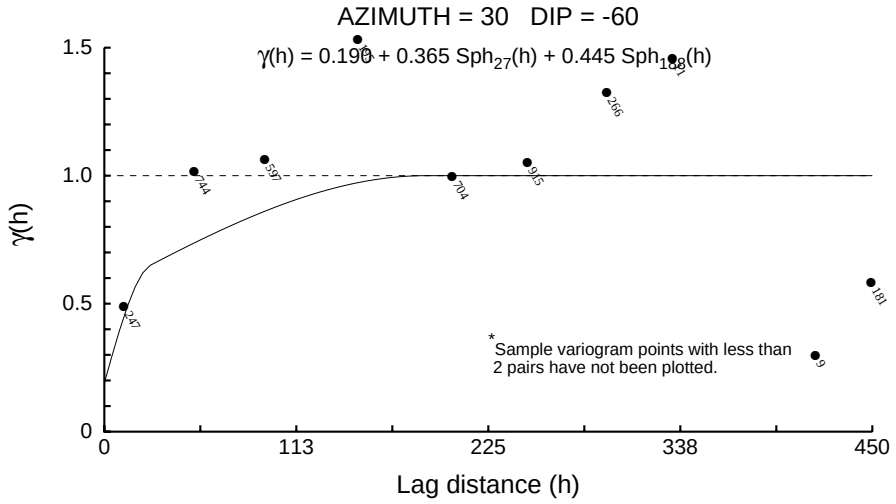


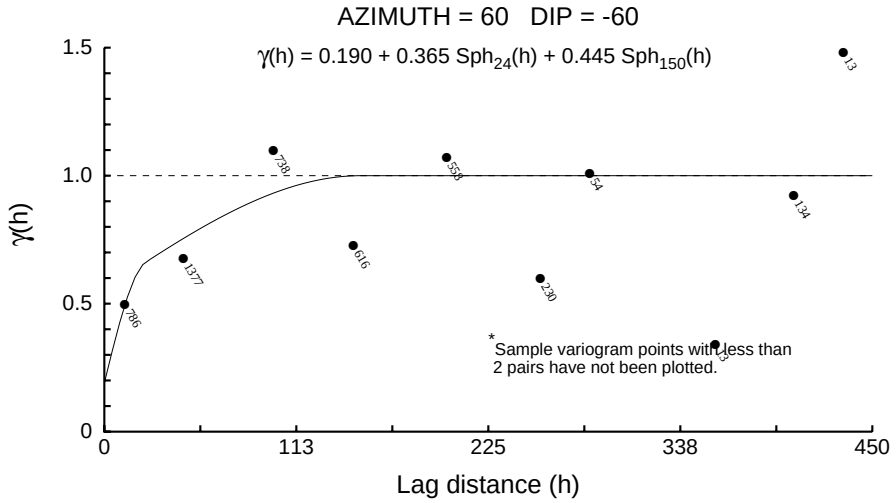




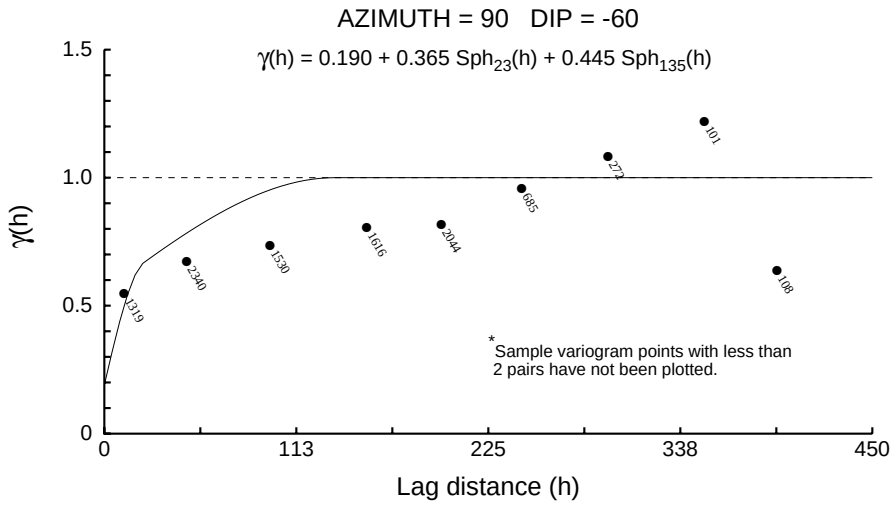
Uncapped Au - All Zones

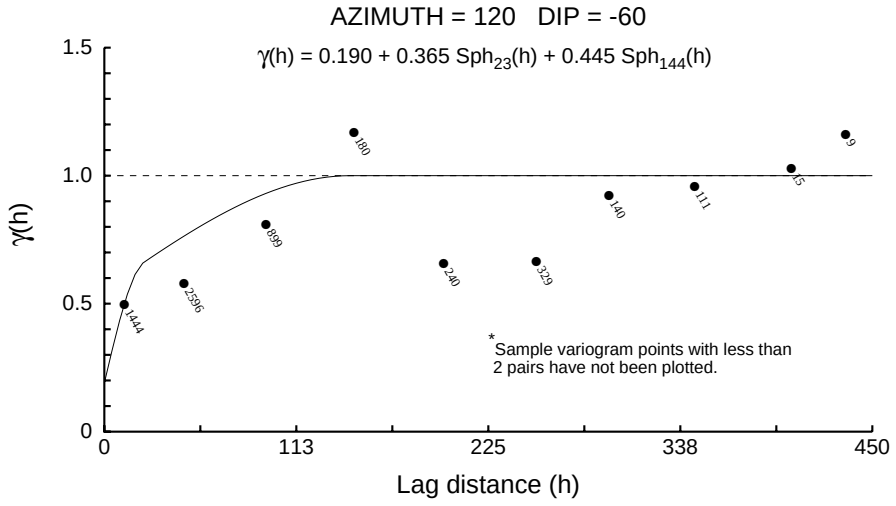


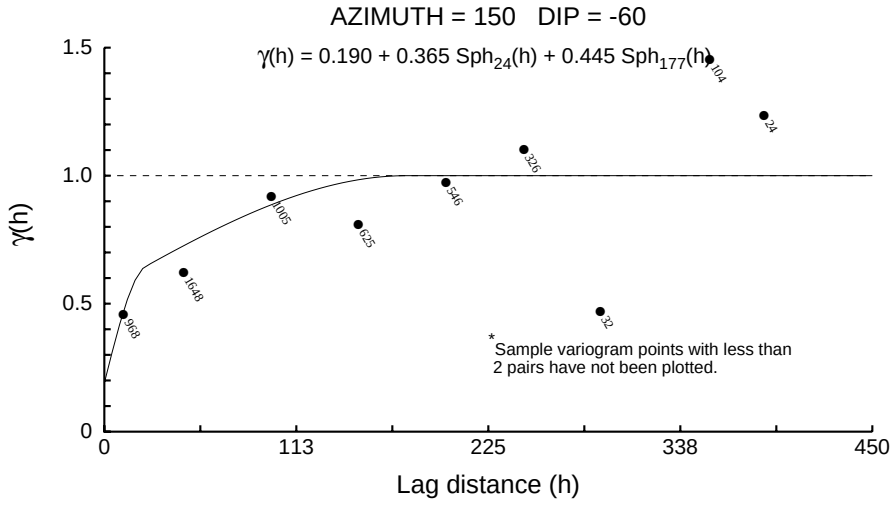




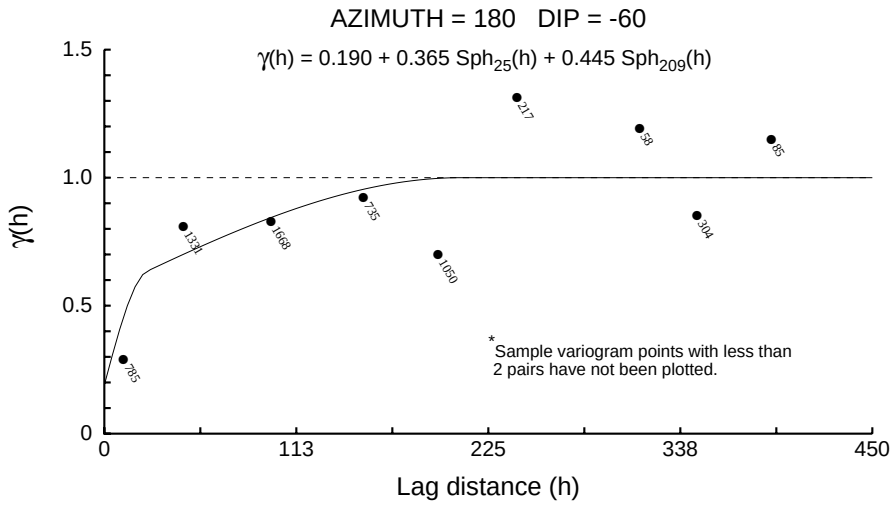
Uncapped Au - All Zones

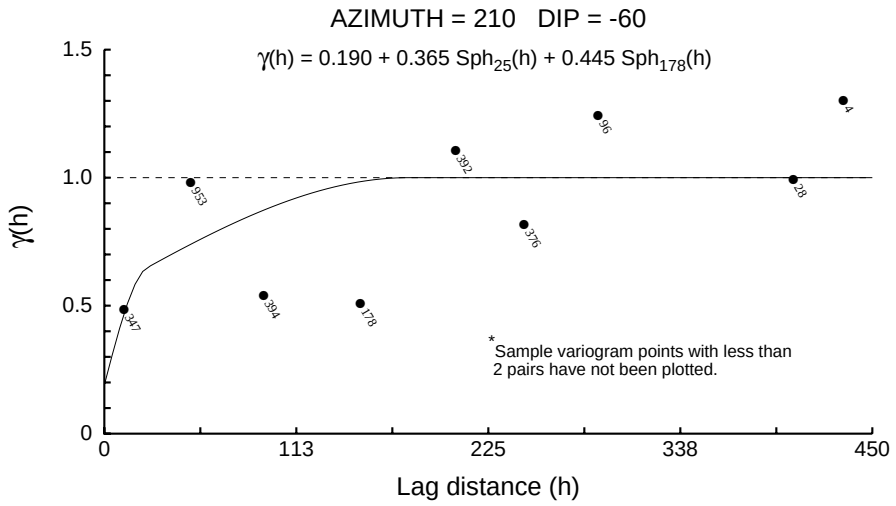


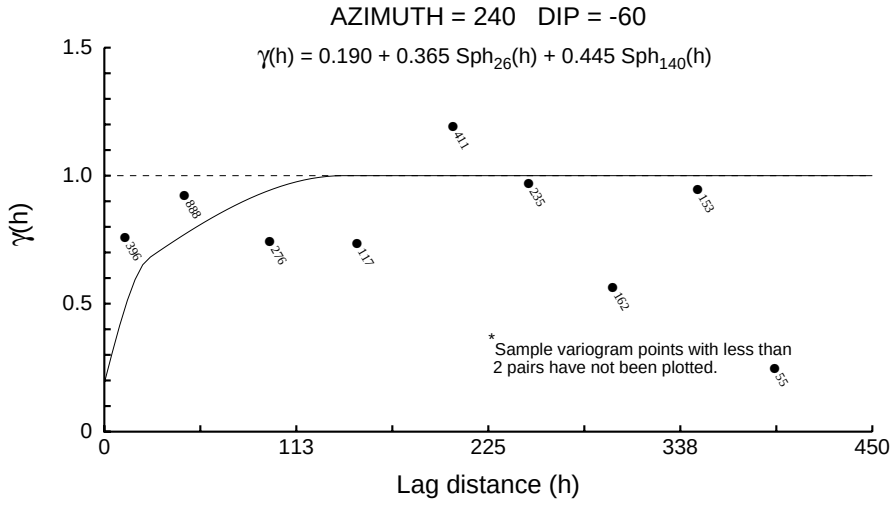




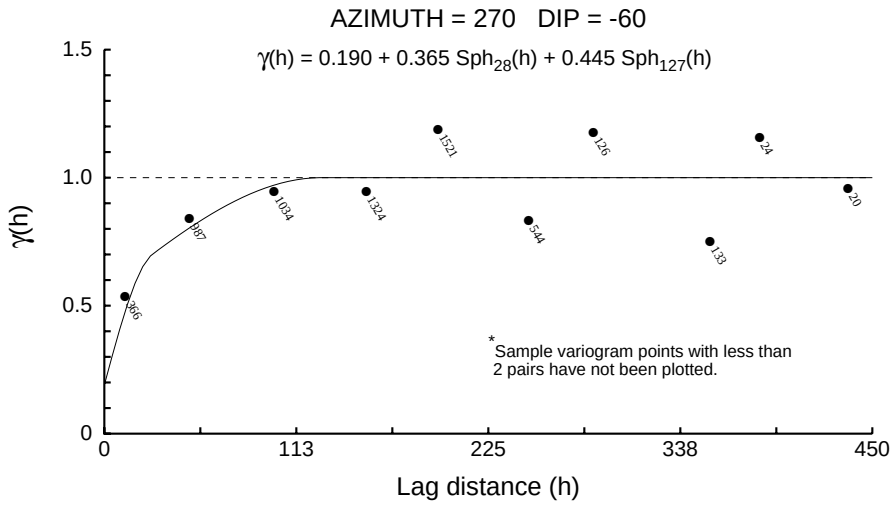
Uncapped Au - All Zones

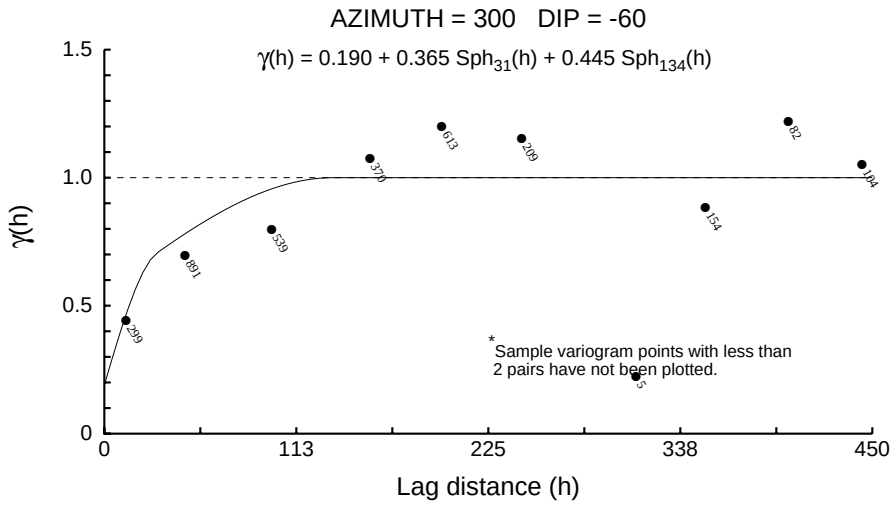


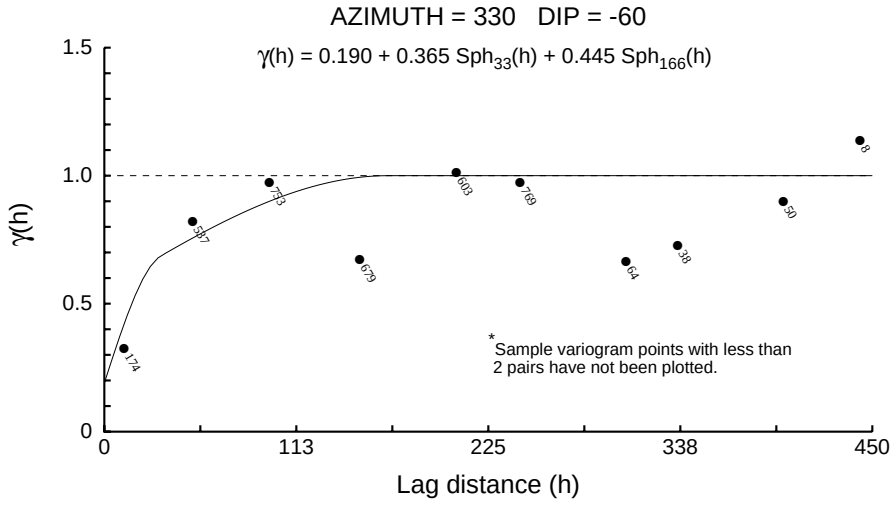




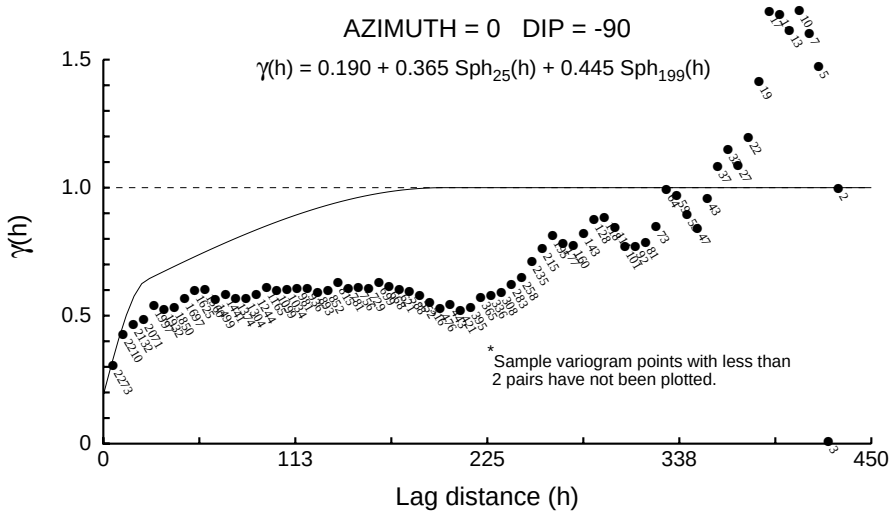
Uncapped Au - All Zones







Uncapped Au - All Zones



Uncapped Au - All Zones

User Defined Rotation Conventions

Nugget ==> 0.190
C1 ==> 0.365
C2 ==> 0.445

First Structure -- Spherical

RH Rotation about the Z axis ==> 2
RH Rotation about the Y' axis ==> -55
RH Rotation about the Z' axis ==> -61
Range along the Z' axis ==> 22 Azimuth ==> 268 Dip ==> 35
Range along the Y' axis ==> 25 Azimuth ==> 44 Dip ==> 46
Range along the X' axis ==> 47 Azimuth ==> 160 Dip ==> 23

Second Structure -- Spherical

RH Rotation about the Z axis ==> 7
RH Rotation about the Y' axis ==> -2
RH Rotation about the Z' axis ==> -11
Range along the Z' axis ==> 200 Azimuth ==> 263 Dip ==> 88
Range along the Y' axis ==> 244 Azimuth ==> 4 Dip ==> 0
Range along the X' axis ==> 79 Azimuth ==> 94 Dip ==> 2

Modeling Criteria

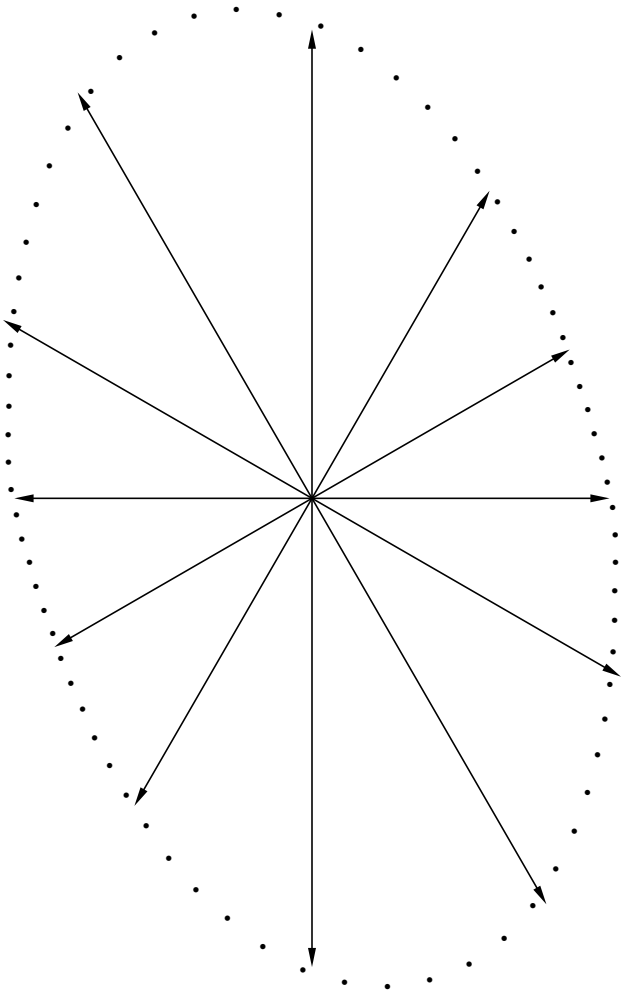
Minimum number pairs req'd ==> 2
Sample variogram points weighted by # pairs

Uncapped Au - All Zones

Structure Number 1

Rose Diagram of Ranges Dipping 0 Degrees
Scale:

50 Units

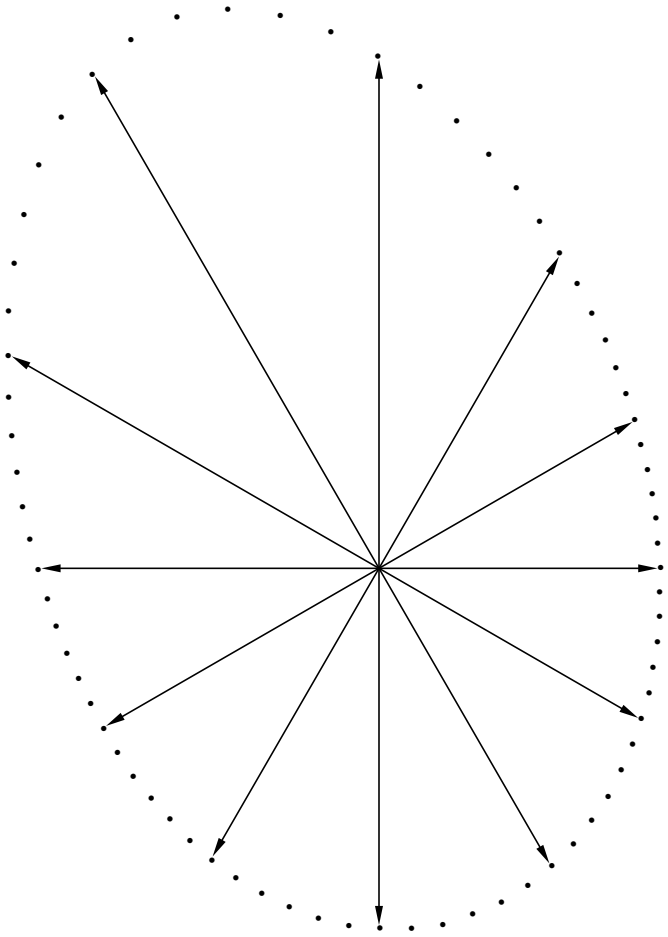


Uncapped Au - All Zones

Structure Number 1

Rose Diagram of Ranges Dipping 30 Degrees
Scale:

50 Units

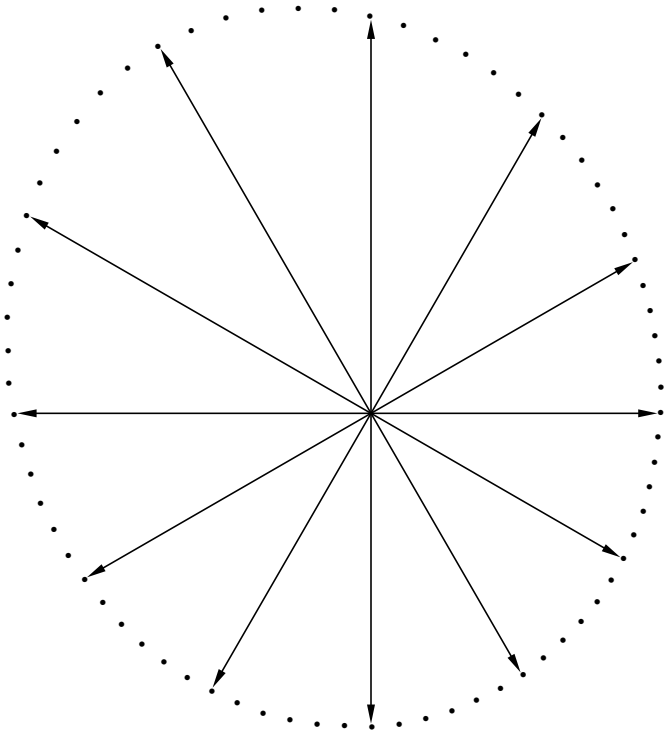


Uncapped Au - All Zones

Structure Number 1

Rose Diagram of Ranges Dipping 60 Degrees
Scale:

50 Units

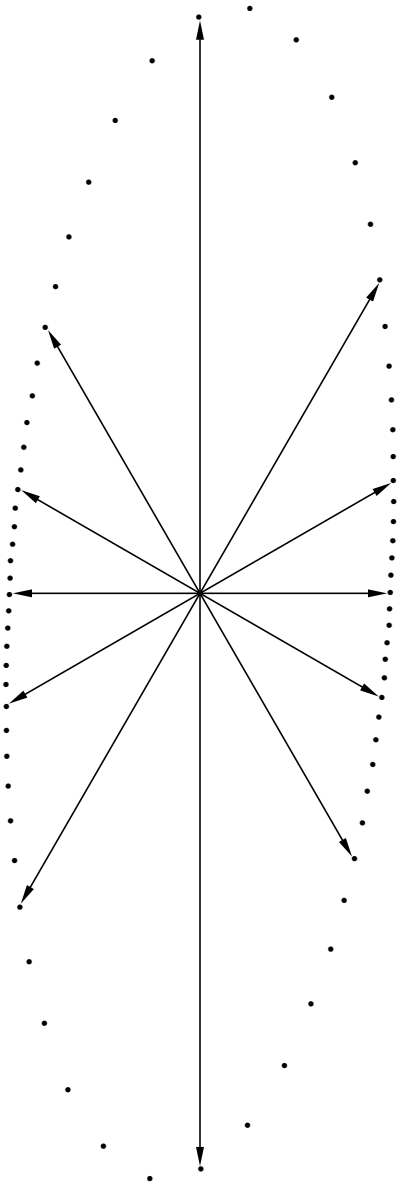


Uncapped Au - All Zones

Structure Number 2

Rose Diagram of Ranges Dipping 0 Degrees
Scale:

200 Units

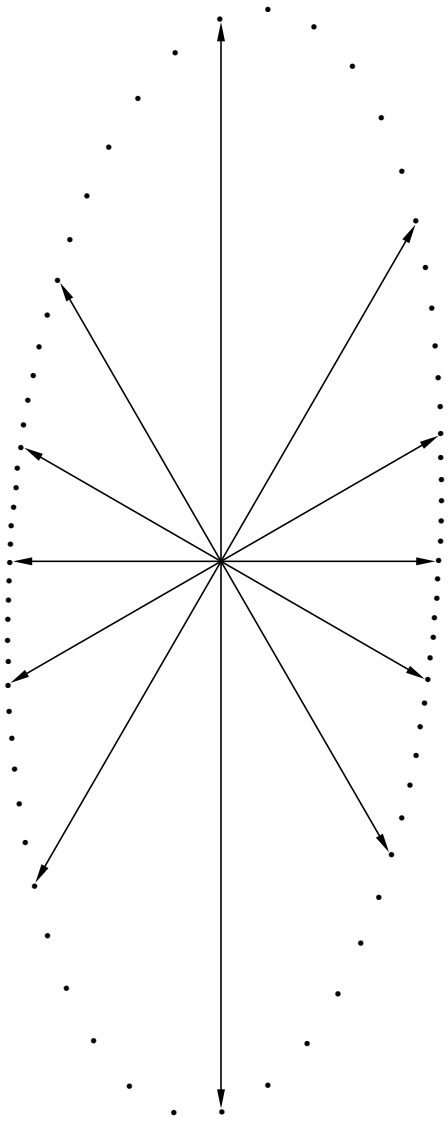


Uncapped Au - All Zones

Structure Number 2

Rose Diagram of Ranges Dipping 30 Degrees
Scale:

200 Units

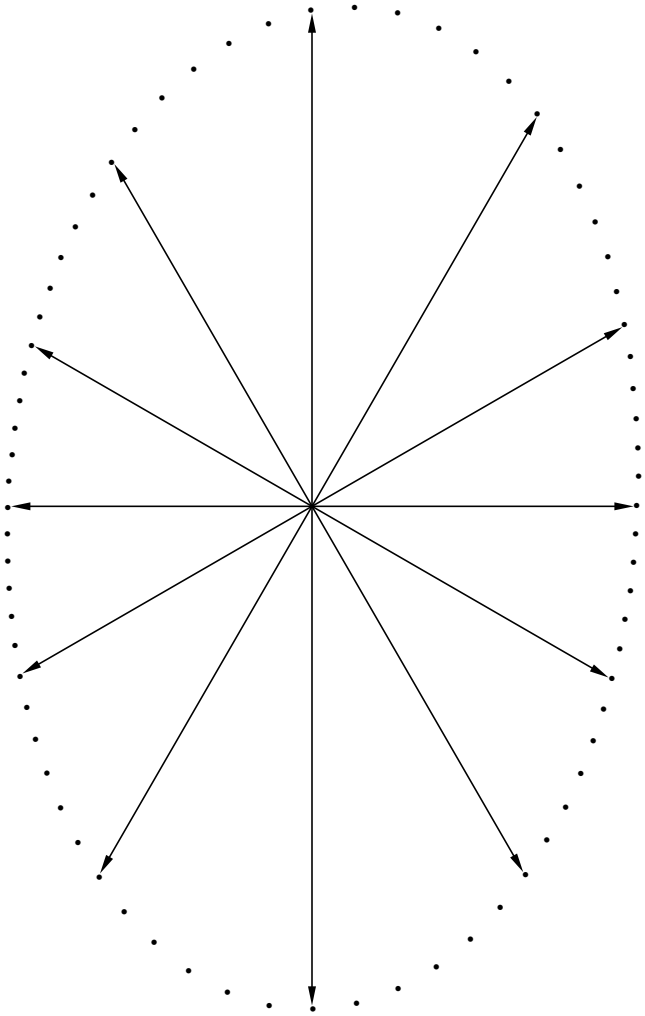


Uncapped Au - All Zones

Structure Number 2

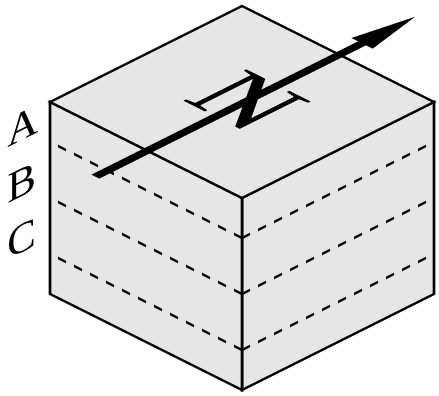
Rose Diagram of Ranges Dipping 60 Degrees
Scale:

200 Units

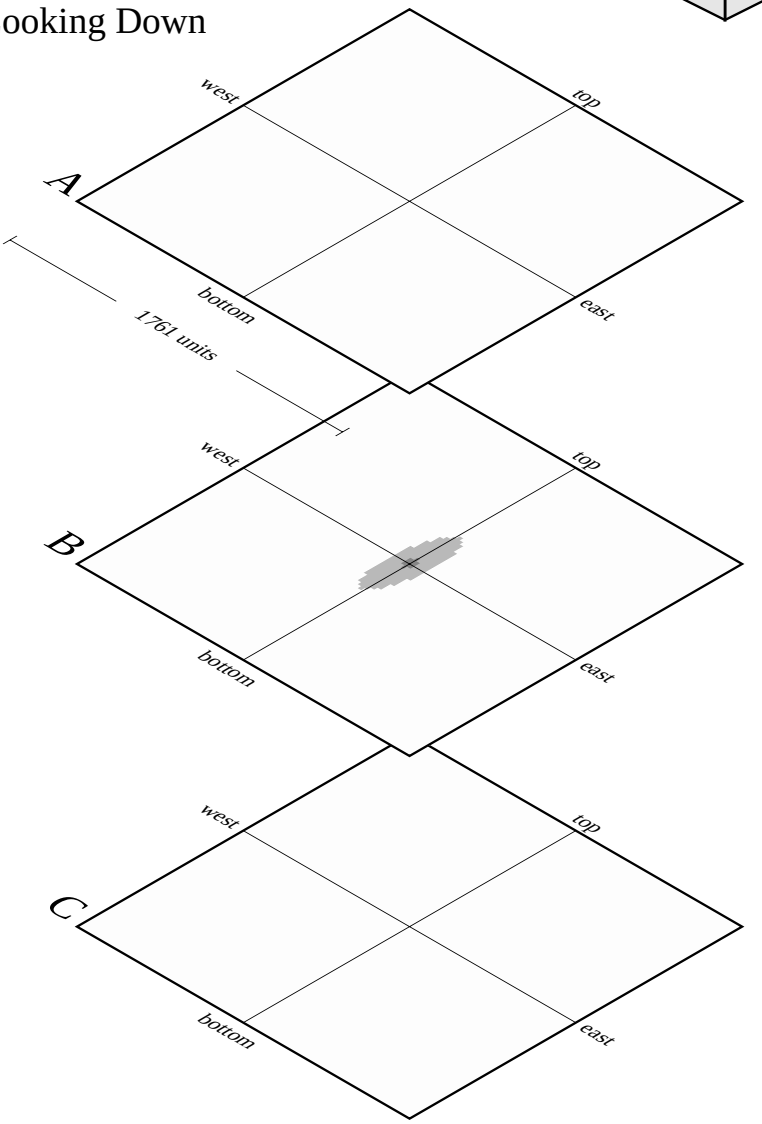


Horizontal Slices Through the Ellipsoids

Reference Cube



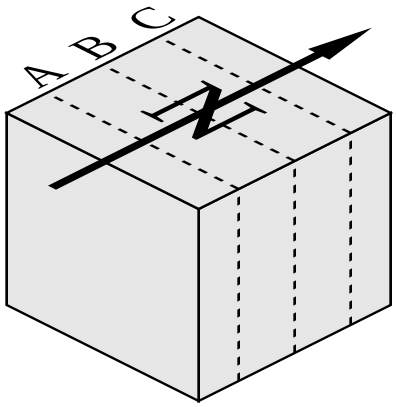
X-Y Planes Looking Down



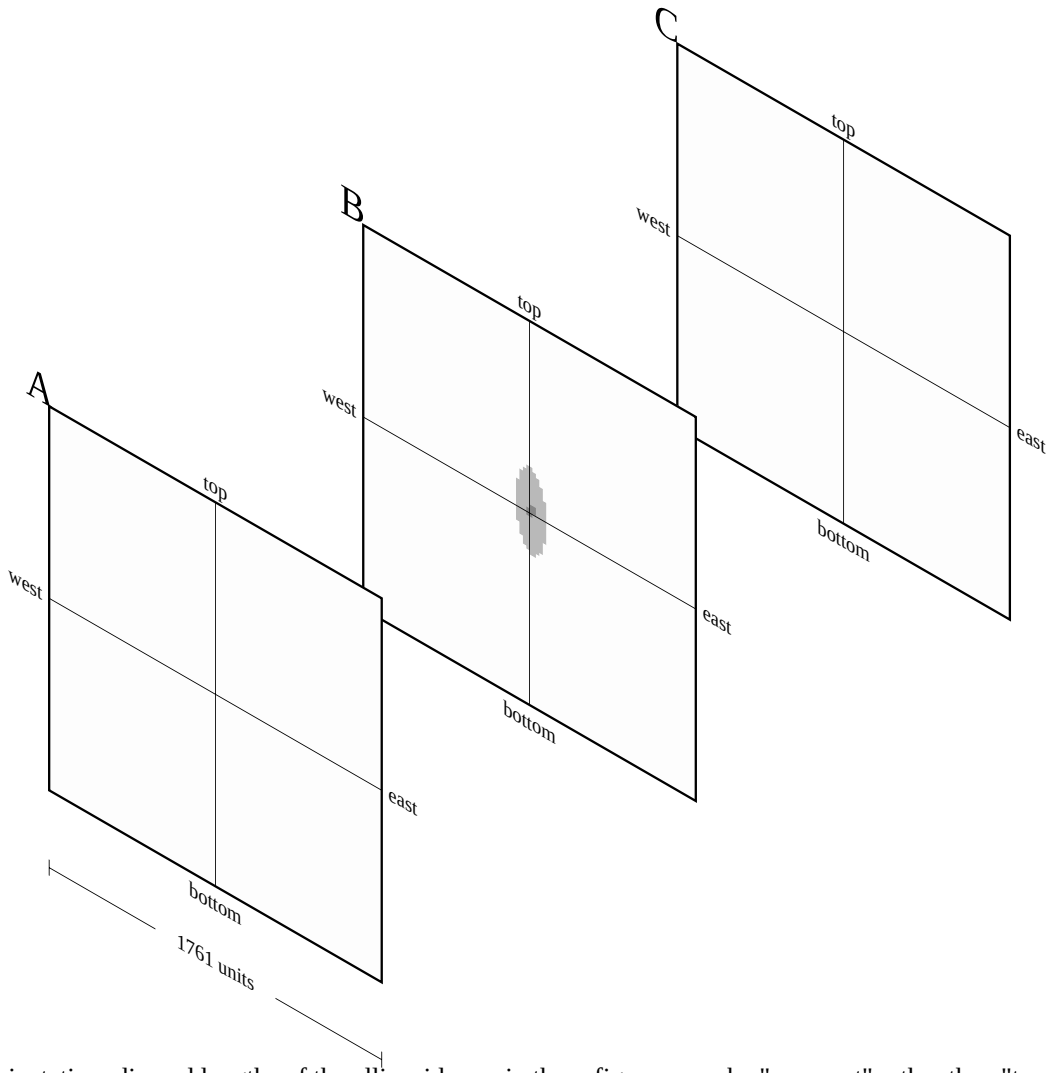
Note -- the orientation, dip and lengths of the ellipsoid axes in these figures may be "apparent" rather than "true".

Cross Section Views Through the Ellipsoids

Reference Cube



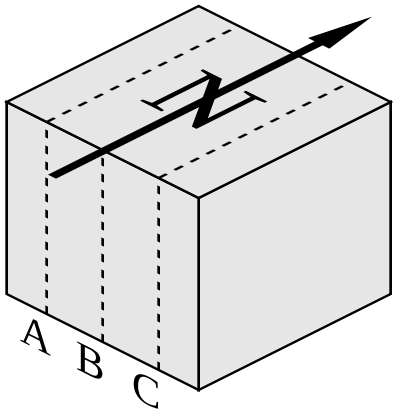
X-Z Planes Looking North



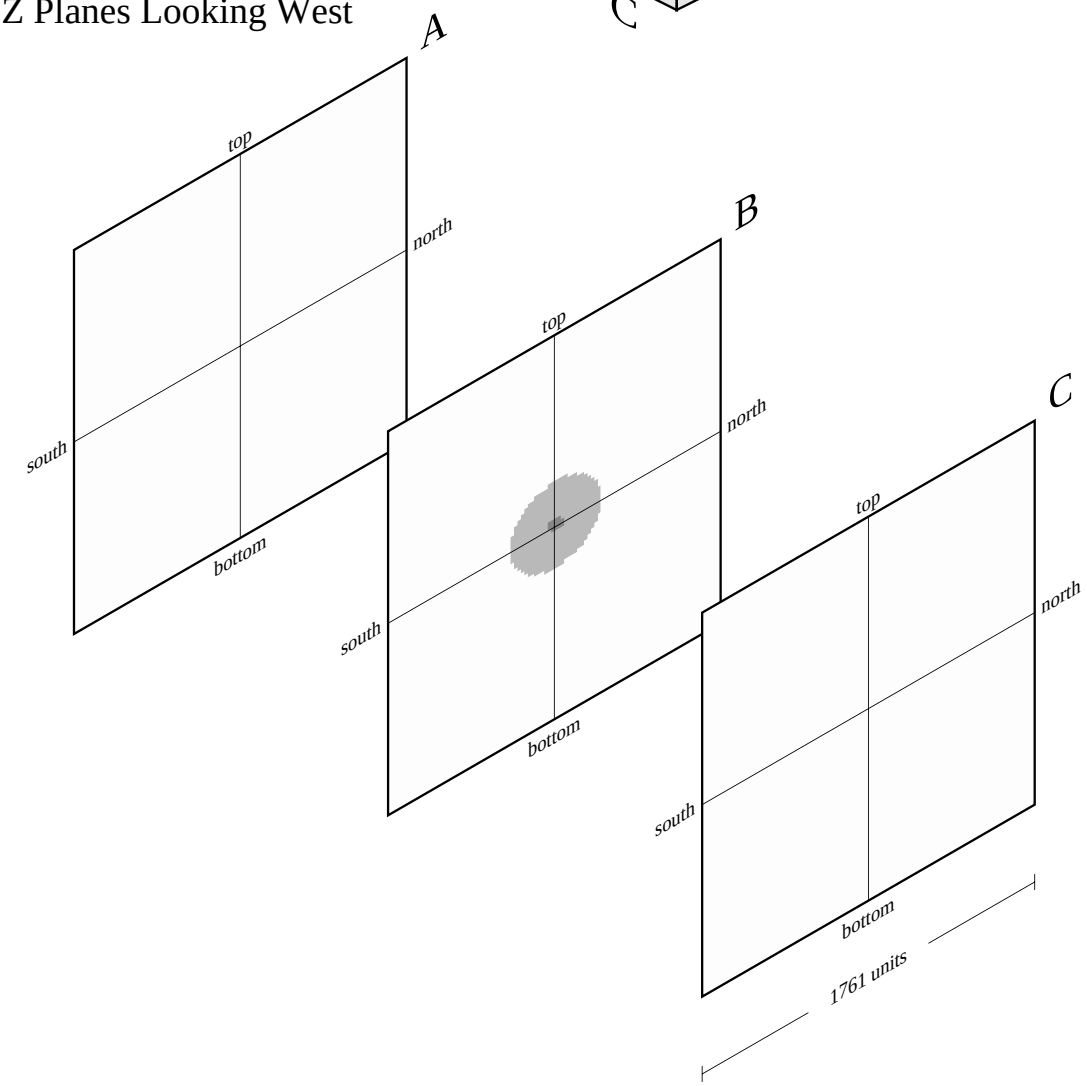
Note -- the orientation, dip and lengths of the ellipsoid axes in these figures may be "apparent" rather than "true".

Long Section Views Through the Ellipsoids

Reference Cube



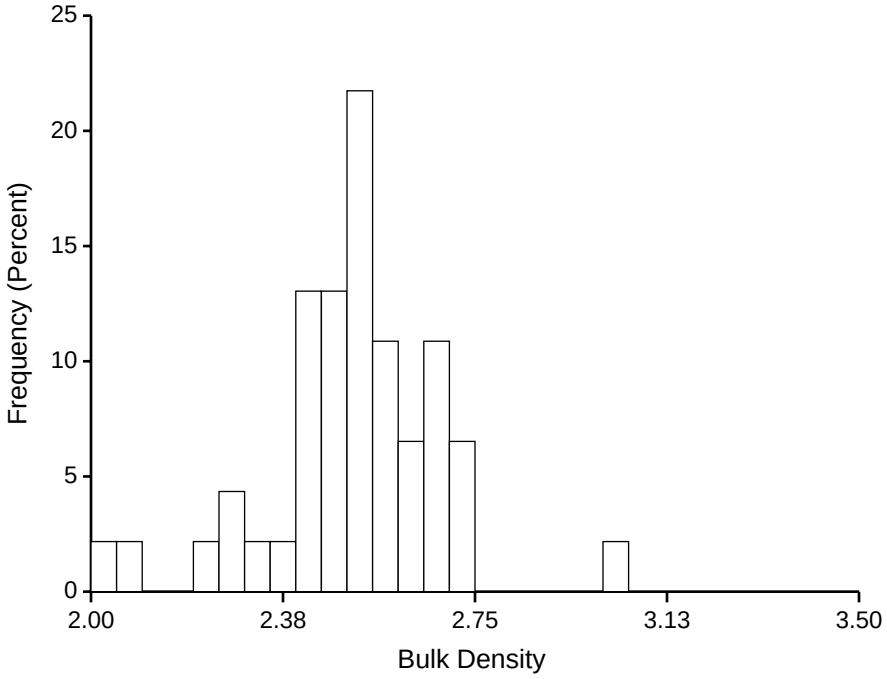
Y-Z Planes Looking West



Note -- the orientation, dip and lengths of the ellipsoid axes in these figures may be "apparent" rather than "true".

APPENDIX C BULK DENSITY HISTOGRAMS

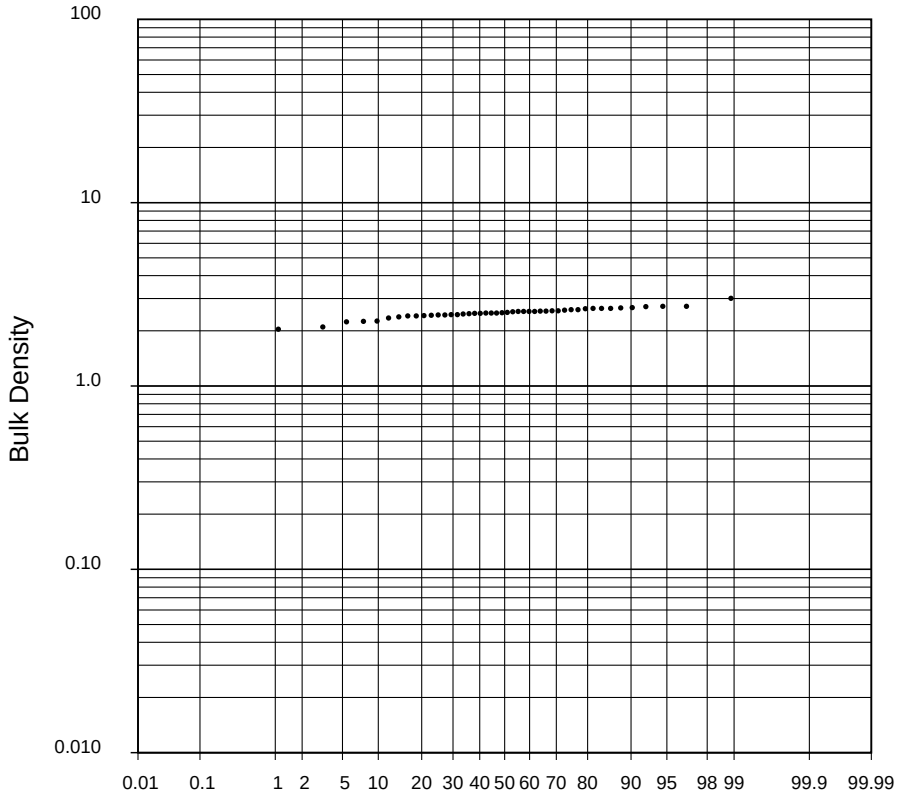
Mirador Project Bulk Density Values Enriched



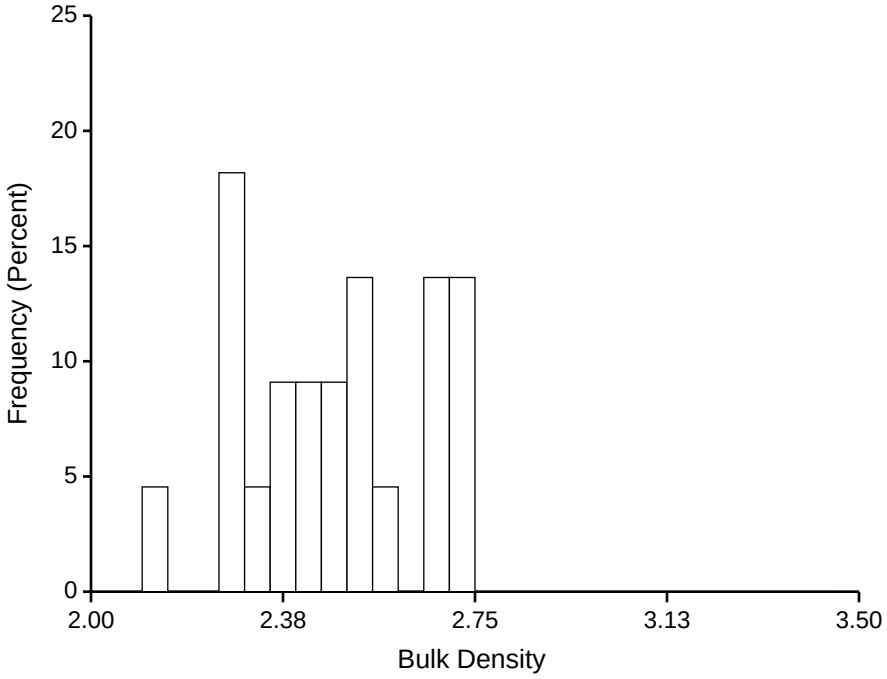
N	46
m	2.51
σ^2	0.03
σ/m	0.07
min	2.04
$q_{0.25}$	2.43
$q_{0.50}$	2.51
$q_{0.75}$	2.59
max	3.01

Class width = 0.05
The last class contains all values ≥ 3.45

Mirador Project Bulk Density Values Enriched



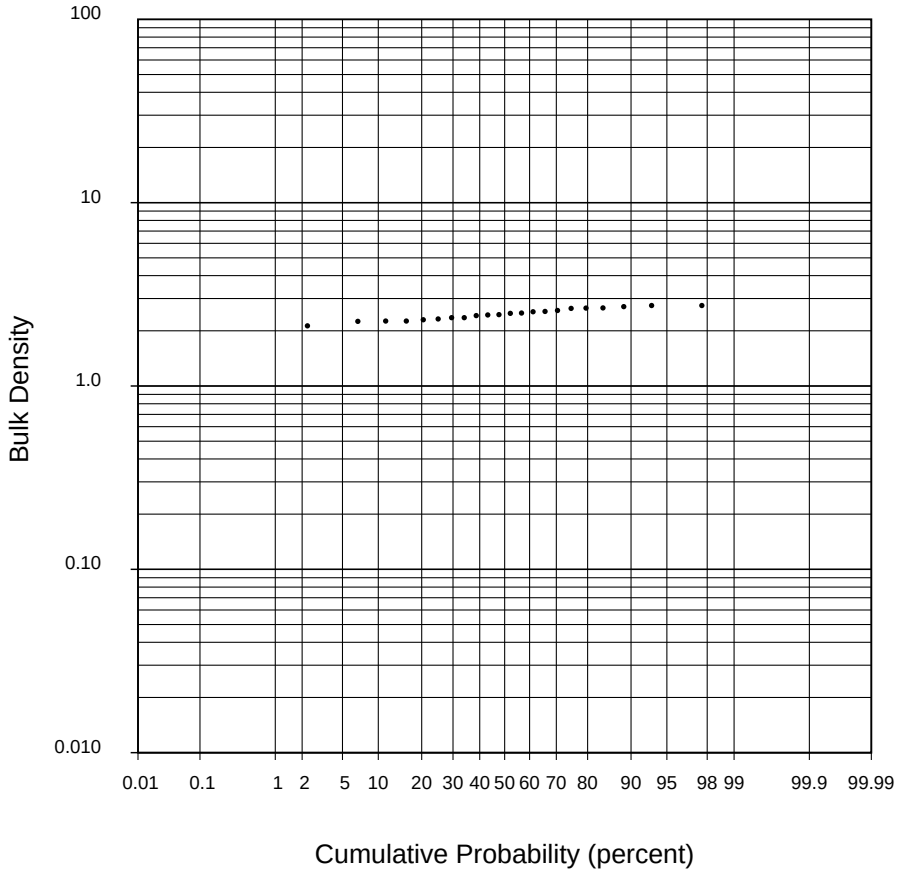
Mirador Project Bulk Density Values Mixed



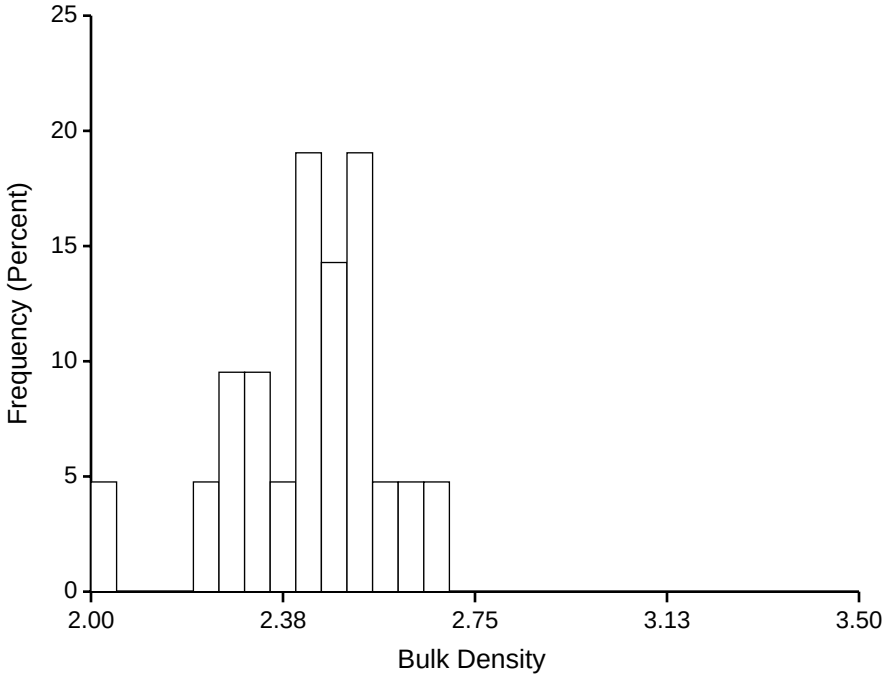
N	22
m	2.47
σ^2	0.03
σ/m	0.07
min	2.13
$q_{0.25}$	2.30
$q_{0.50}$	2.47
$q_{0.75}$	2.58
max	2.75

Class width = 0.05
The last class contains all values ≥ 3.45

Mirador Project Bulk Density Values Mixed



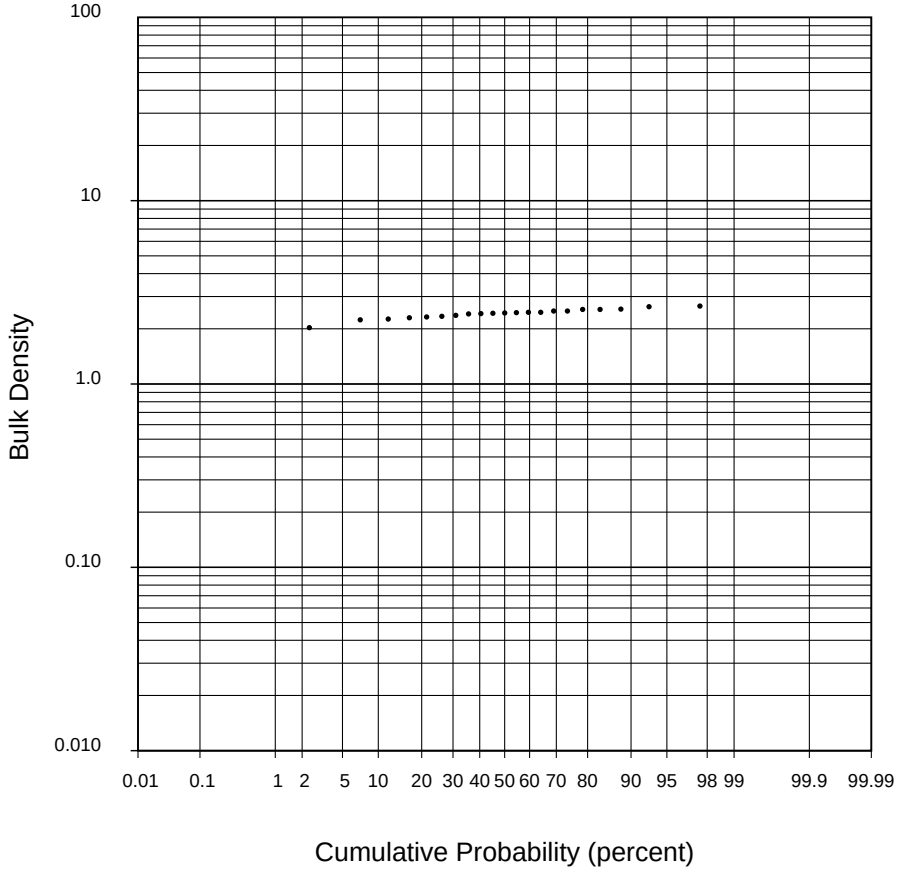
Mirador Project Bulk Density Values Leached



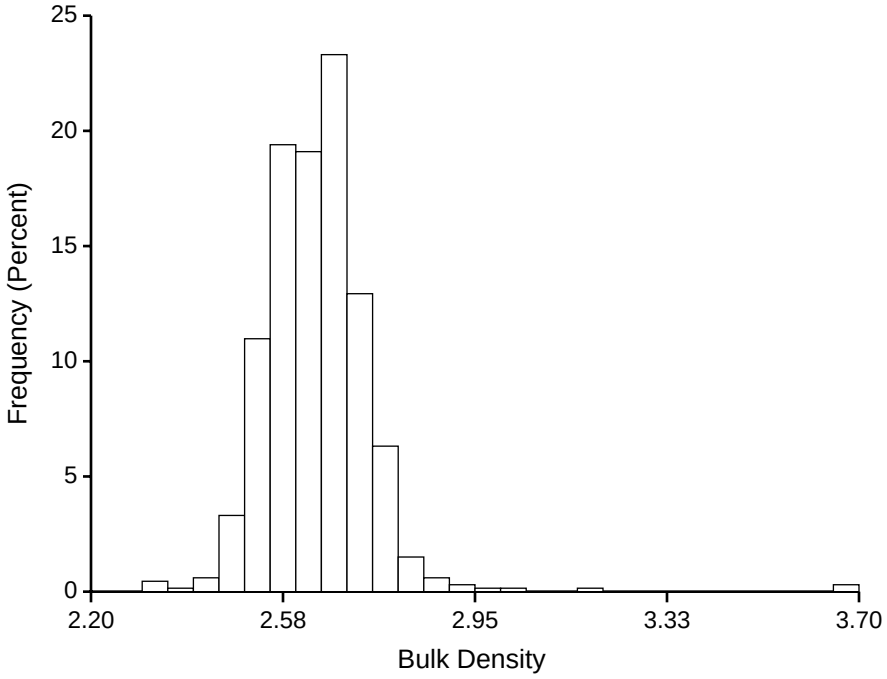
N	21
m	2.42
σ^2	0.02
σ/m	0.06
min	2.03
$q_{0.25}$	2.32
$q_{0.50}$	2.44
$q_{0.75}$	2.50
max	2.66

Class width = 0.05
The last class contains all values ≥ 3.45

Mirador Project Bulk Density Values Leached



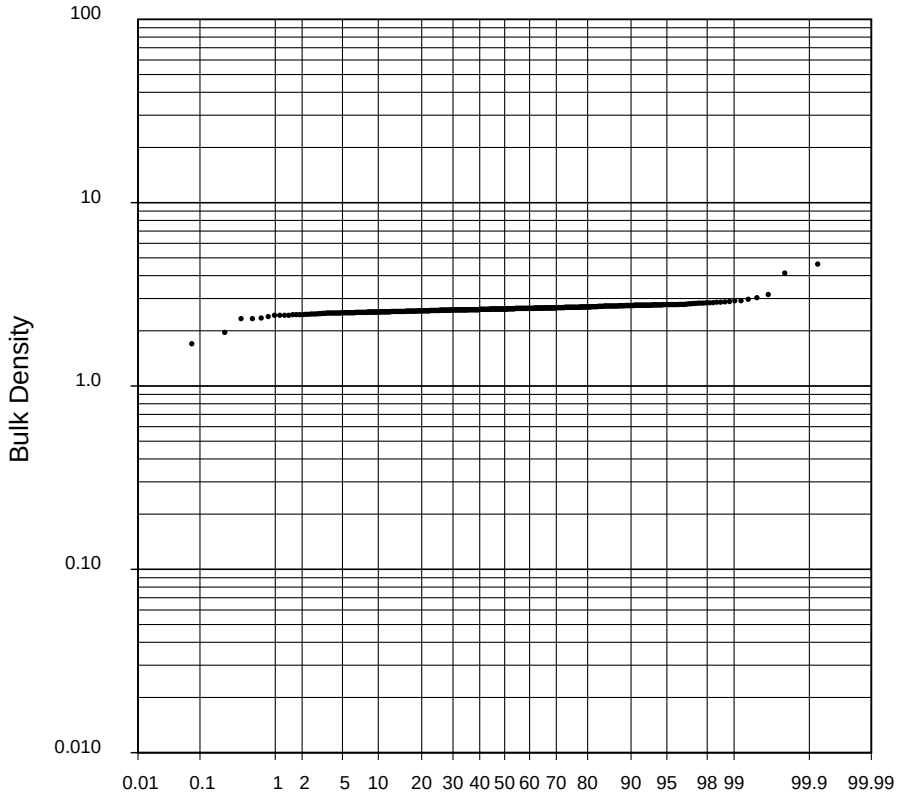
Mirador Project Bulk Density Values MNZD



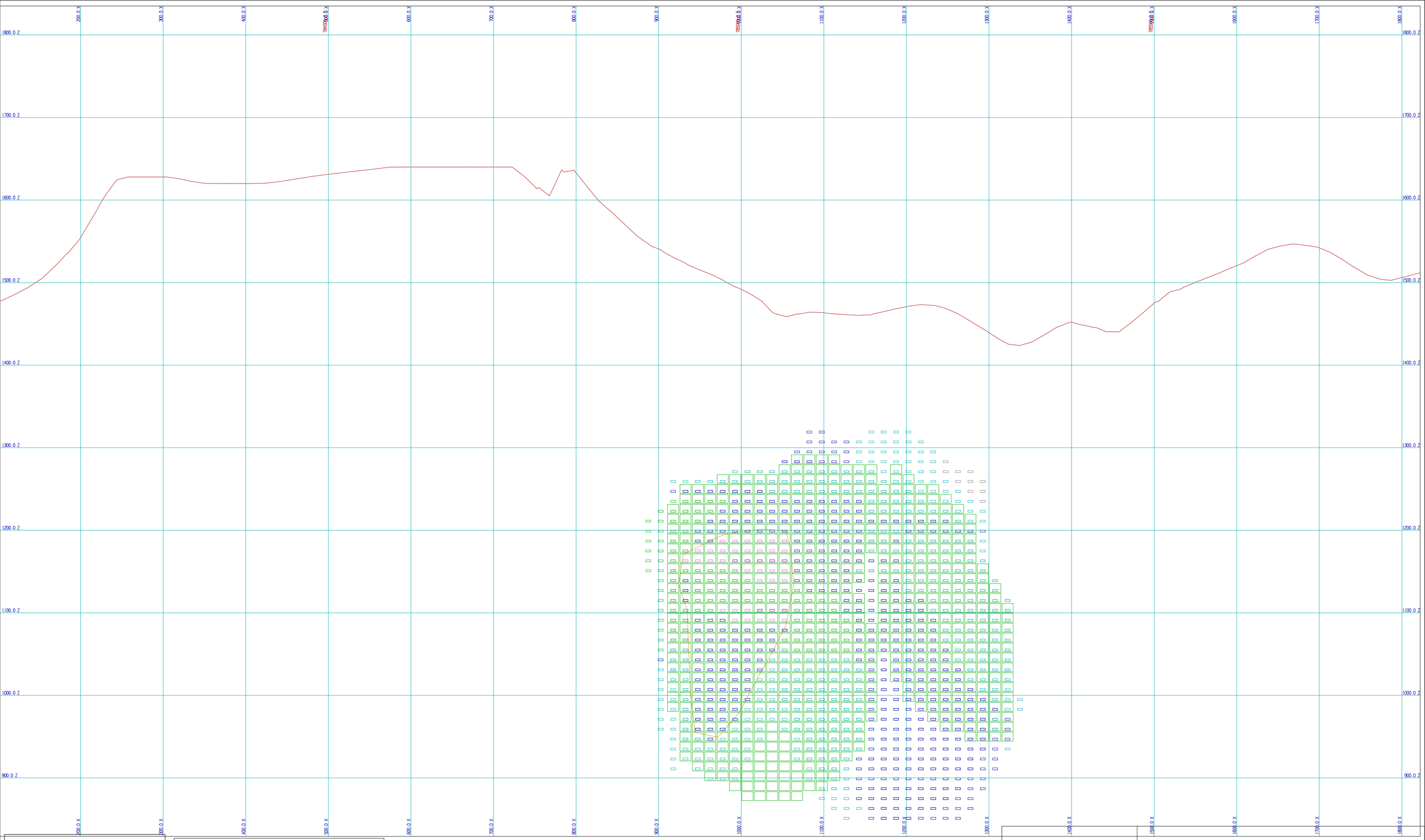
N	665
m	2.64
σ^2	0.02
σ/m	0.05
min	1.70
$q_{0.25}$	2.58
$q_{0.50}$	2.63
$q_{0.75}$	2.69
max	4.62

Class width = 0.05
The last class contains all values ≥ 3.65

Mirador Project Bulk Density Values MNZD



APPENDIX D BLOCK MODEL SECTIONS



CU

0.001	0.300	
0.300	0.400	
0.400	0.500	
0.500	0.600	
0.600	0.700	
0.700	1.000	
1.000	99.000	

UNITS : METRES DATE: 04/10/20 TIME: 01:08:46

DRAWN BY :

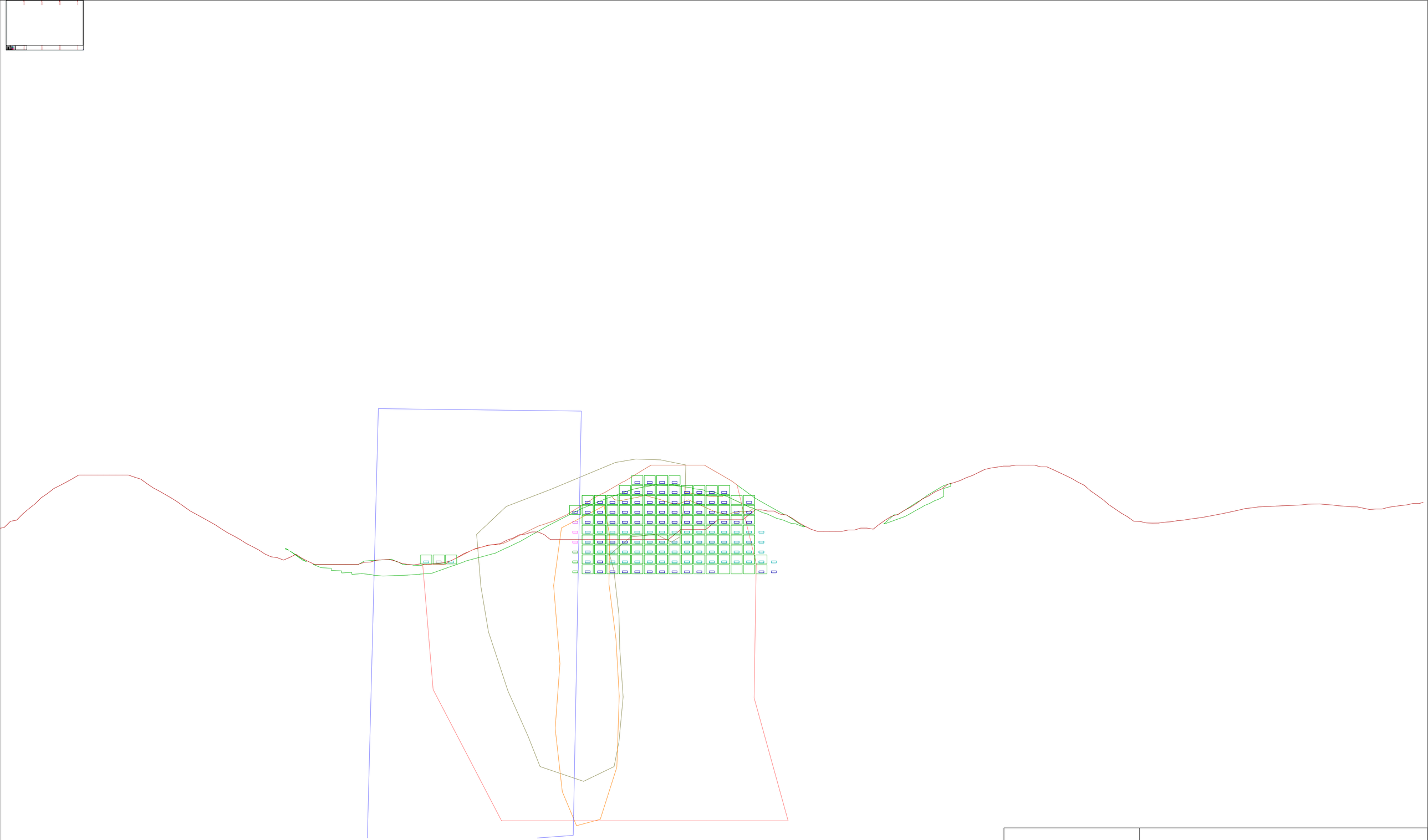
Section 3550EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



UNITS : METRES DATE: 04/10/20 TIME: 01:13:53

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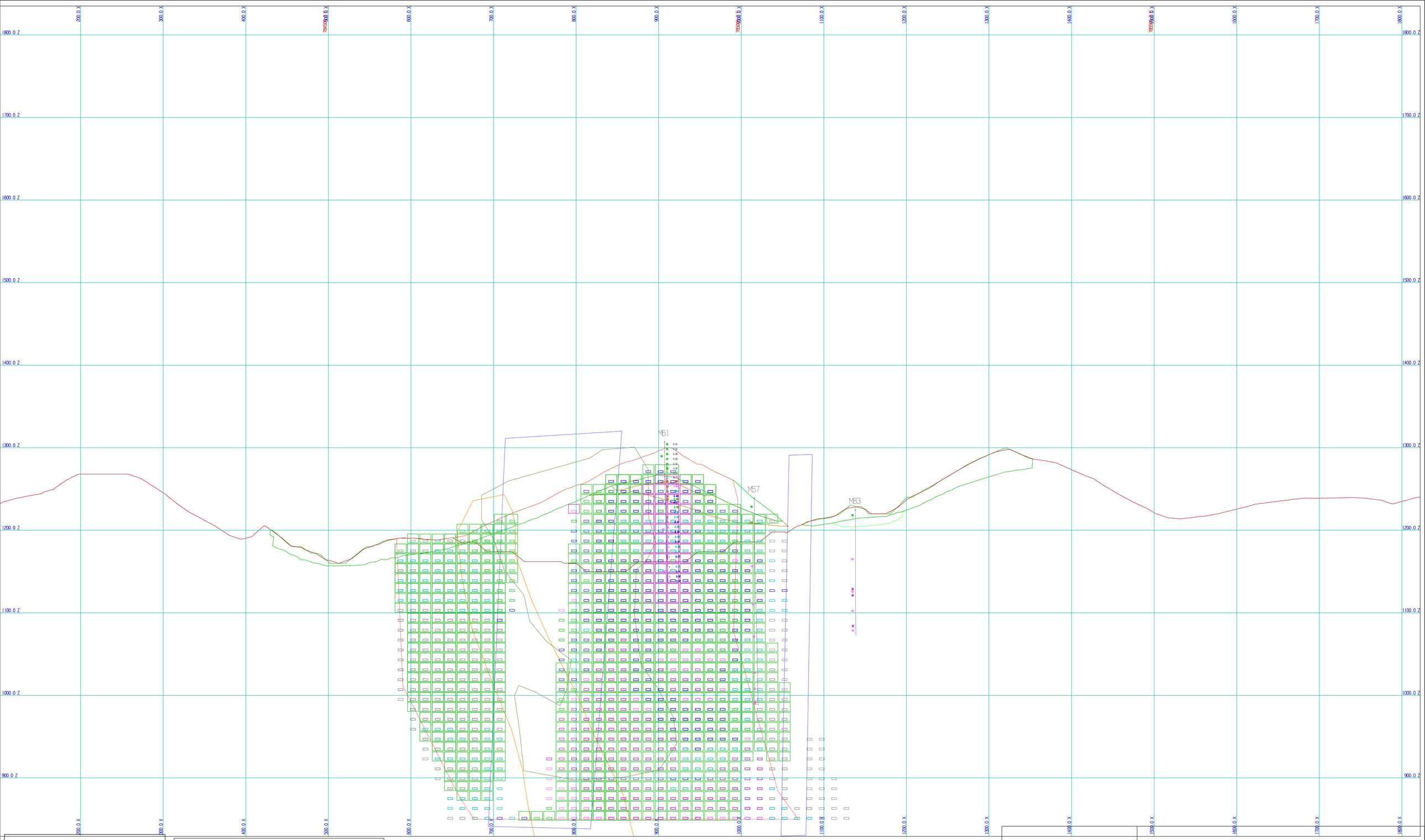
Section 4650EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300	
0.300	0.400	
0.400	0.500	
0.500	0.600	
0.600	0.700	
0.700	1.000	
1.000	99.000	

UNITS : METRES DATE: 04/10/20 TIME: 01.13.48

DRAWN BY :

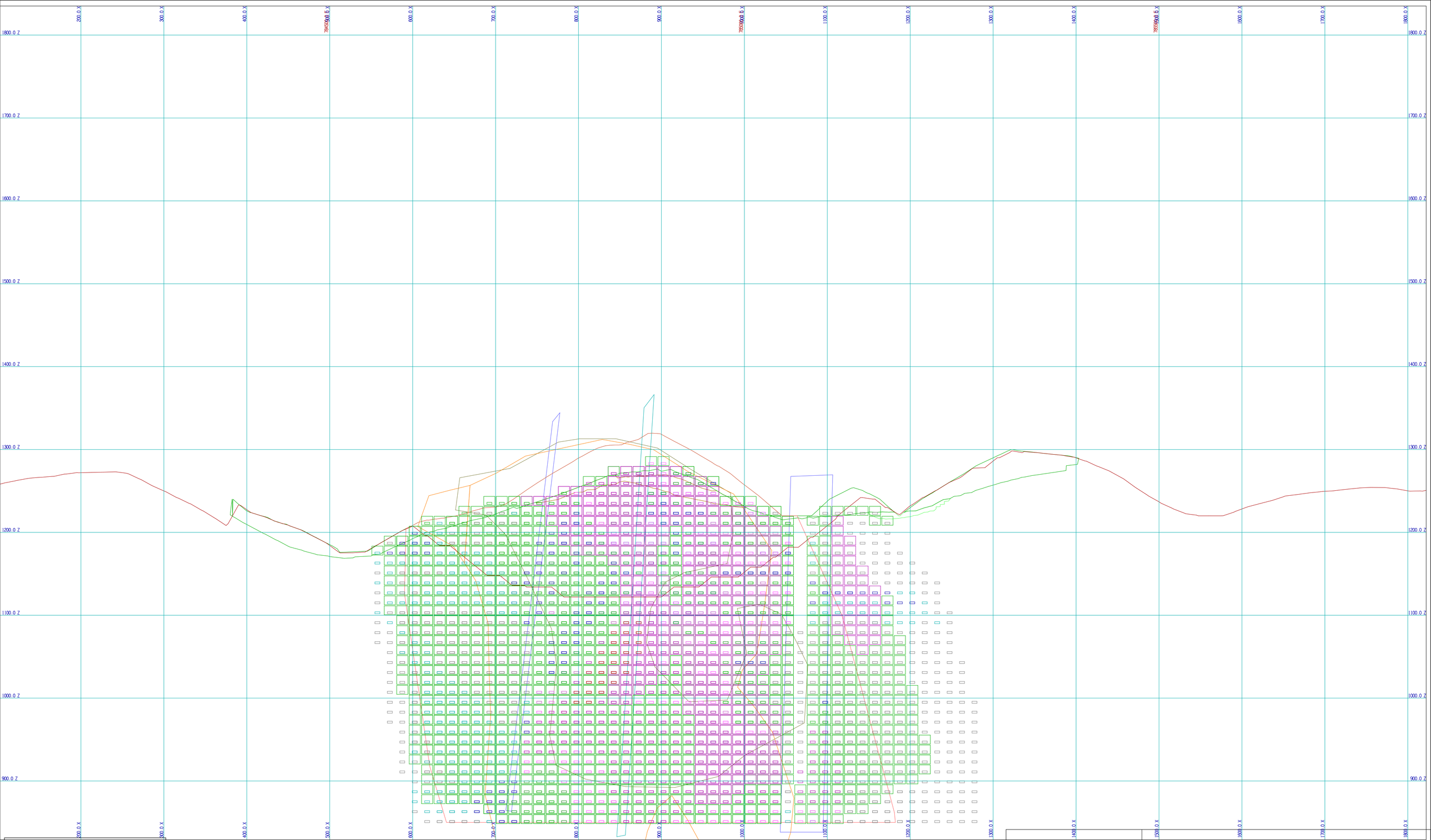
Section 4600EW Mirador Project

Block Model Plots Cu Block Values

Class=blackoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

UNITS : METRES DATE: 04/10/20 TIME: 01.13.46

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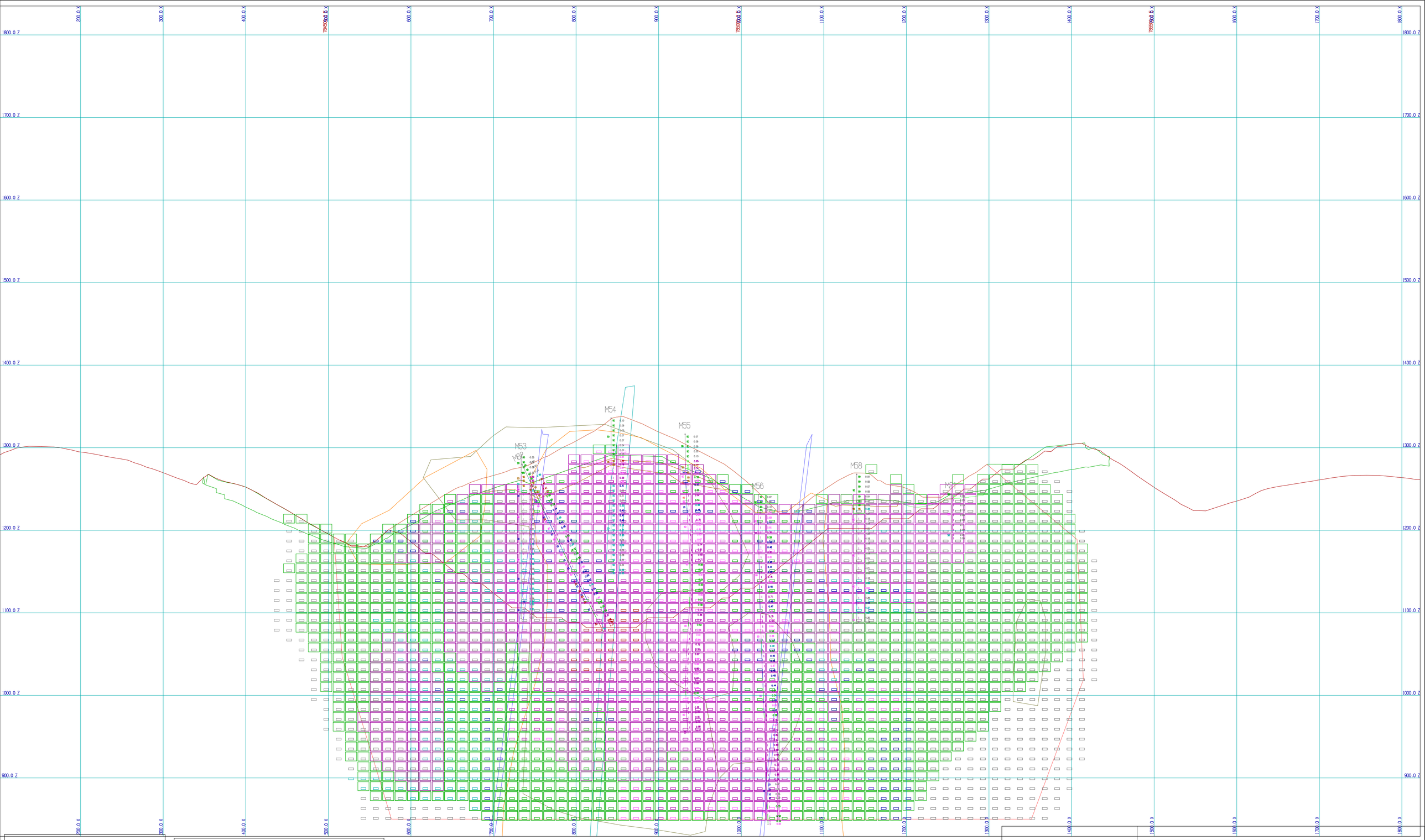
Section 4550EW Mirador Project

Block Model Plots Cu Block Values

Class=blackoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

UNITS : METRES DATE: 04/10/20 TIME: 01.13.42

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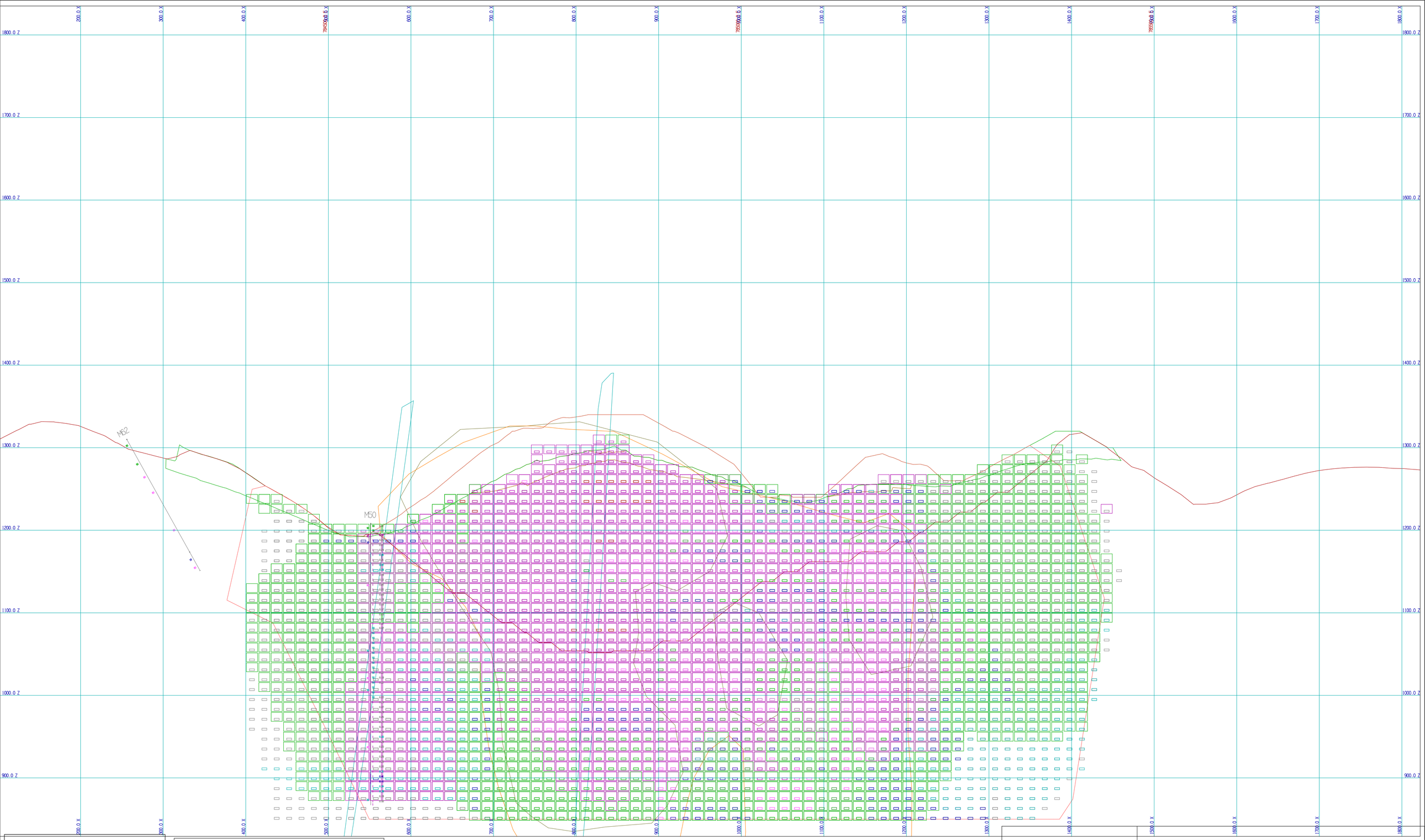
Section 4500EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

UNITS : METRES DATE: 04/10/20 TIME: 01.13.23

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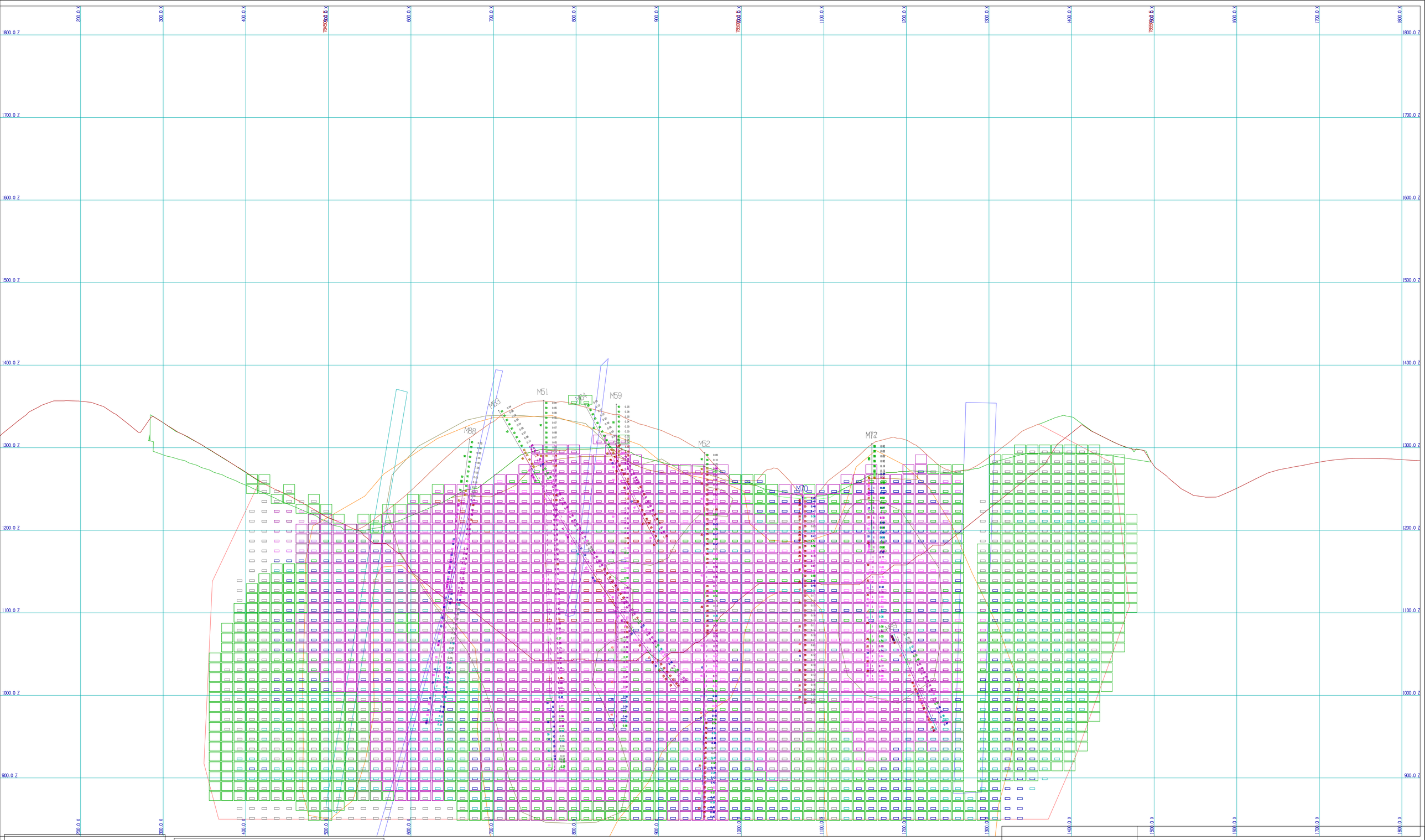
Section 4450EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

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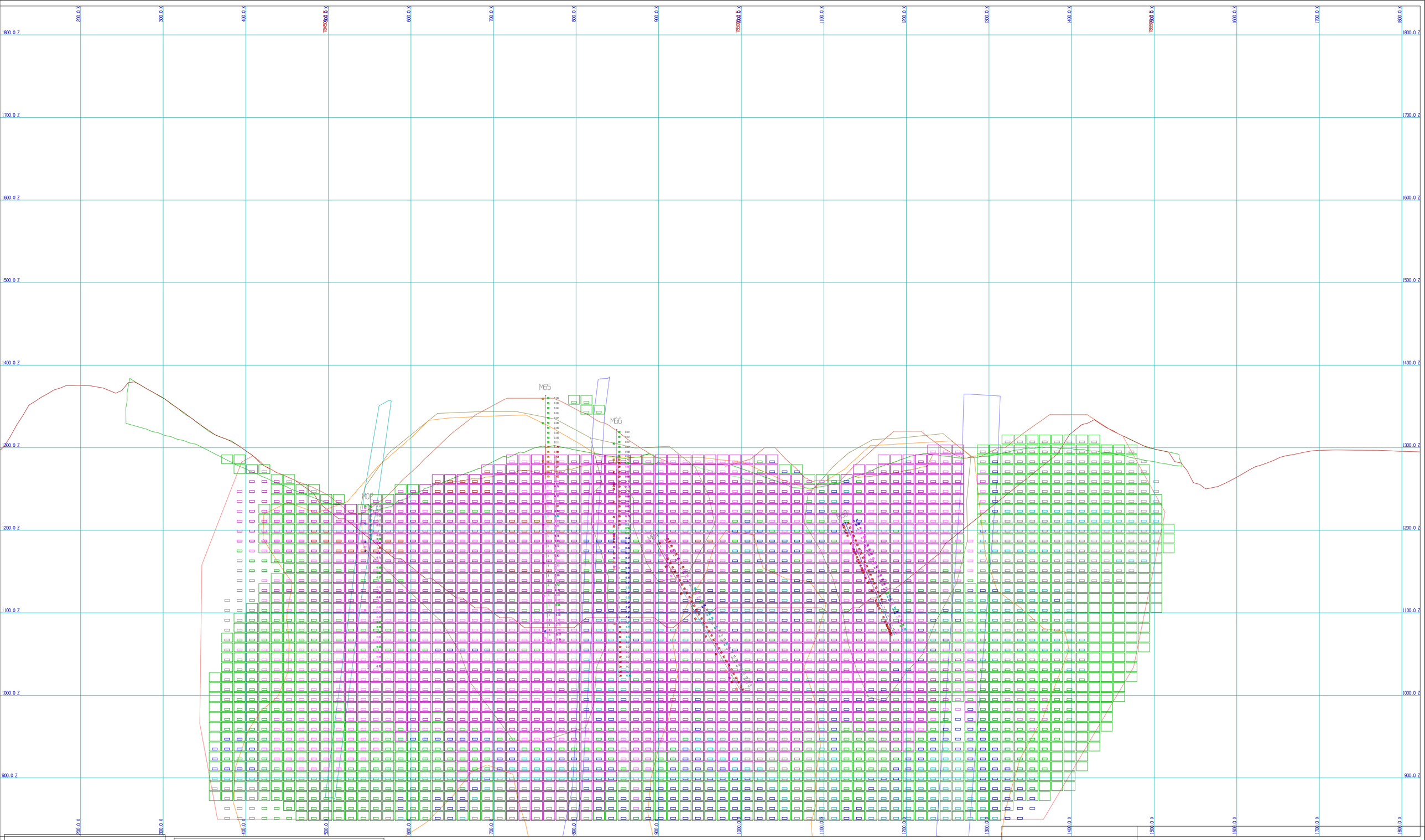
Section 4400EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

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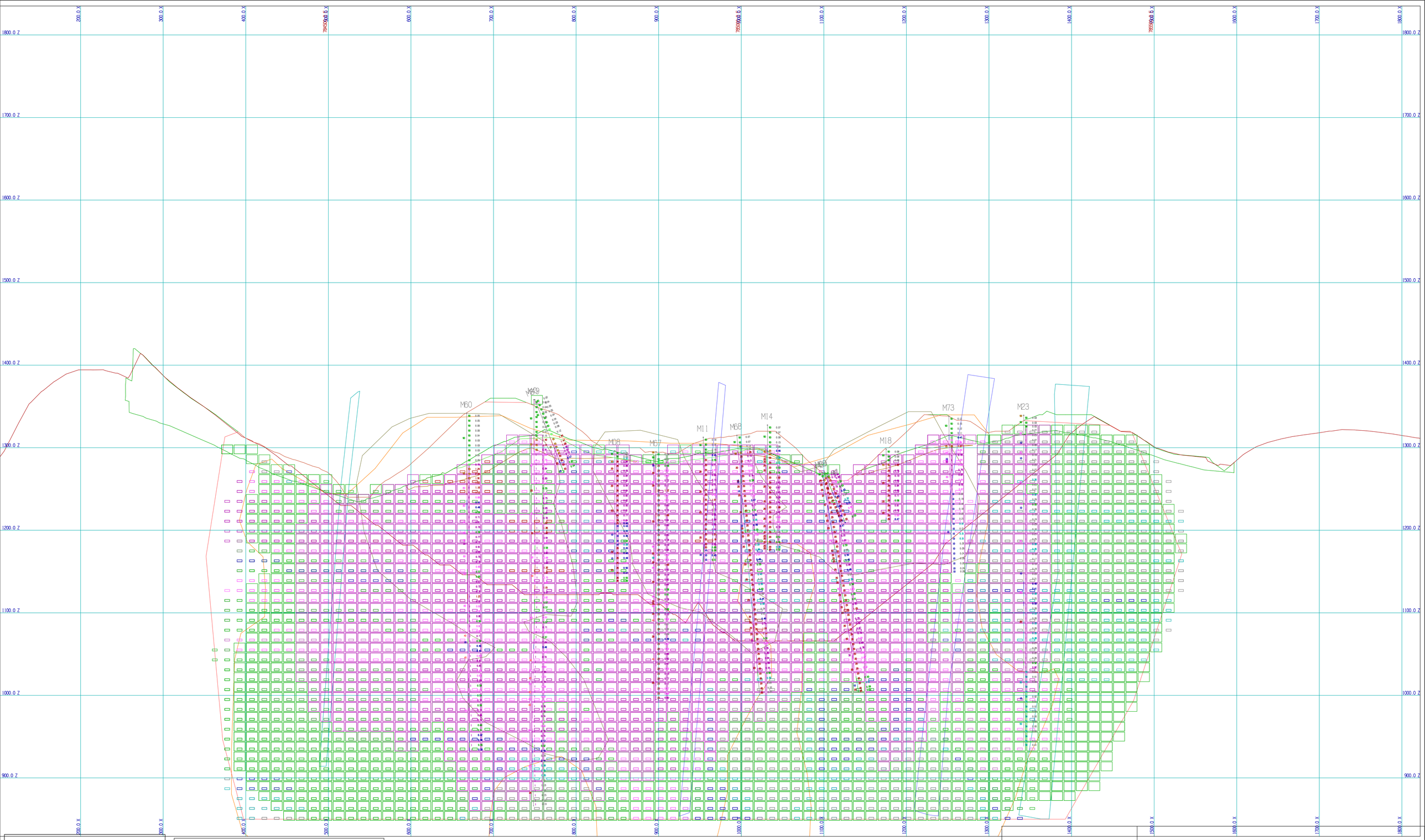
Section 4350EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

UNITS : METRES DATE: 04/10/20 TIME: 01.12.48

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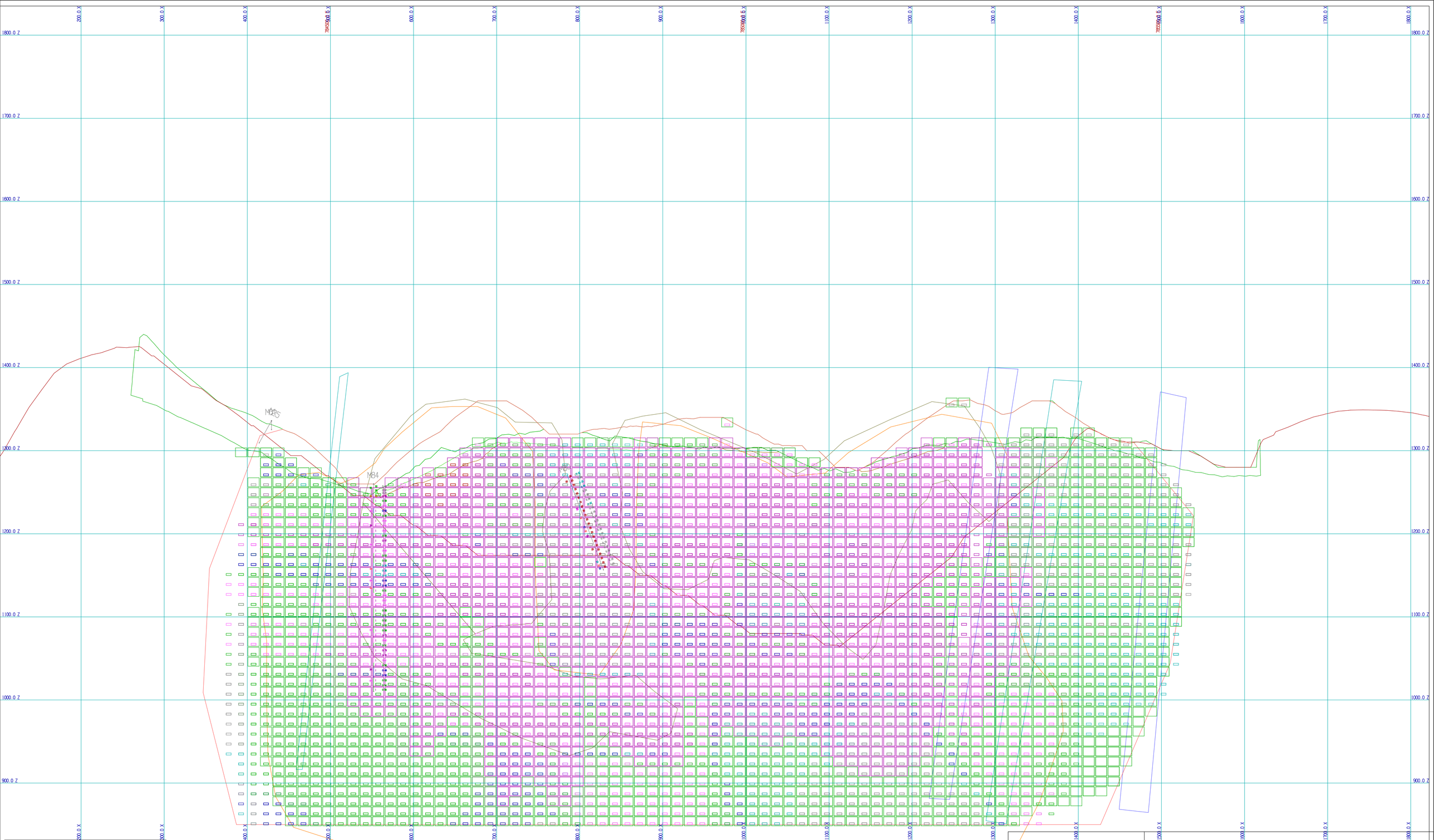
Section 4300EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU	
0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

UNITS : METRES DATE: 04/10/20 TIME: 01:12:33

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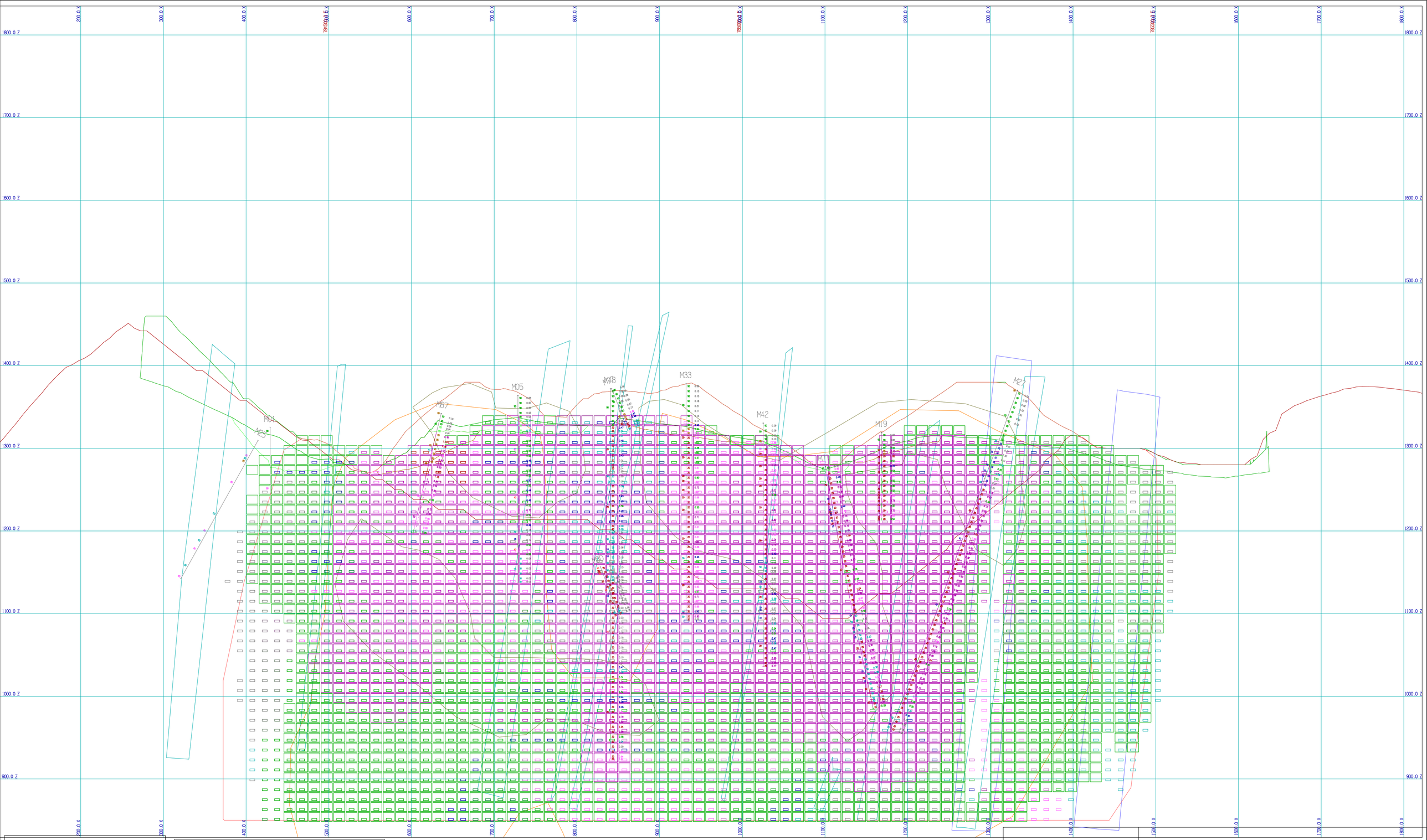
Section 4250EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

UNITS : METRES DATE: 04/10/20 TIME: 01:12:17

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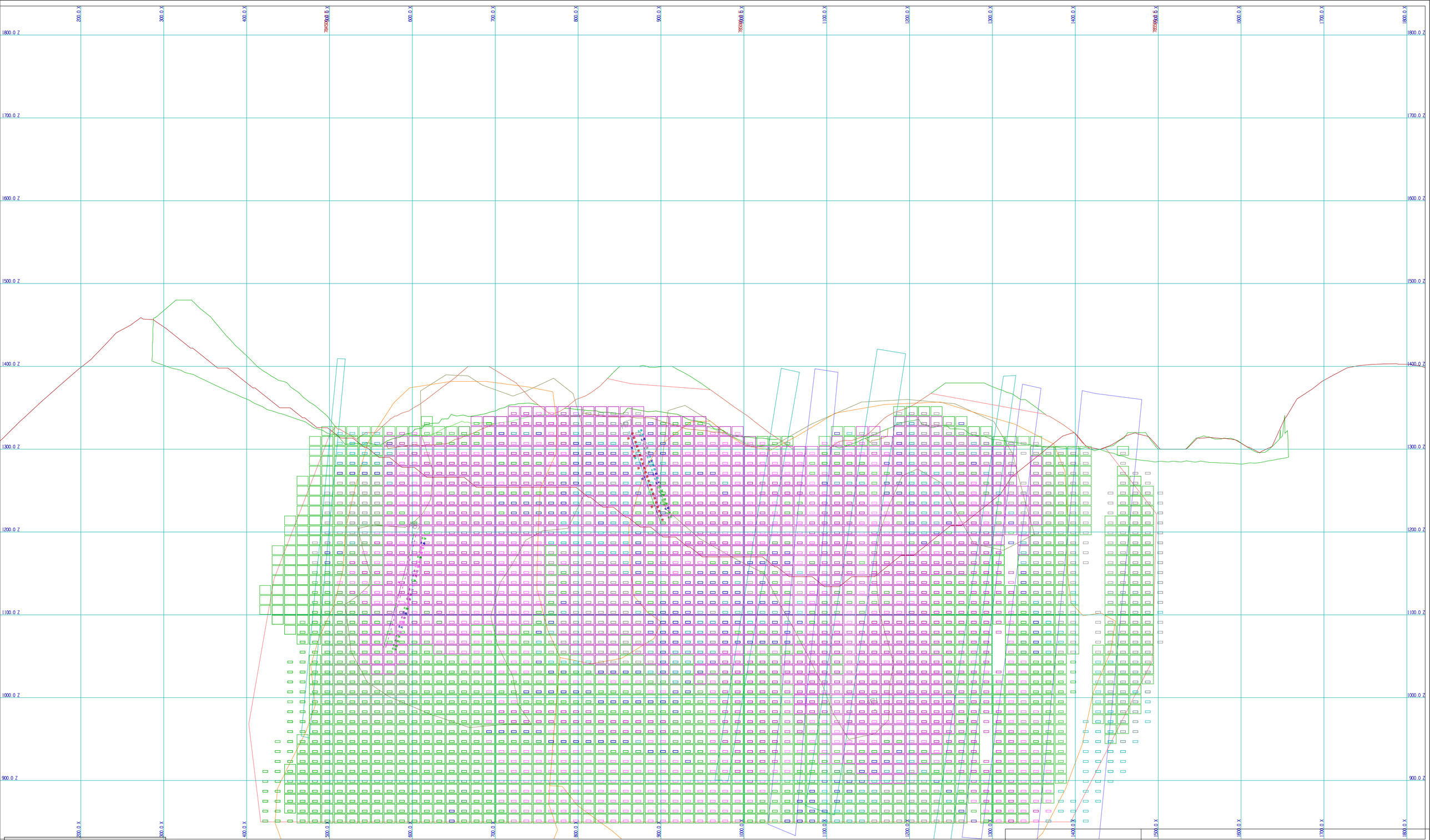
Section 4200EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300	
0.300	0.400	
0.400	0.500	
0.500	0.600	
0.600	0.700	
0.700	1.000	
1.000	99.000	

UNITS : METRES DATE: 04/10/20 TIME: 01:12:00

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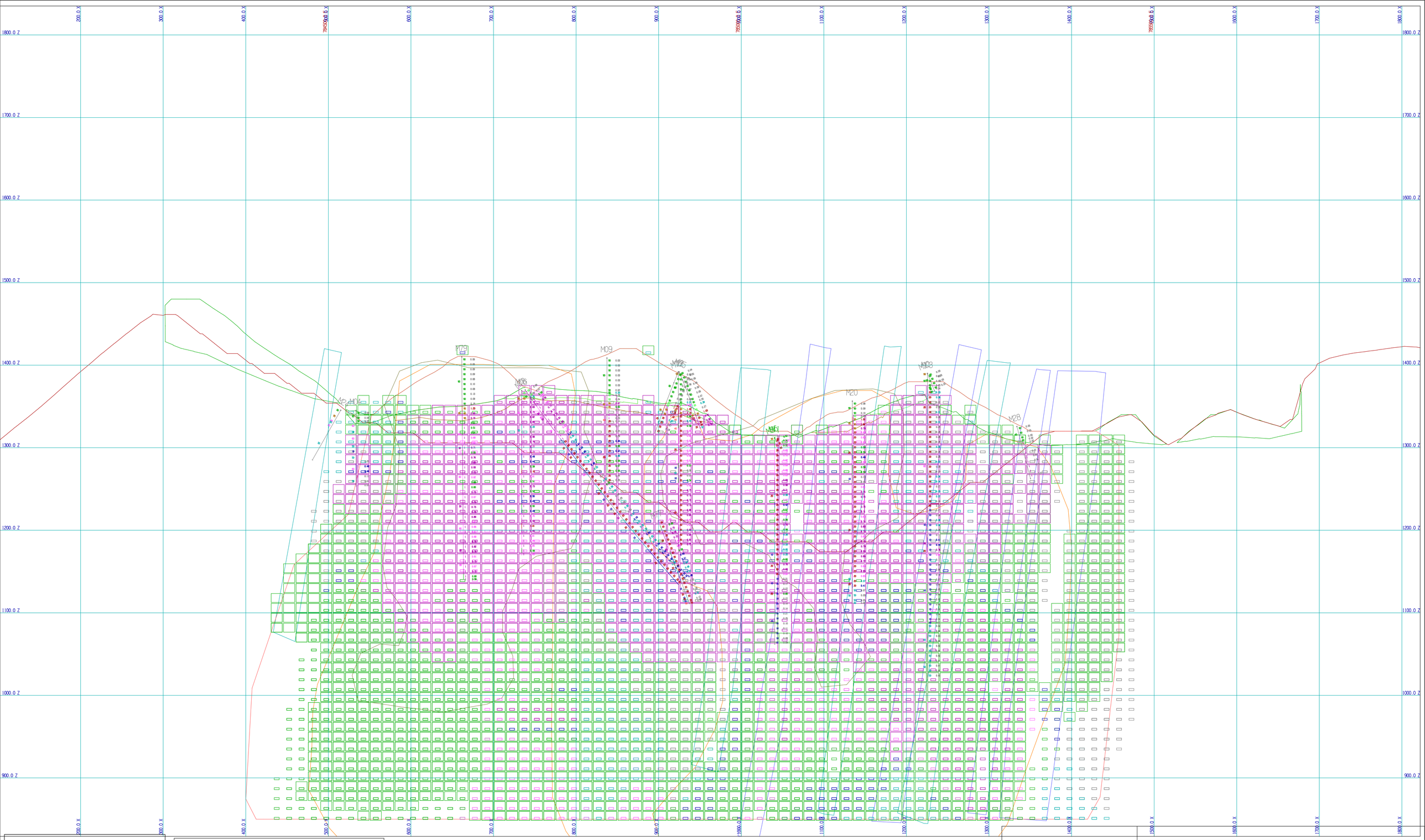
Section 4150EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

UNITS : METRES DATE: 04/10/20 TIME: 01:11:48

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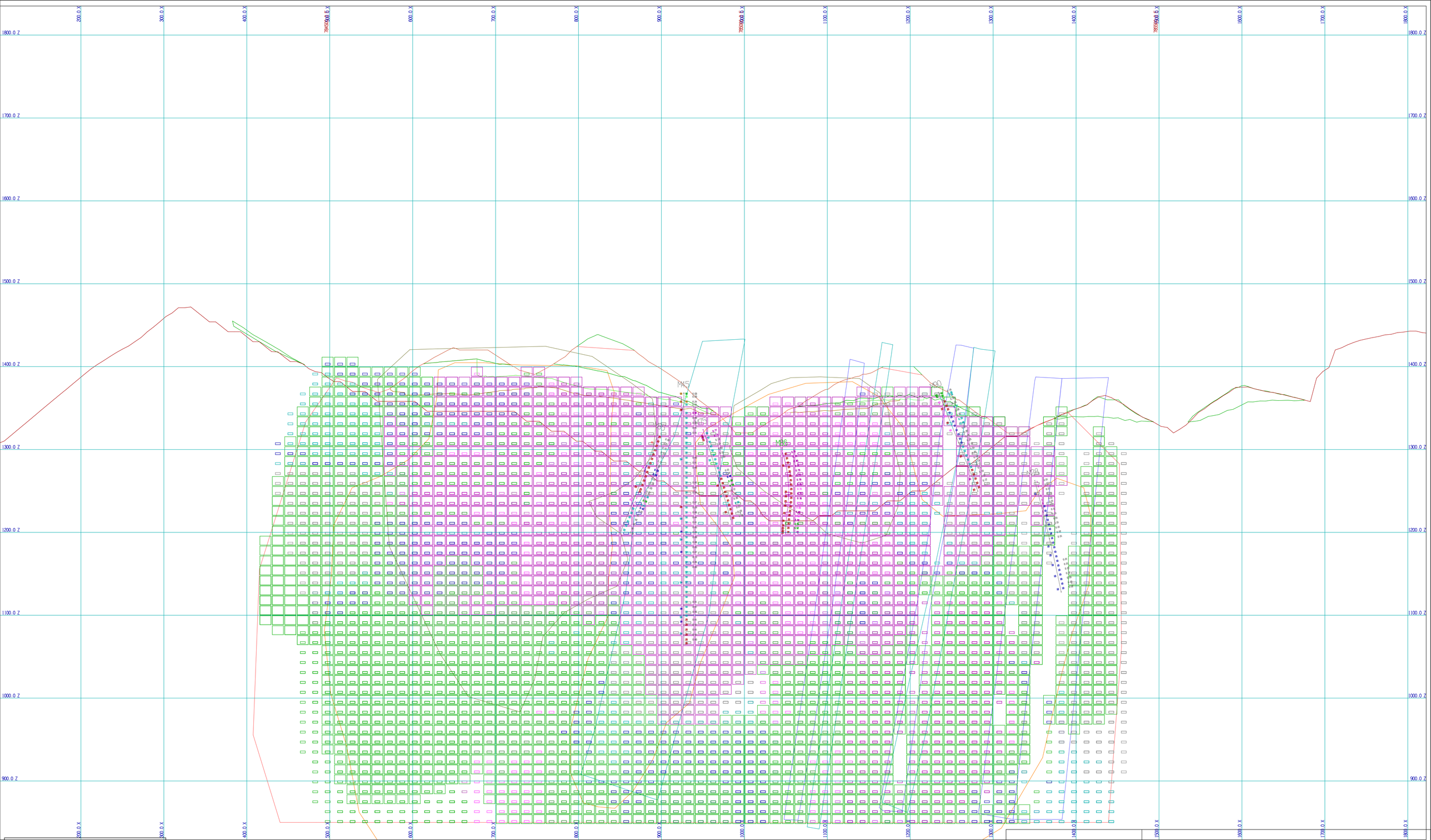
Section 4100EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

UNITS : METRES DATE: 04/10/20 TIME: 01.11.34

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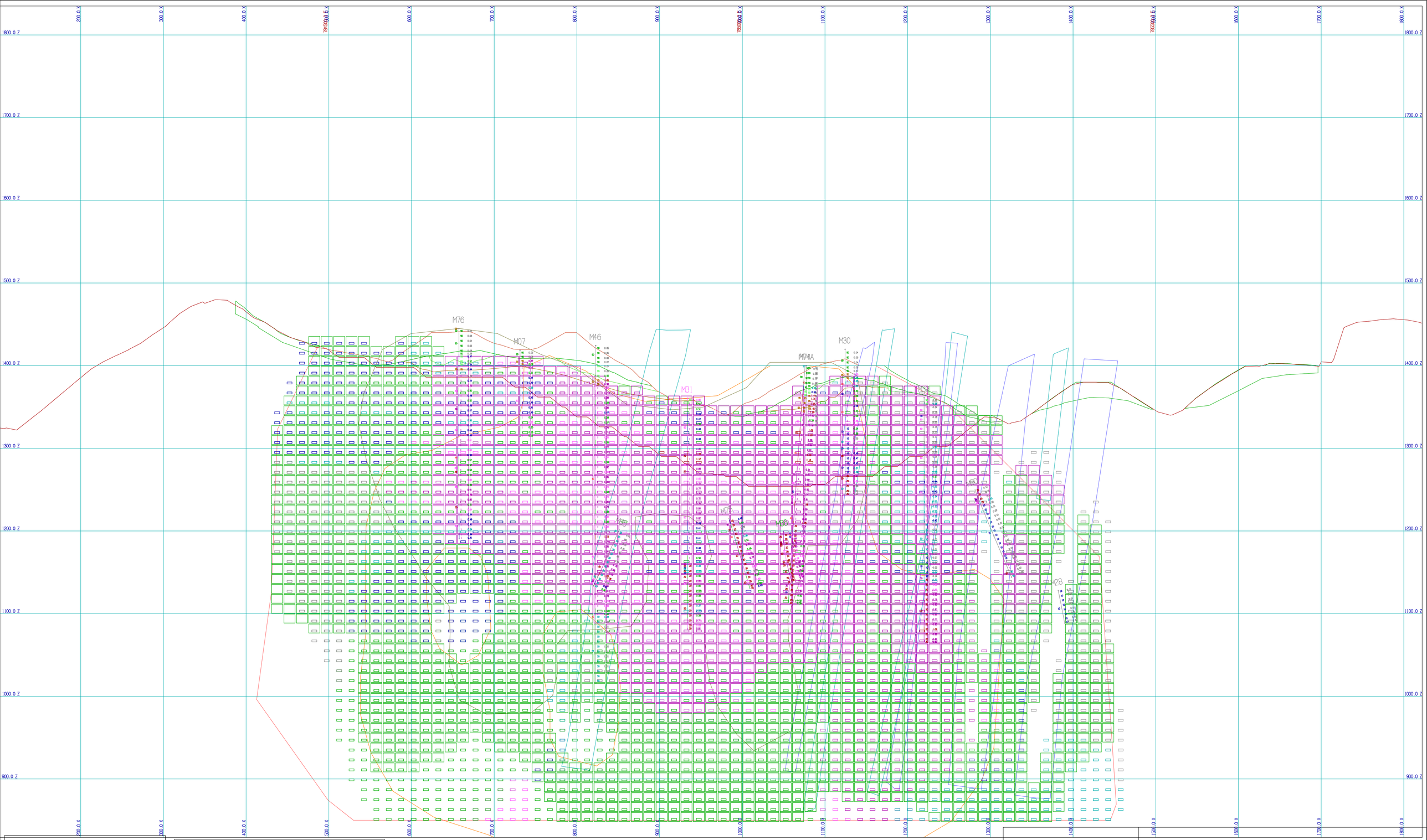
Section 4050EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

UNITS : METRES DATE: 04/10/20 TIME: 01:11:19

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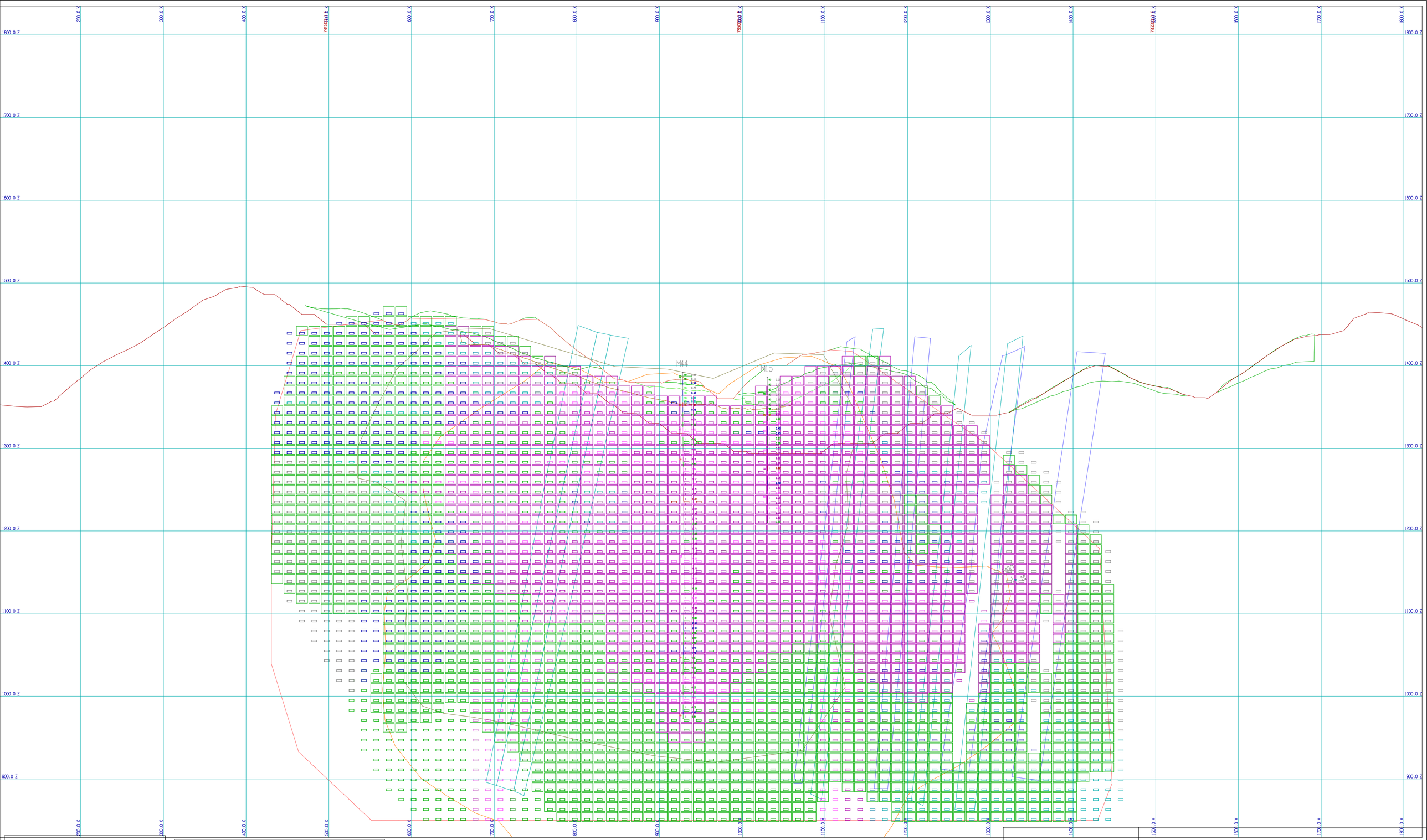
Section 4000EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

UNITS : METRES DATE: 04/10/20 TIME: 01:11:02

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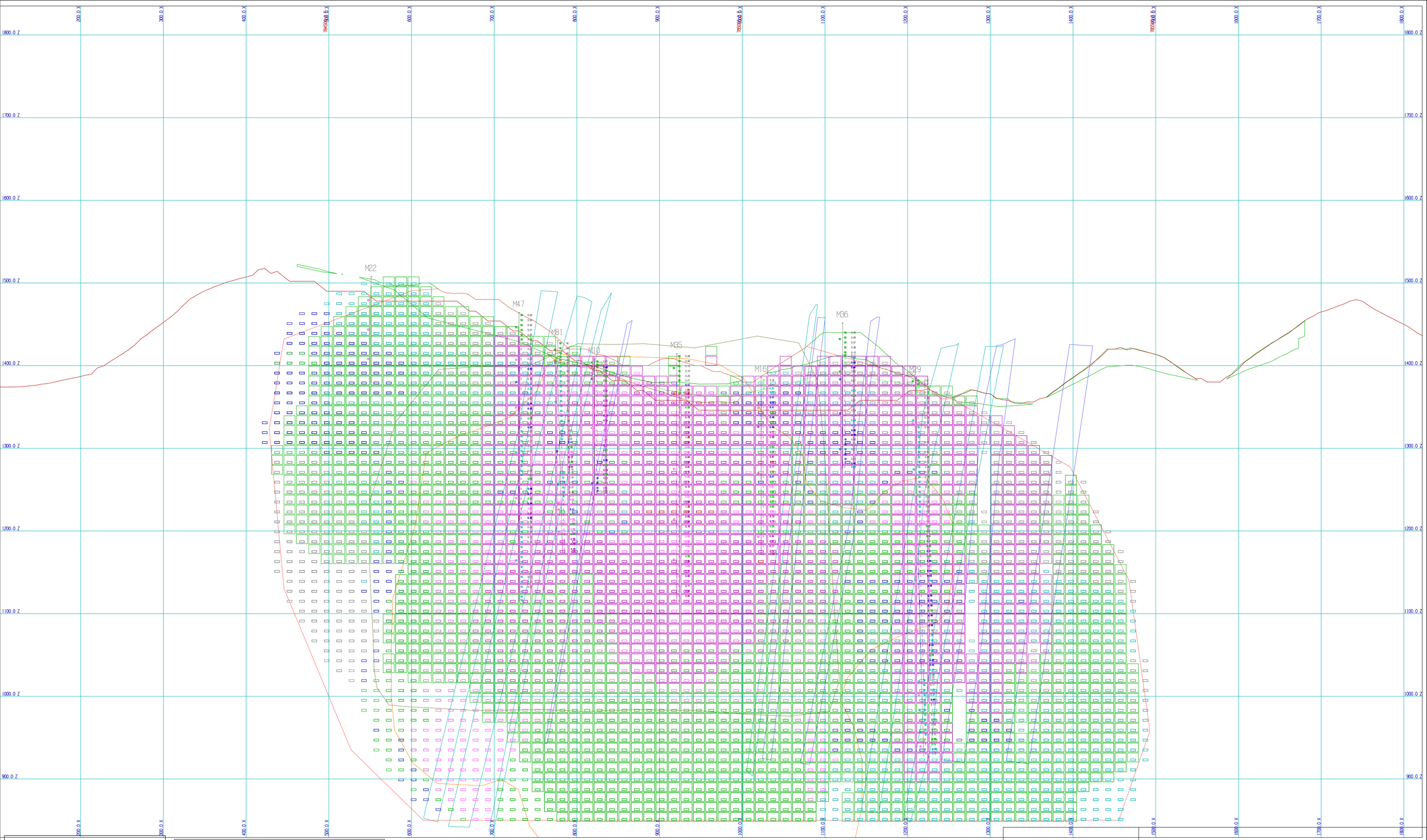
Section 3950EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

UNITS : METRES DATE: 04/10/20 TIME: 01.10.45

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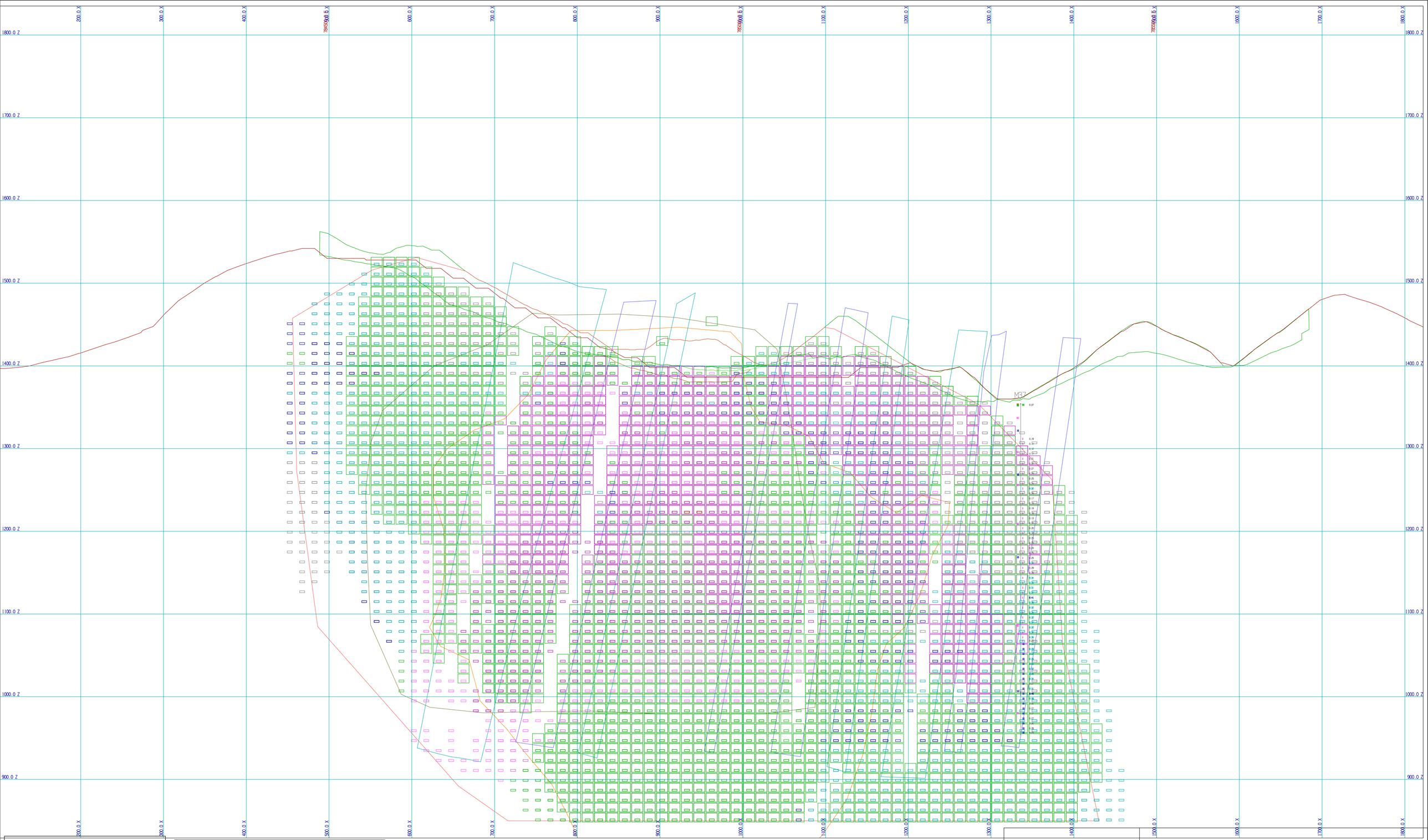
Section 3900EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300	
0.300	0.400	
0.400	0.500	
0.500	0.600	
0.600	0.700	
0.700	1.000	
1.000	99.000	

UNITS : METRES DATE: 04/10/20 TIME: 01.10.29

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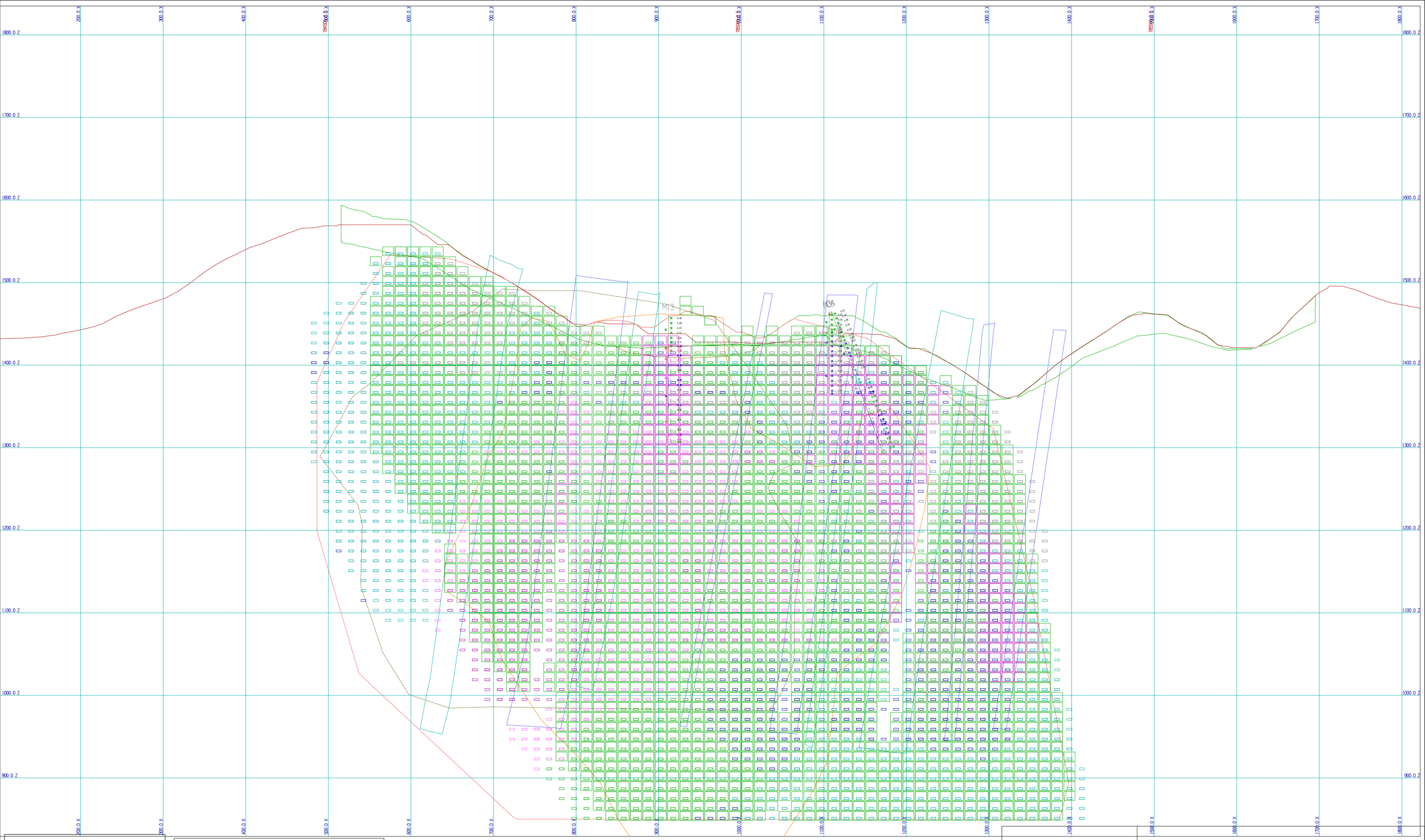
Section 3850EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

UNITS : METRES DATE: 04/10/20 TIME: 01.10.14

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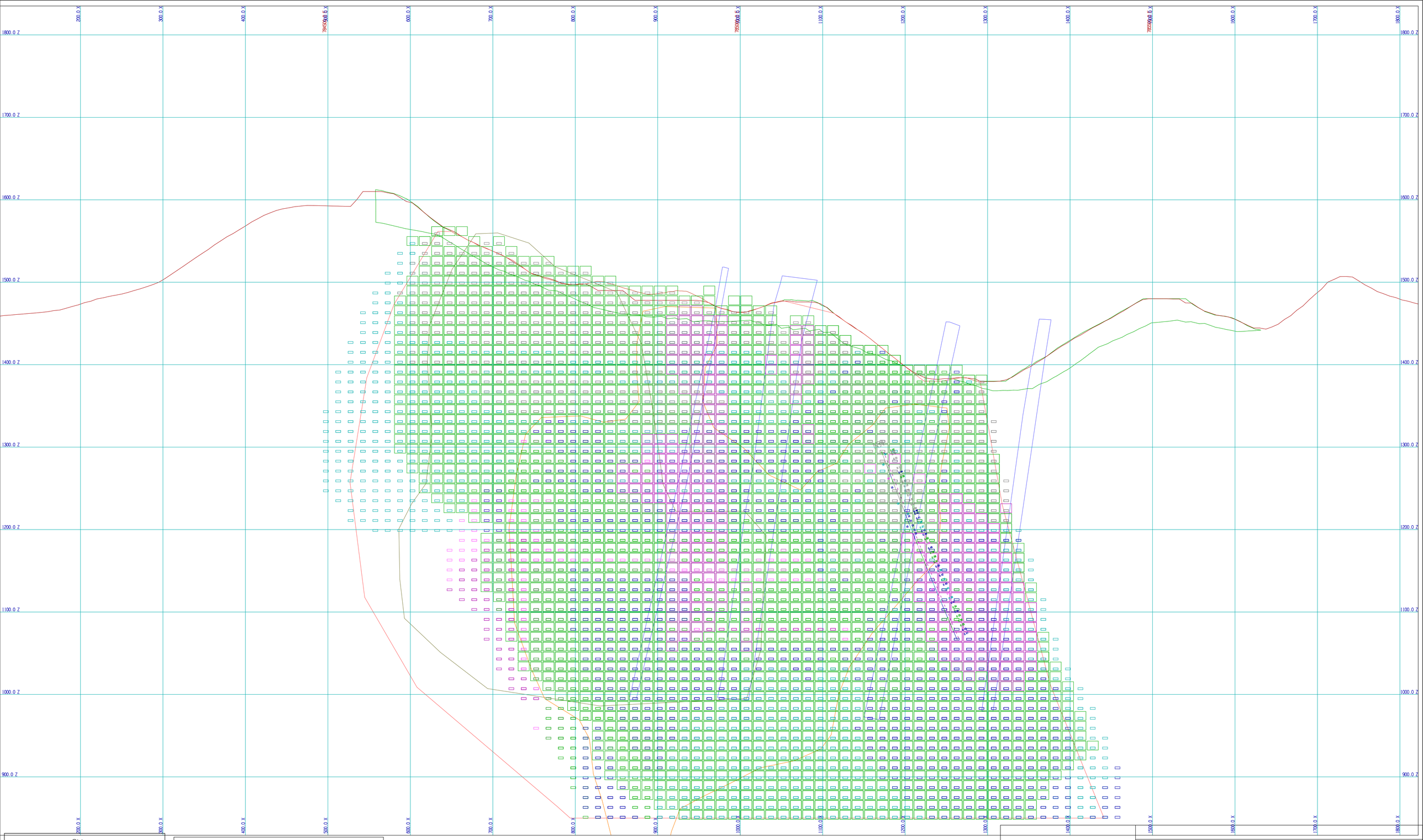
Section 3800EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

UNITS : METRES DATE: 04/10/20 TIME: 01:09:56

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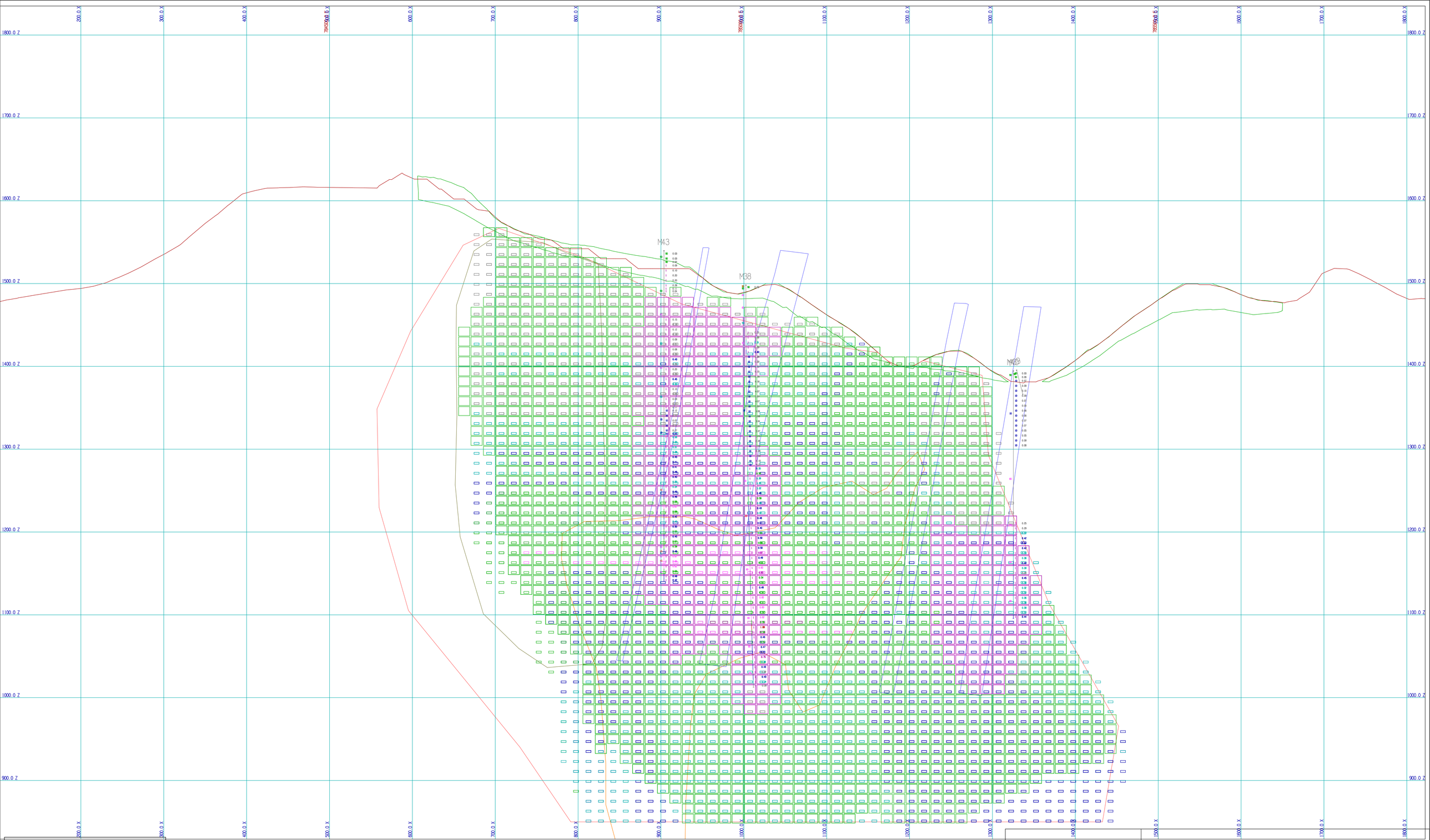
Section 3750EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU	
0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

UNITS : METRES DATE: 04/10/20 TIME: 01:09:40

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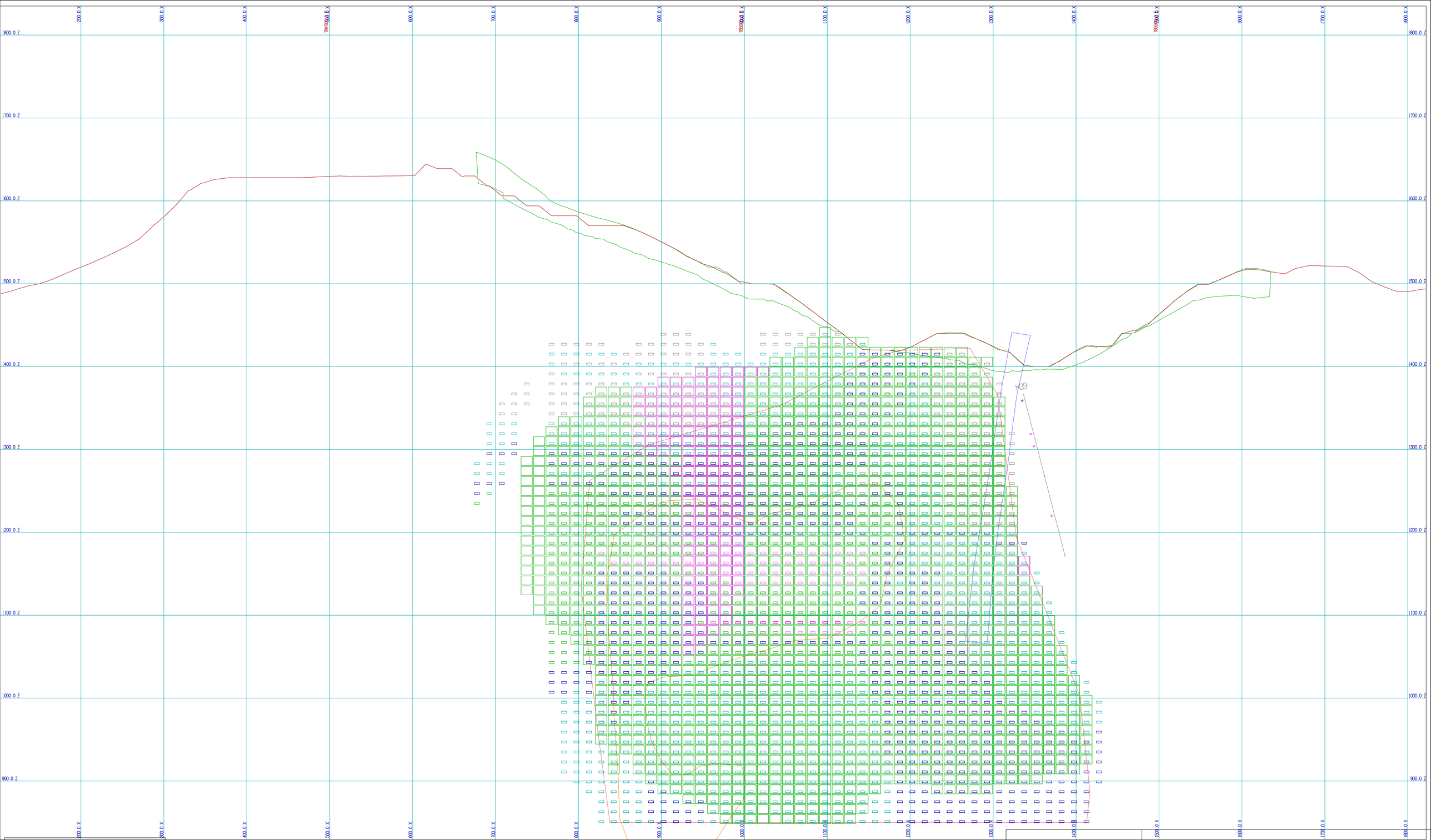
Section 3700EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300	
0.300	0.400	
0.400	0.500	
0.500	0.600	
0.600	0.700	
0.700	1.000	
1.000	99.000	

UNITS : METRES DATE: 04/10/20 TIME: 01:09:27

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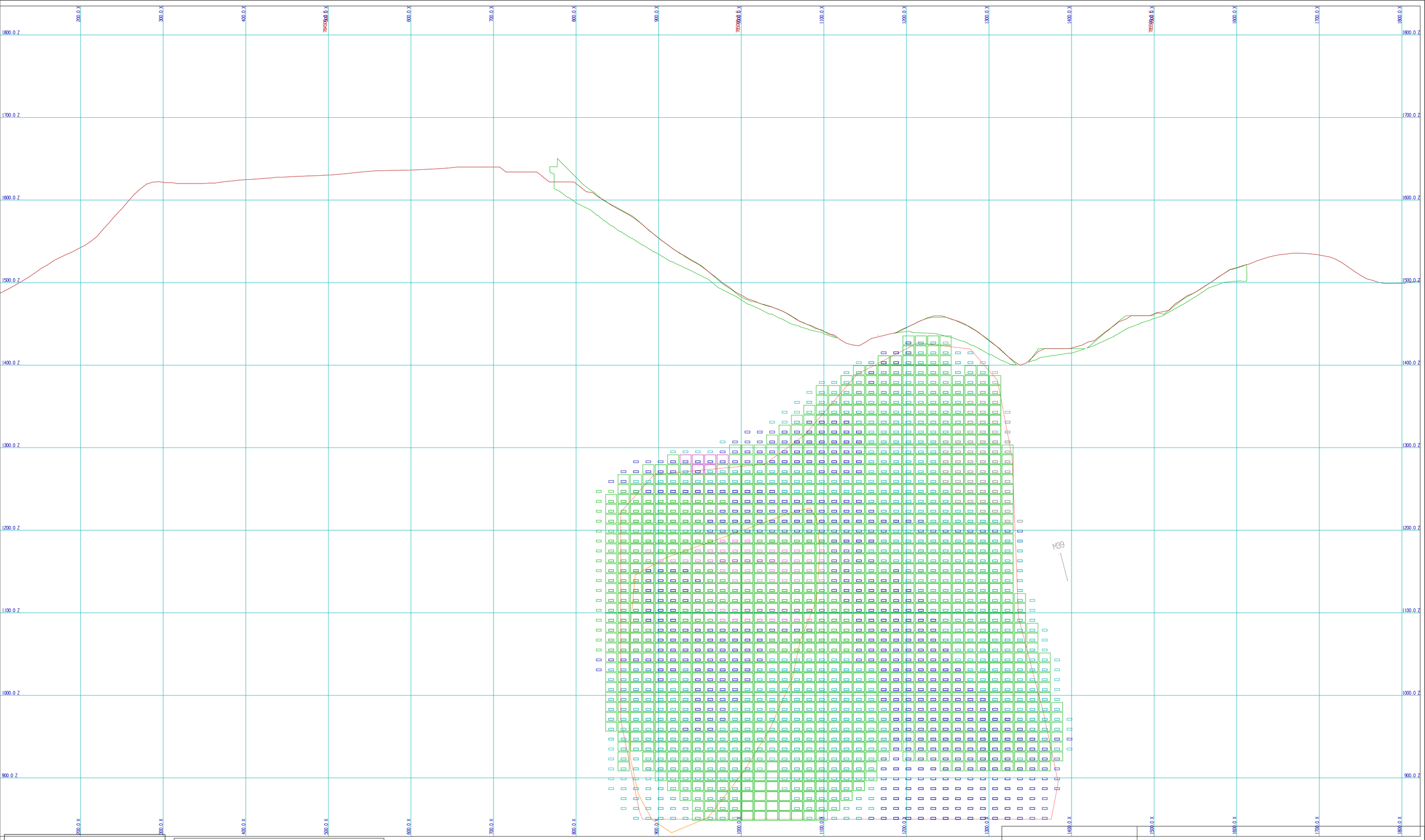
Section 3650EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



CU

0.001	0.300	
0.300	0.400	
0.400	0.500	
0.500	0.600	
0.600	0.700	
0.700	1.000	
1.000	99.000	

UNITS : METRES DATE: 04/10/20 TIME: 01:09:14

DRAWN BY :

Section 3600EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International

CU	
0.001	0.300
0.300	0.400
0.400	0.500
0.500	0.600
0.600	0.700
0.700	1.000
1.000	99.000

UNITS : METRES DATE: 04/10/20 TIME: 01:14:06

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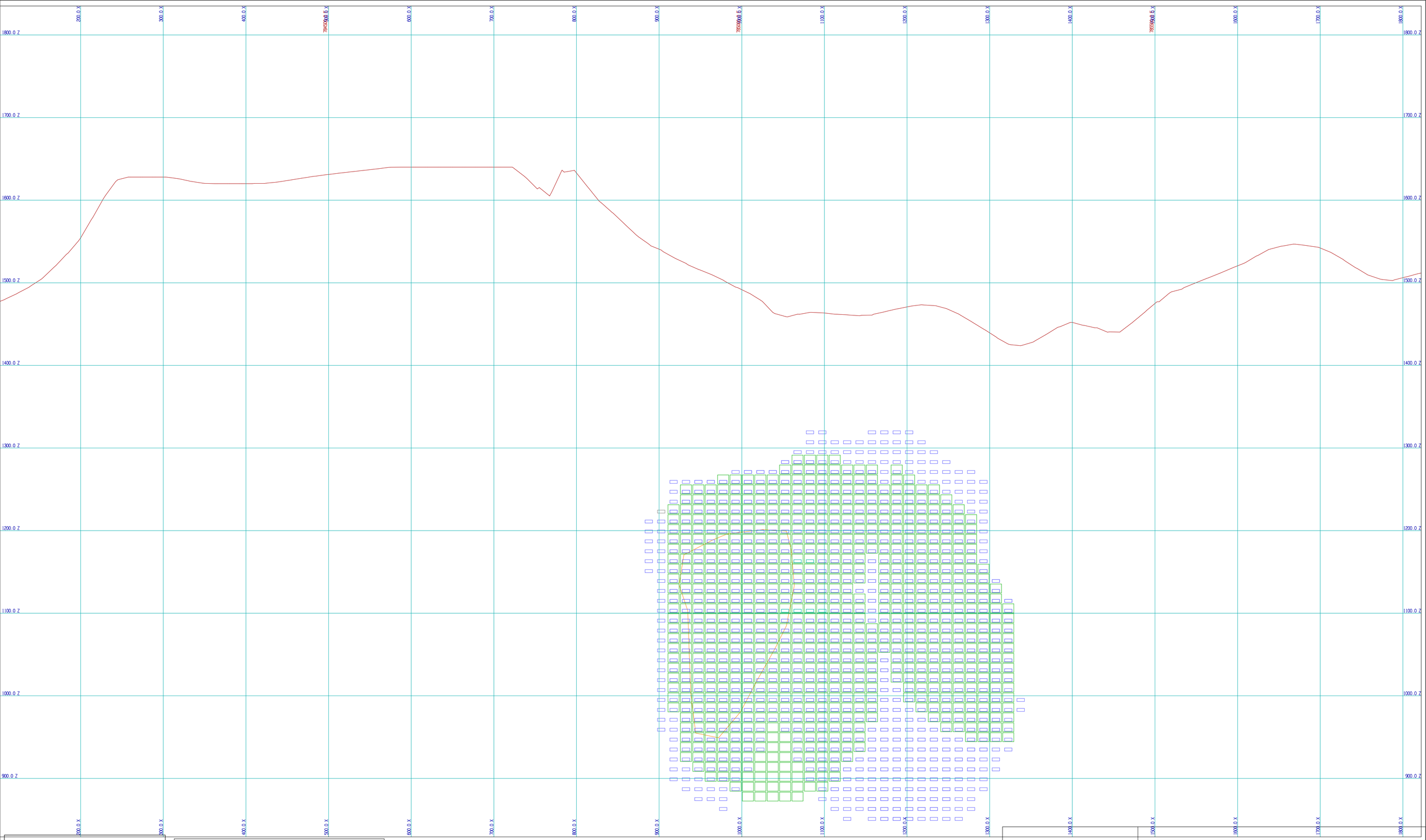
Section 4700EW Mirador Project

Block Model Plots Cu Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100	
0.100	0.150	
0.150	0.200	
0.200	0.250	
0.250	0.300	
0.300	0.500	
0.500	10.000	

UNITS : METRES DATE: 04/10/20 TIME: 01.00.11

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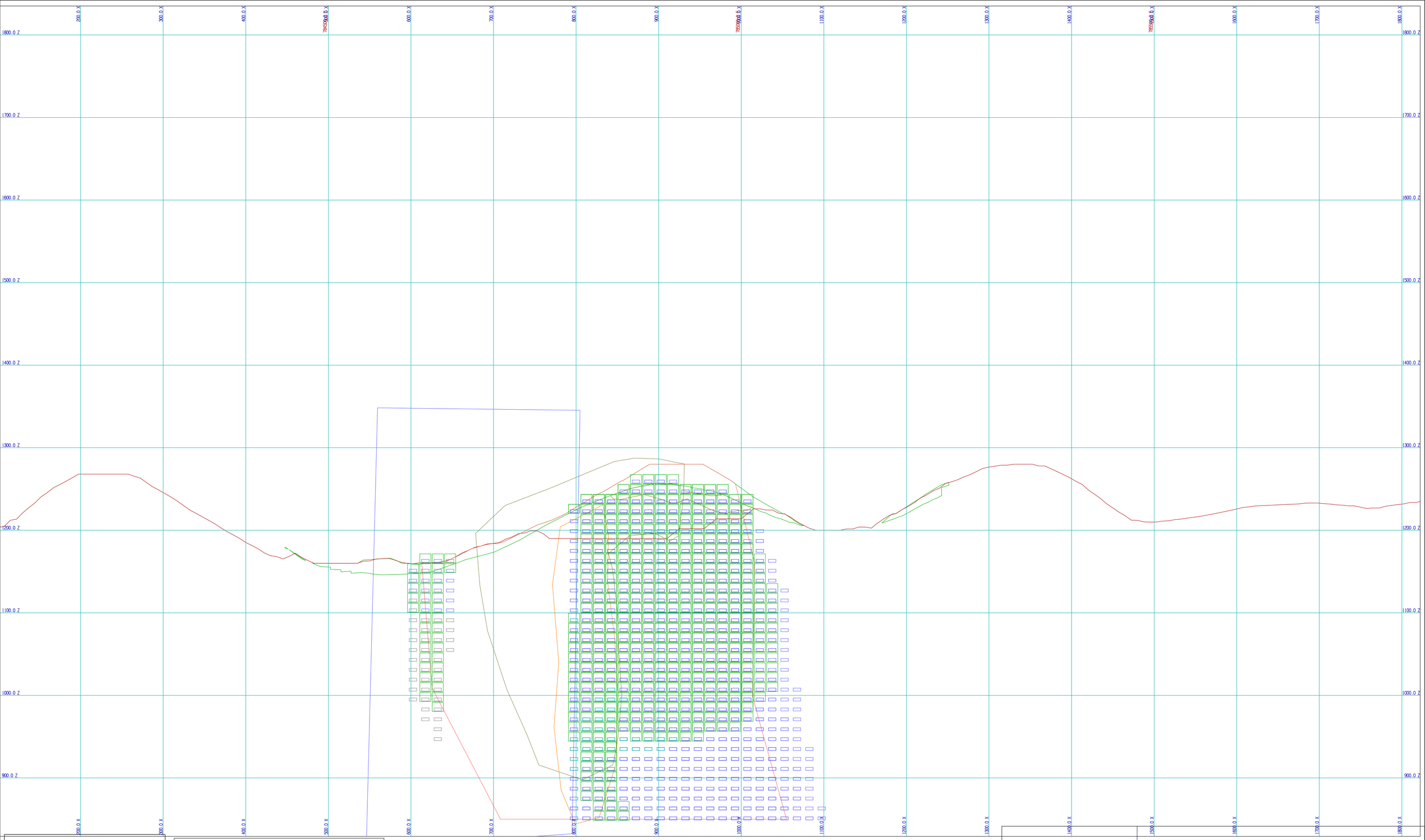
Section 3550EW Mirador Project

Block Model Plots Au Block Values

Class=blackoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:04:21

DRAWN BY :

Section 4650EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International

M61

M57

M83

AU	
0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:04:18

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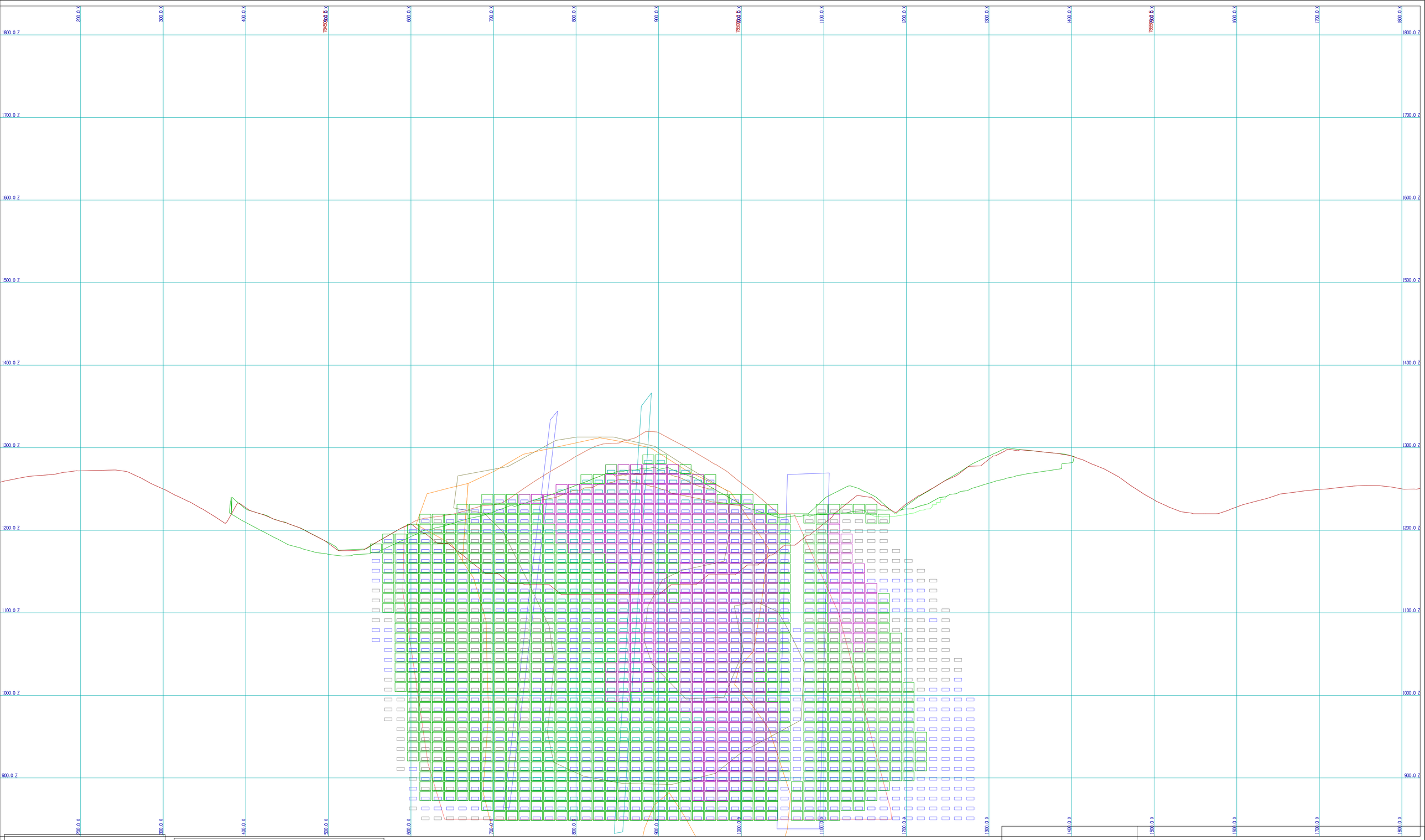
Section 4600EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:04:15

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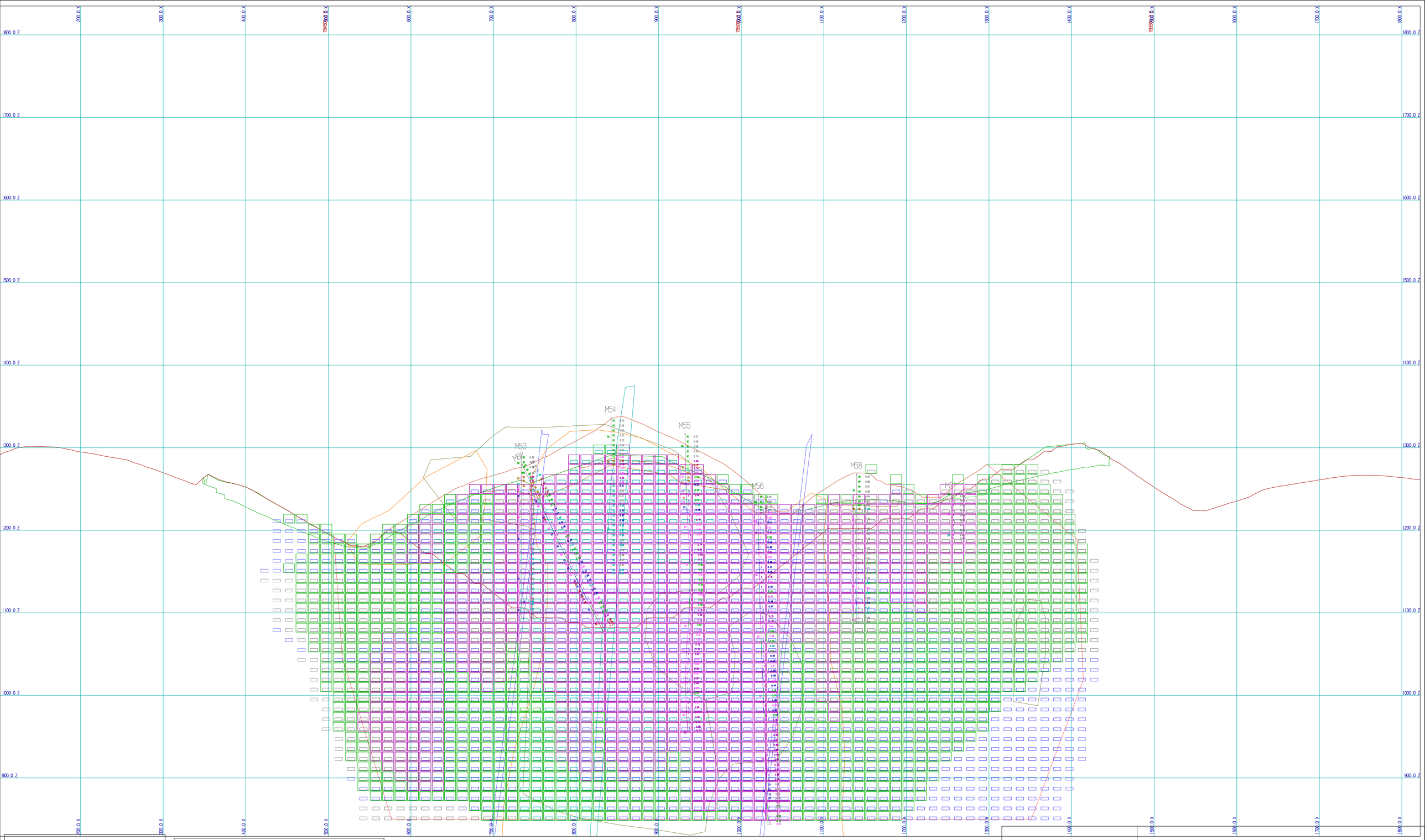
Section 4550EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:04:00

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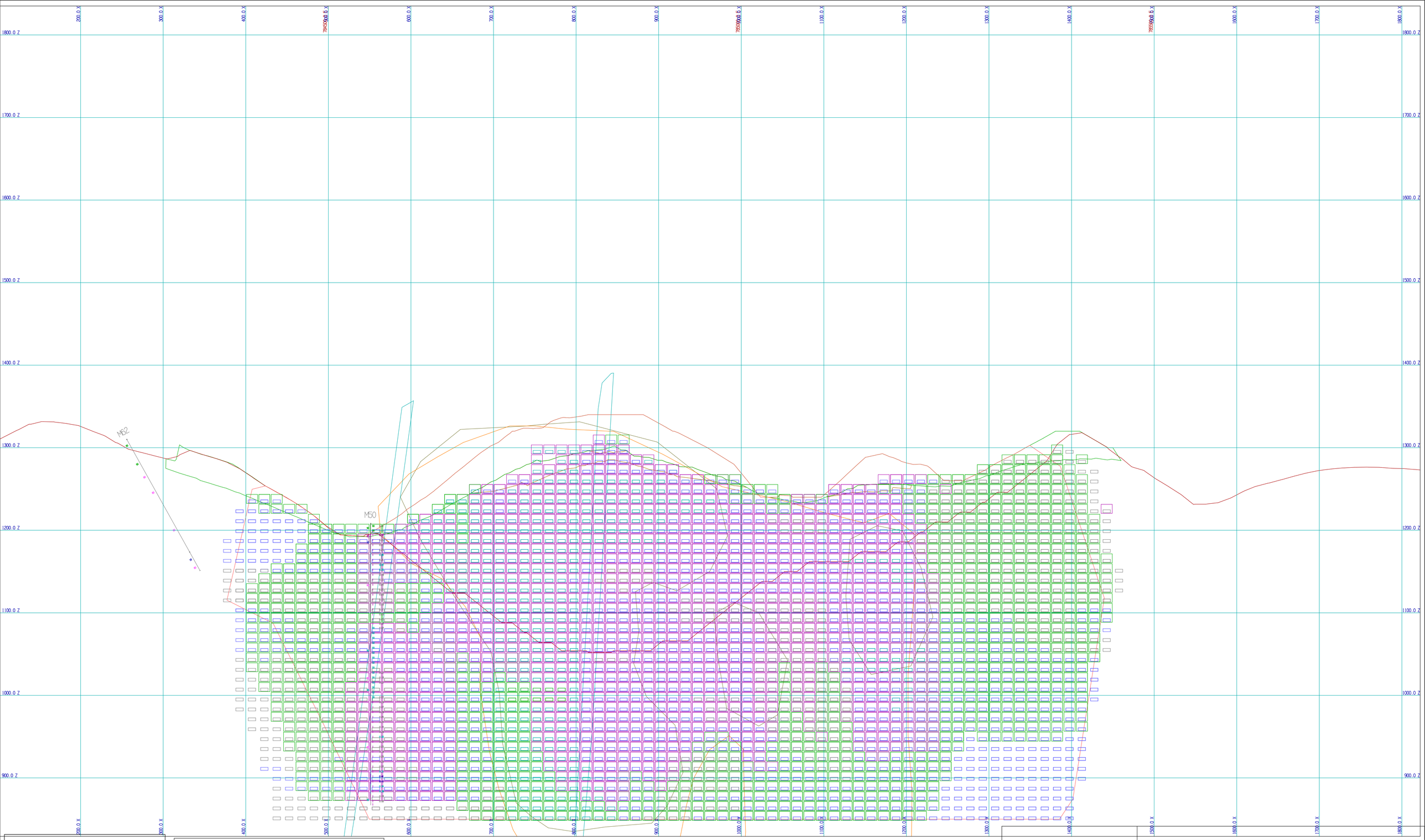
Section 4500EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:03:56

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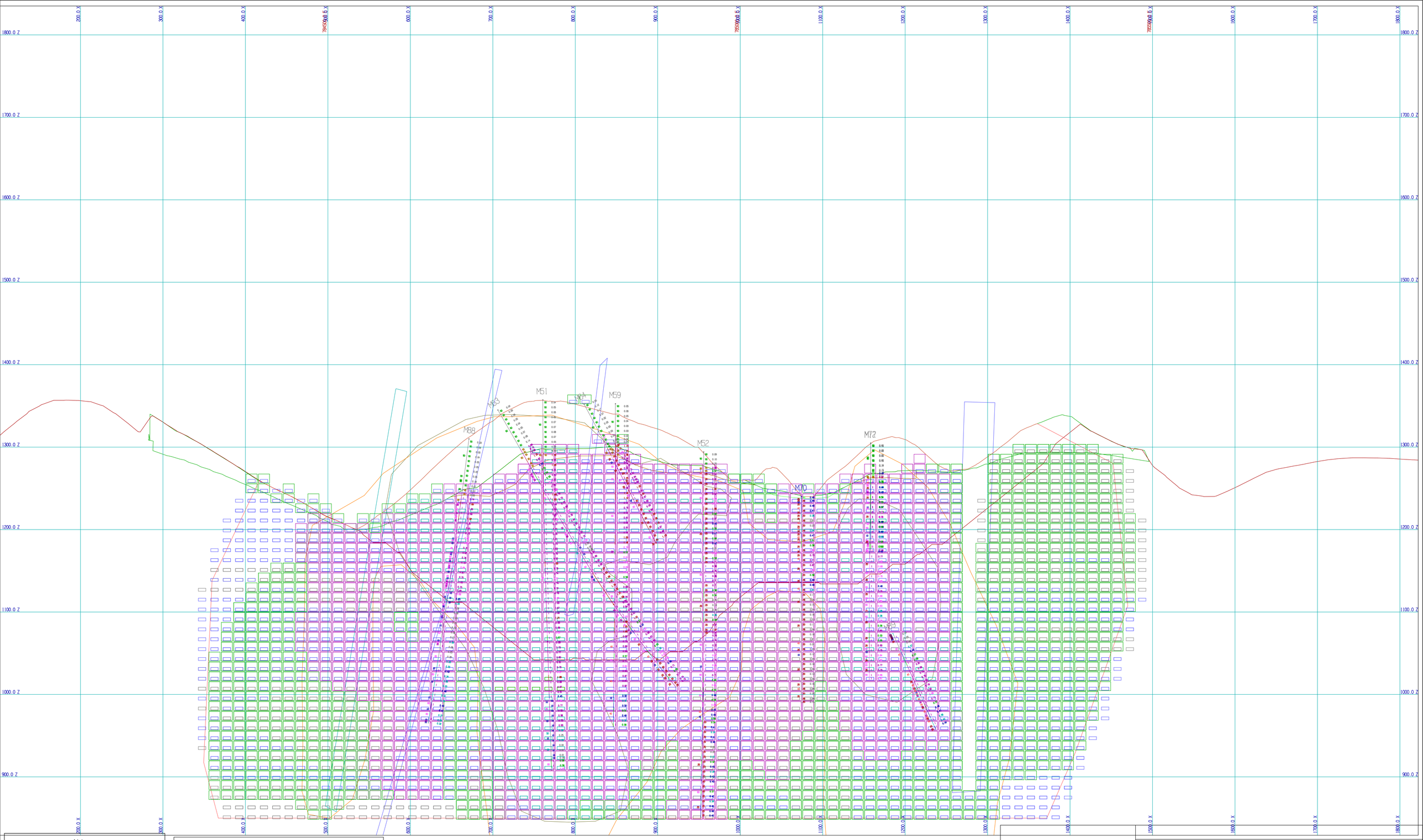
Section 4450EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:03:48

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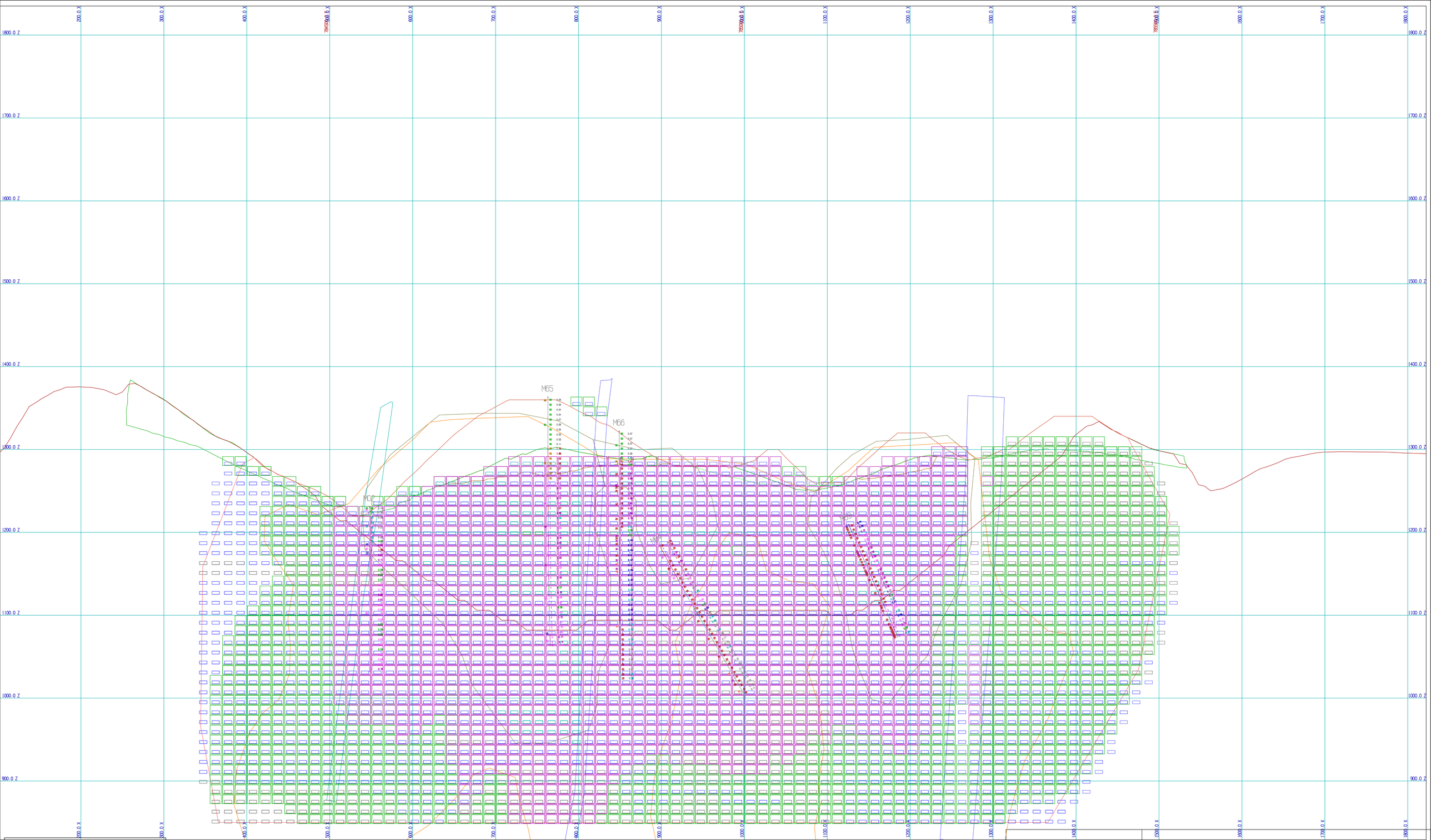
Section 4400EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:03:37

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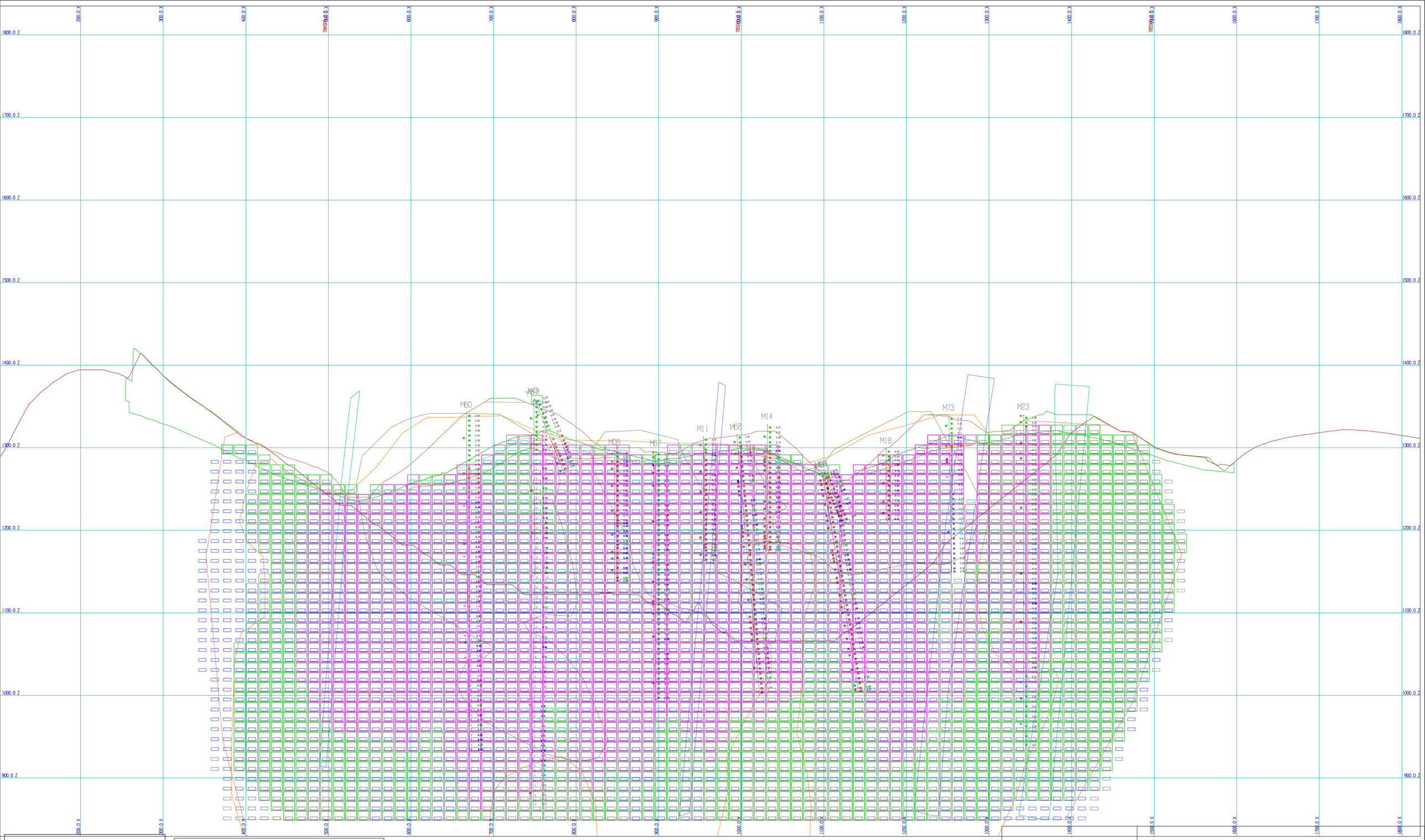
Section 4350EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:03:20

DRAWN BY :

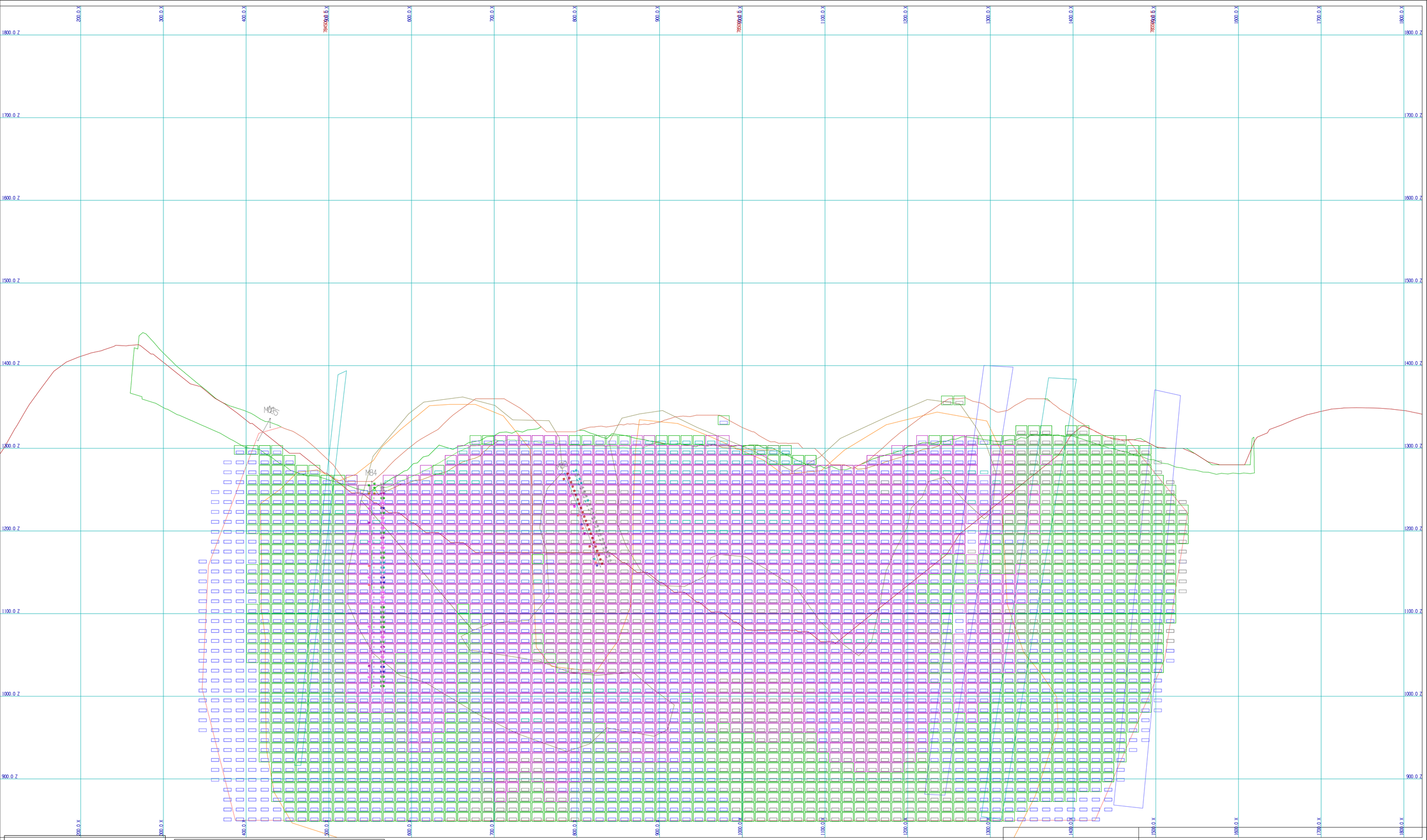
Section 4300EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:03:05

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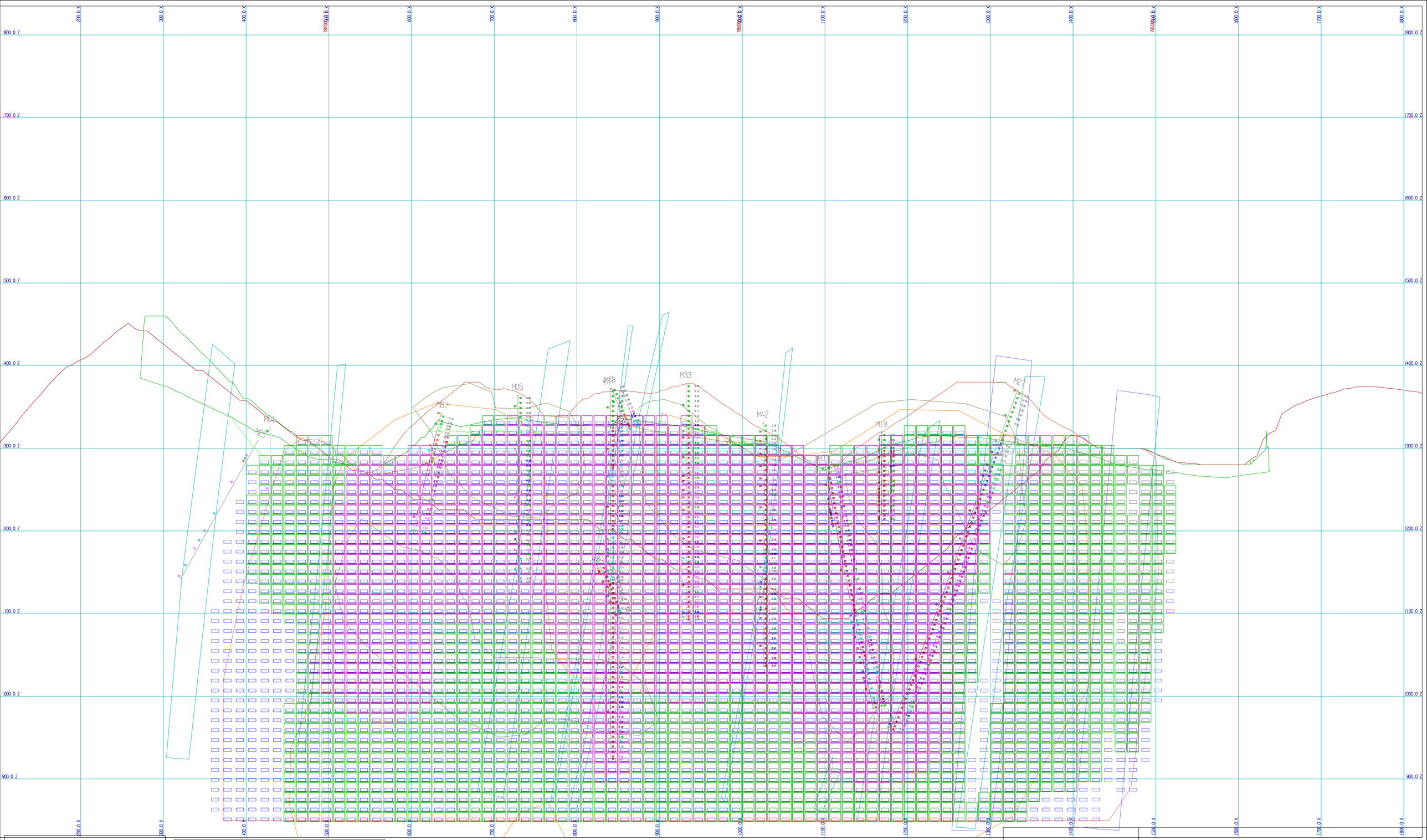
Section 4250EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:02:48

DRAWN BY :

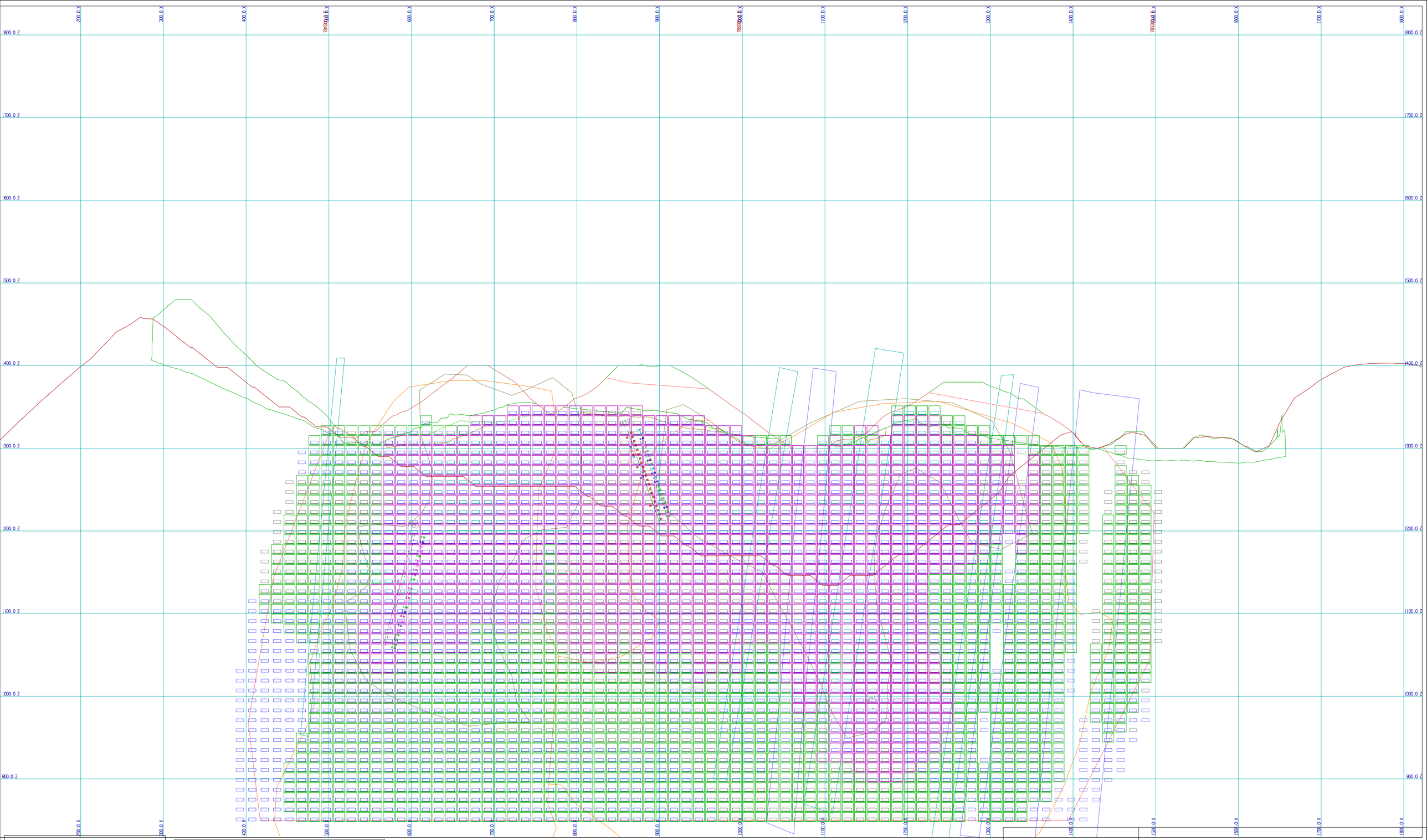
Section 4200EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:02:32

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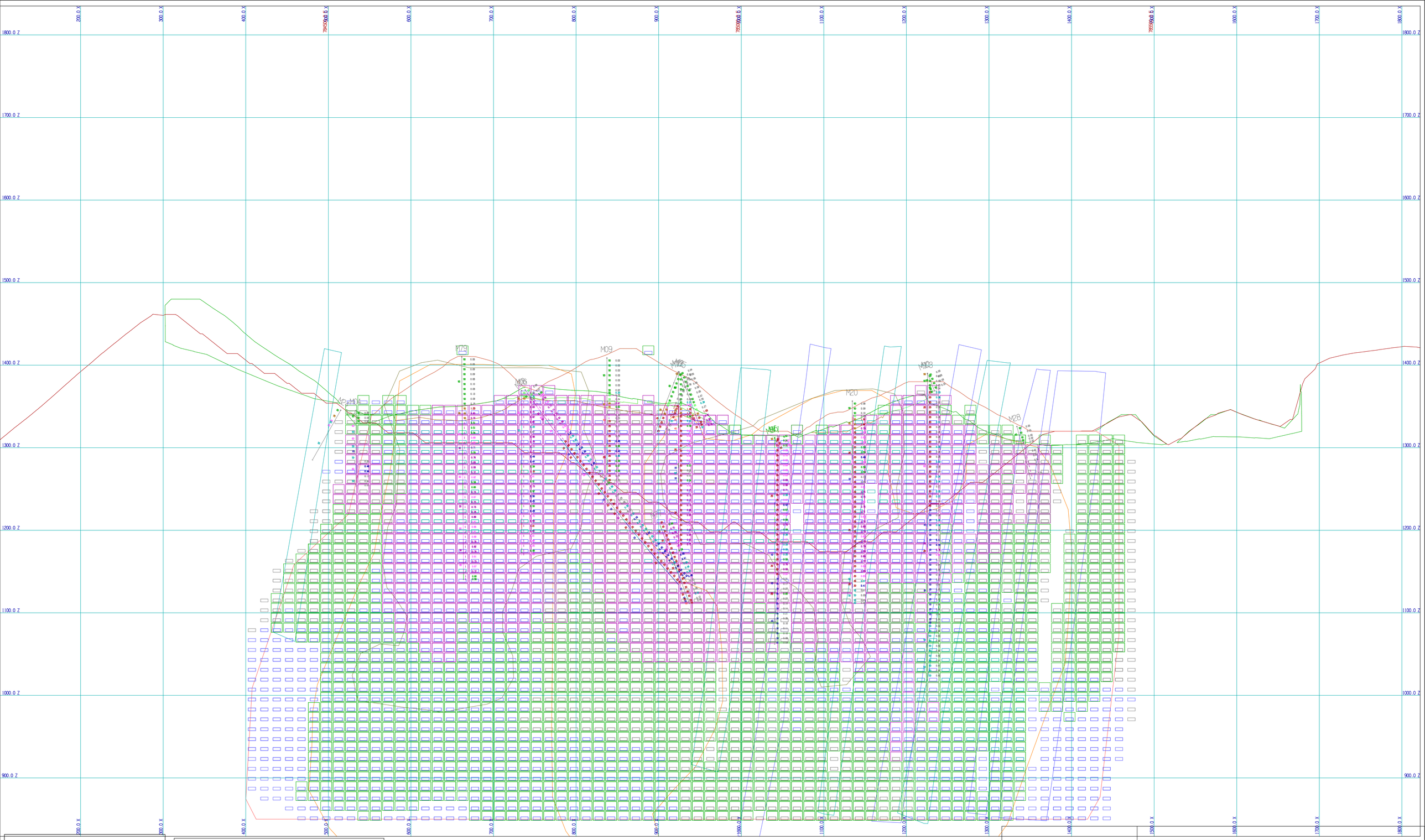
Section 4150EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:02:15

DRAWN BY :

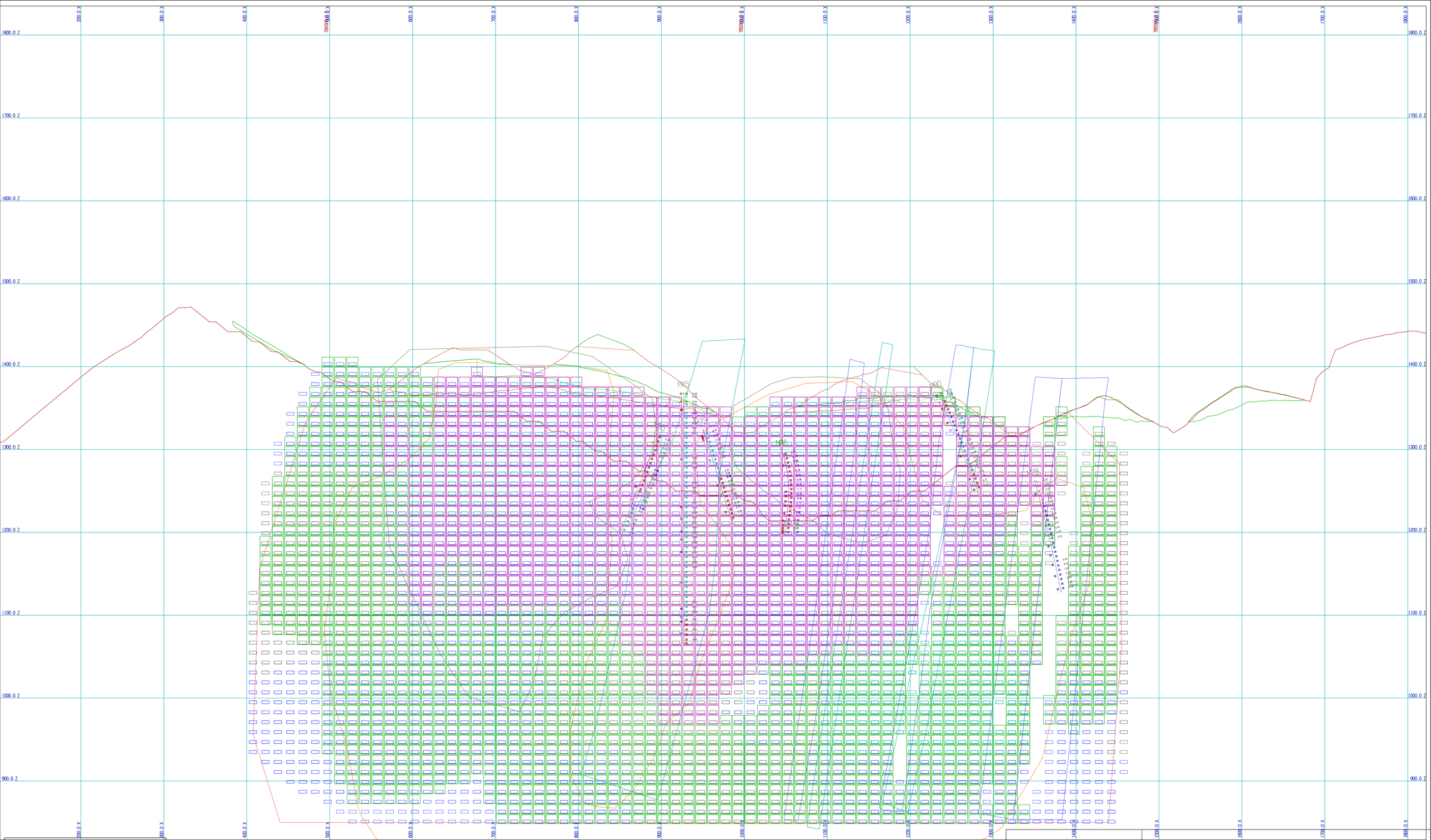
Section 4100EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01.02.04

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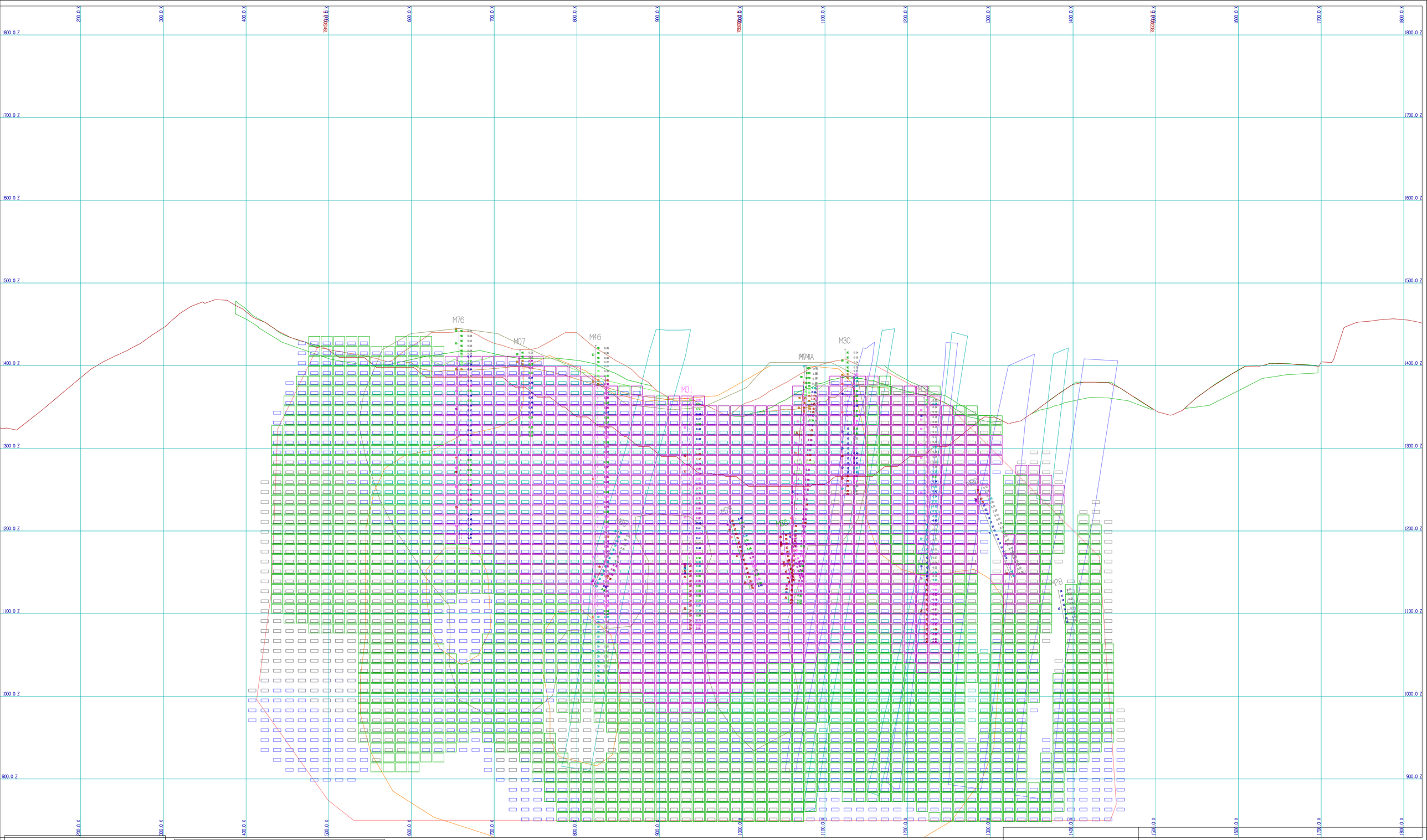
Section 4050EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:01:50

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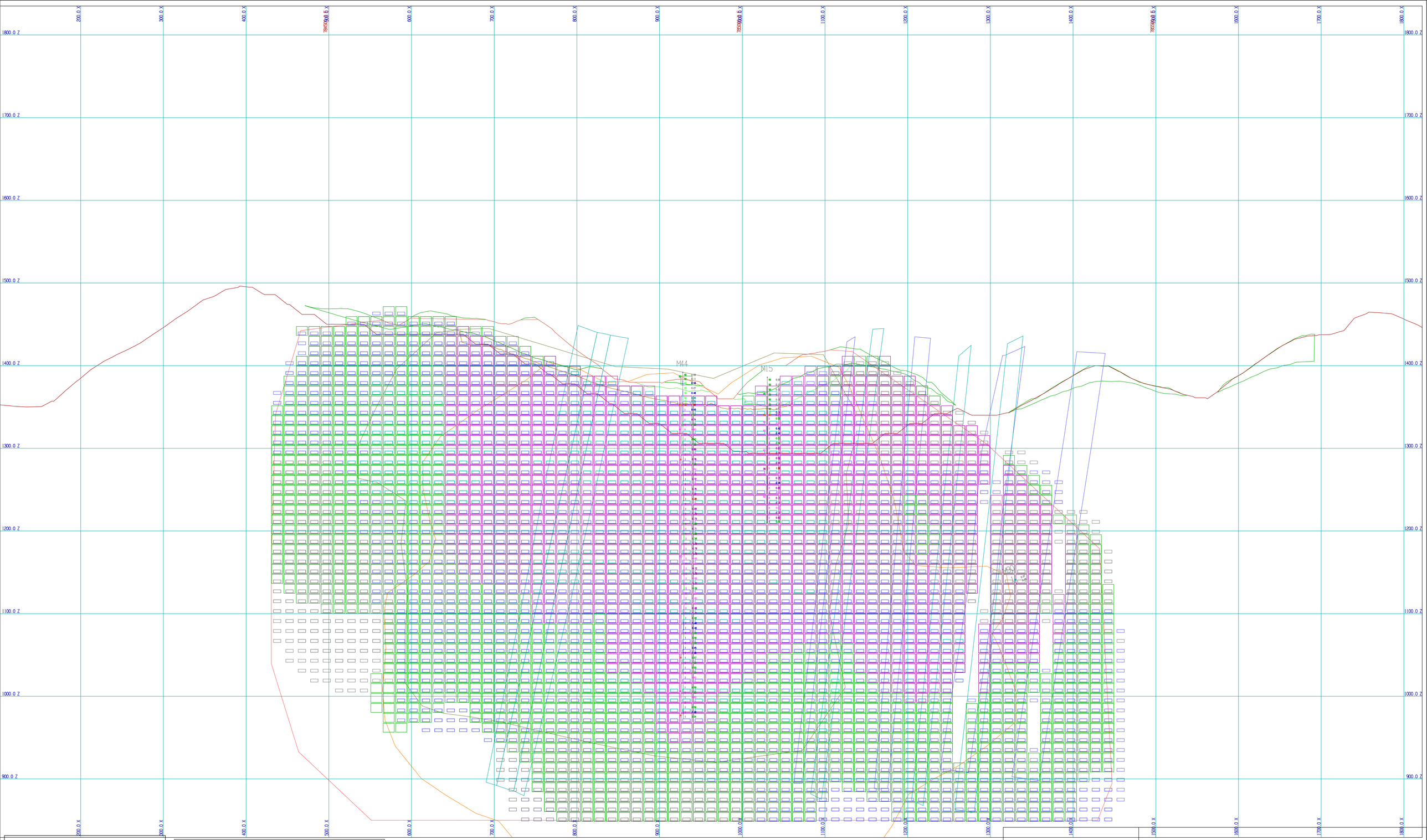
Section 4000EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:01:39

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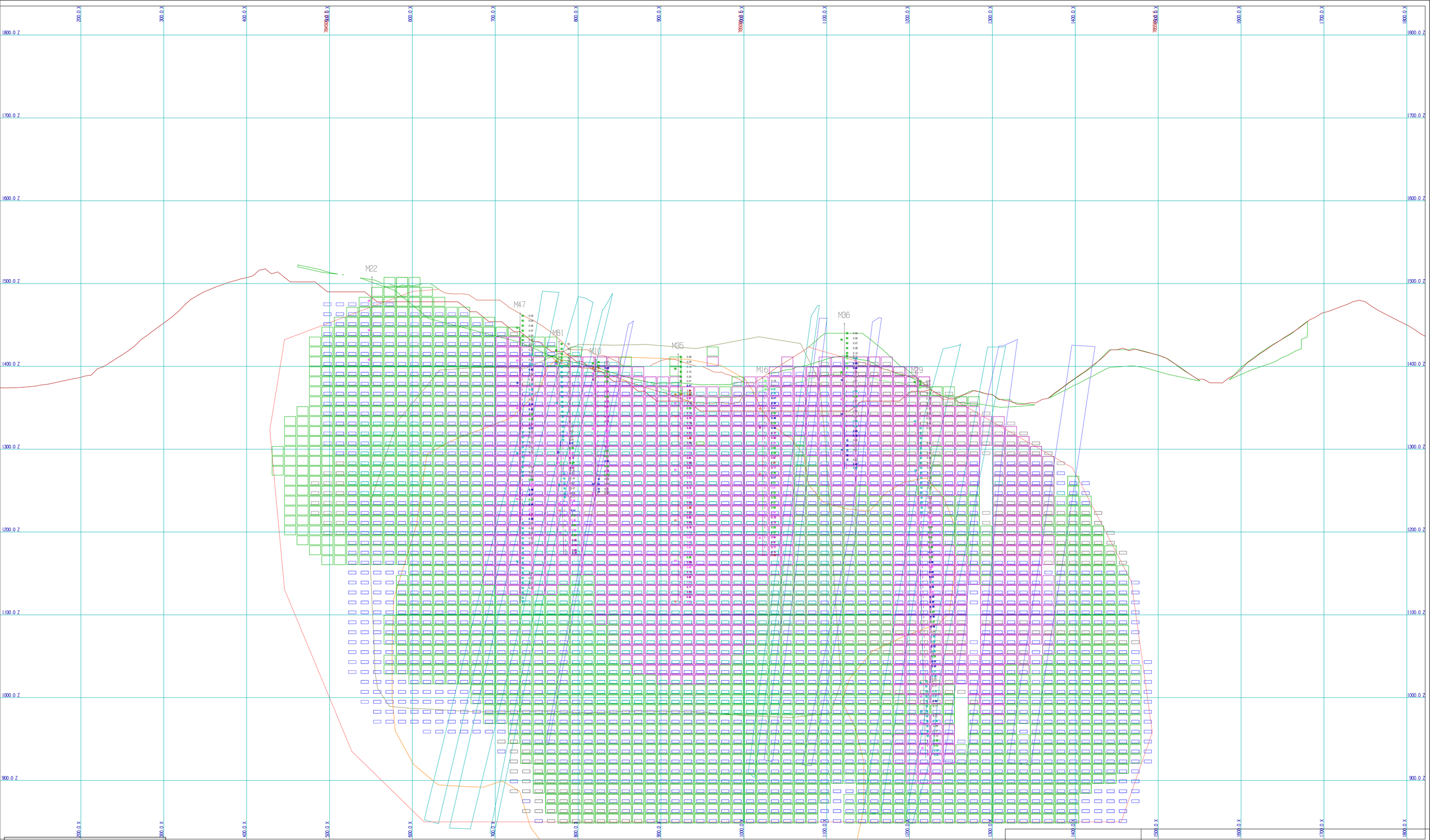
Section 3950EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:01:25

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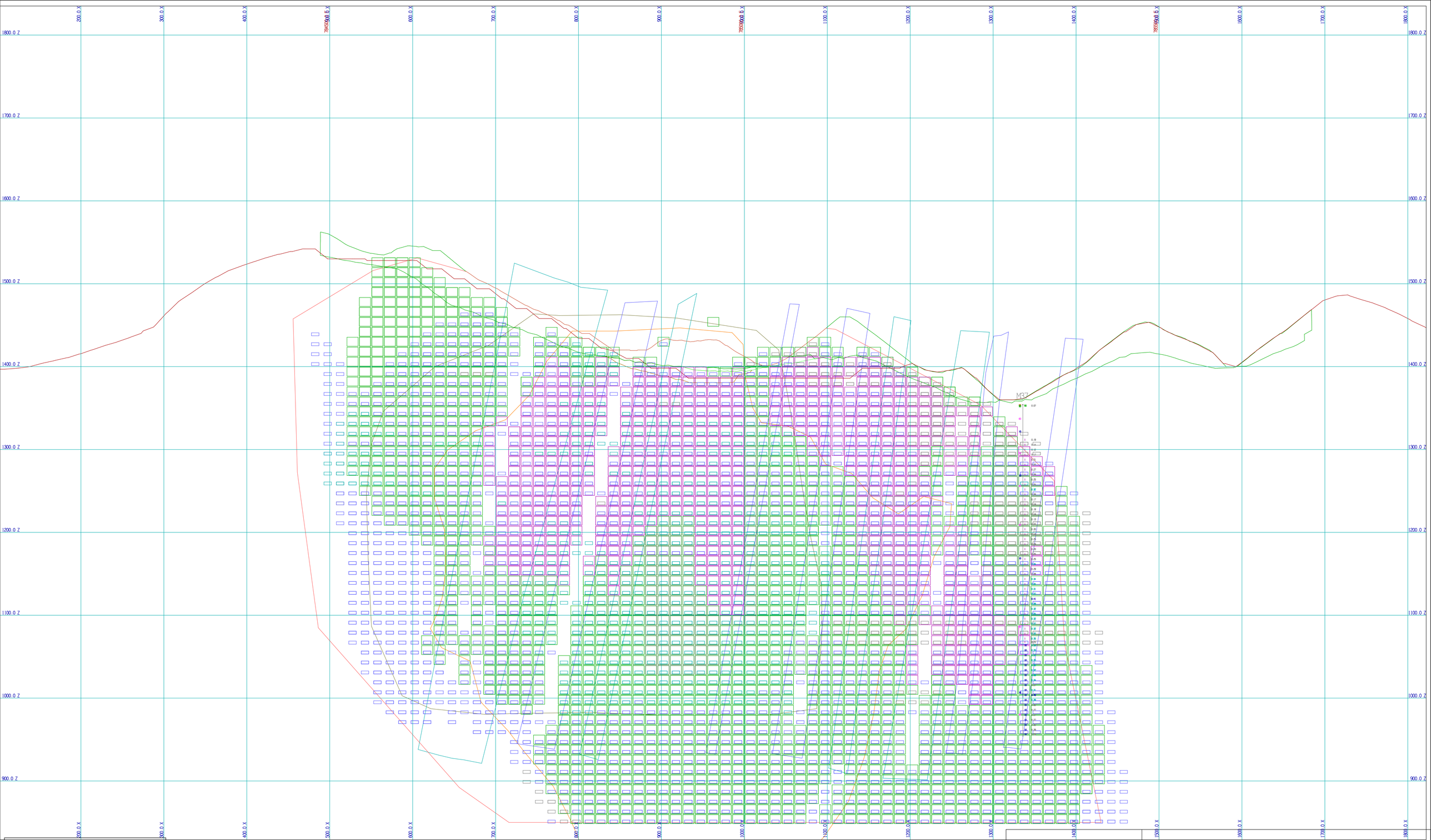
Section 3900EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:01:11

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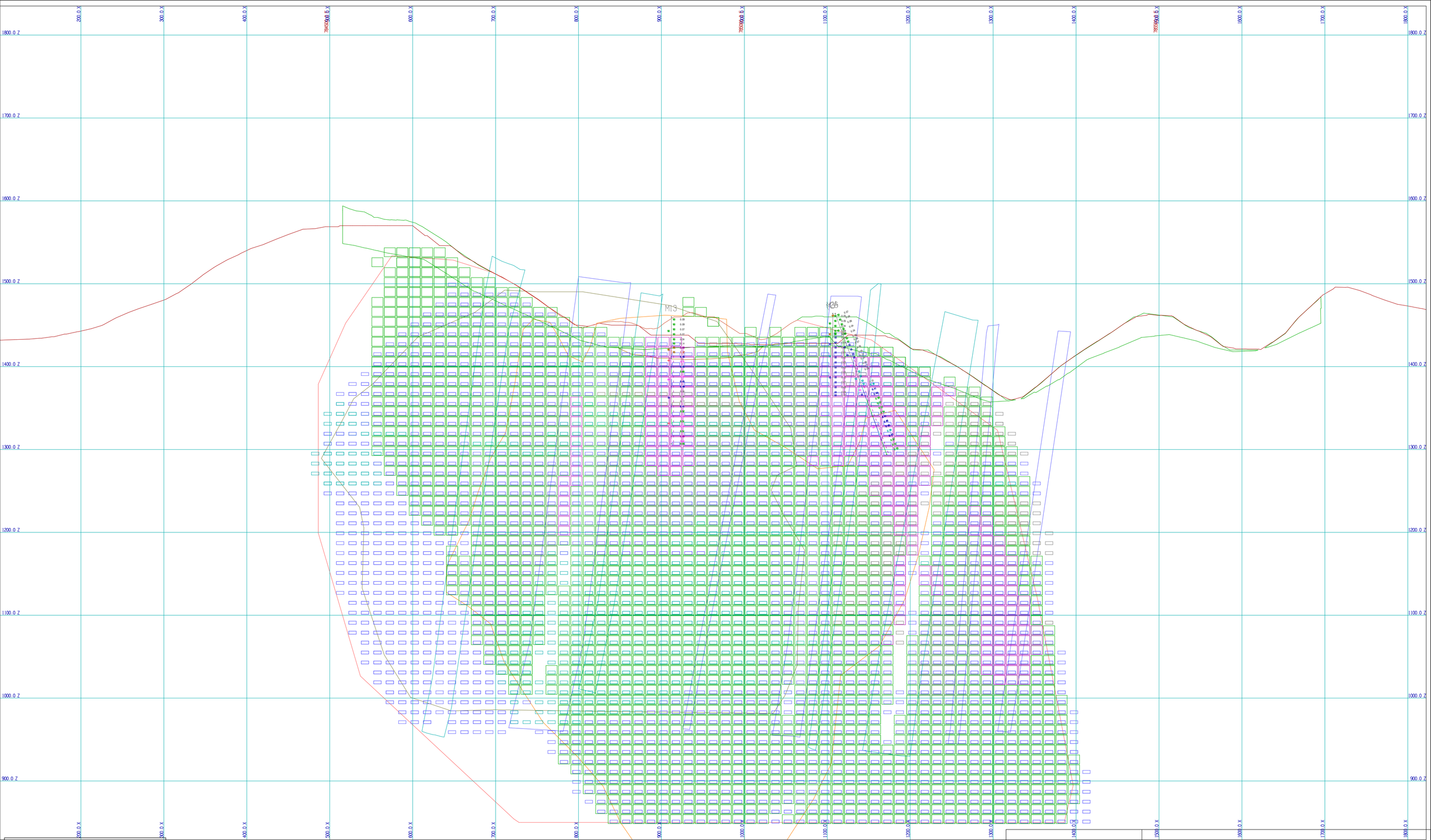
Section 3850EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:01:02

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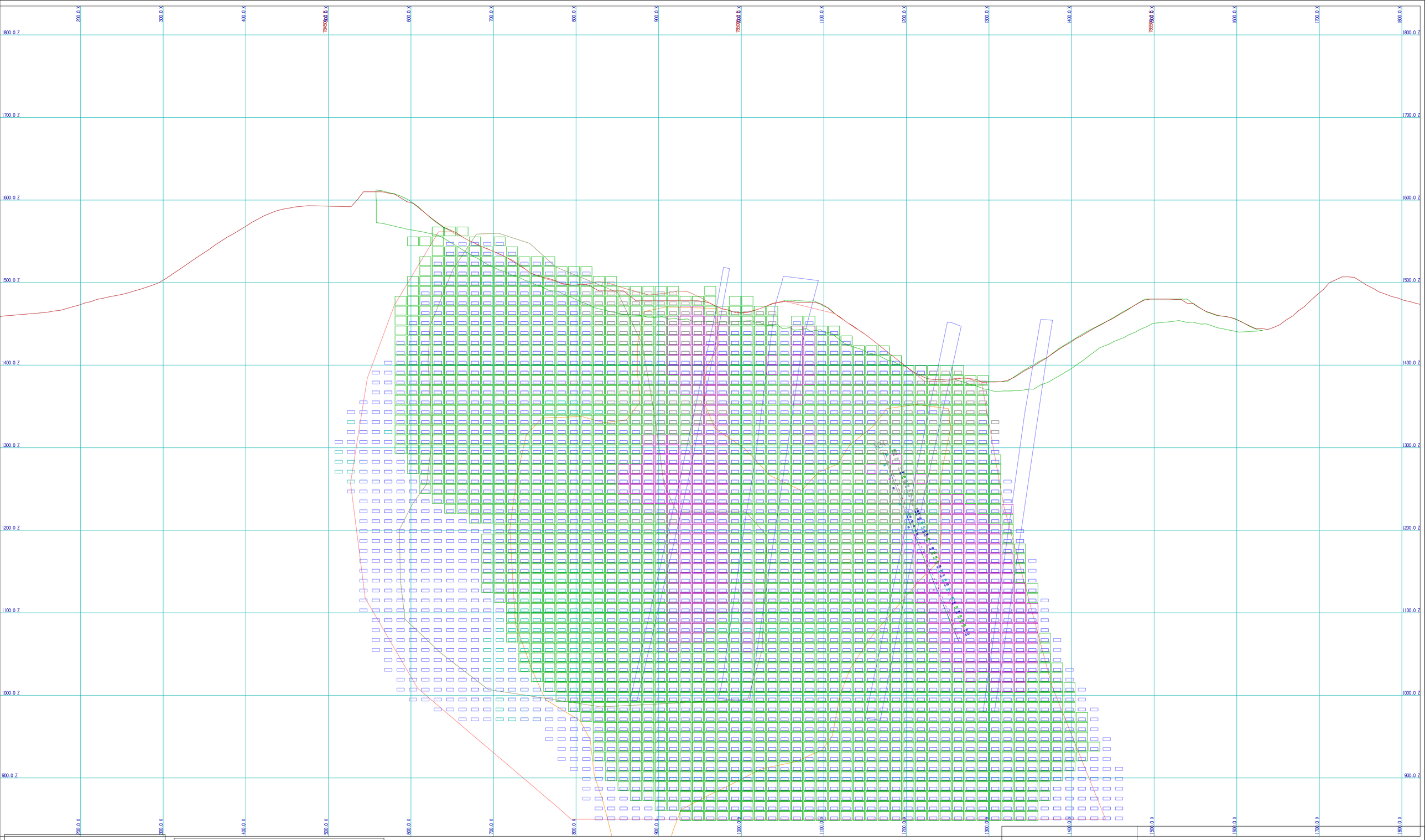
Section 3800EW Mirador Project

Block Model Plots Au Block Values

Class=blackoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:00:51

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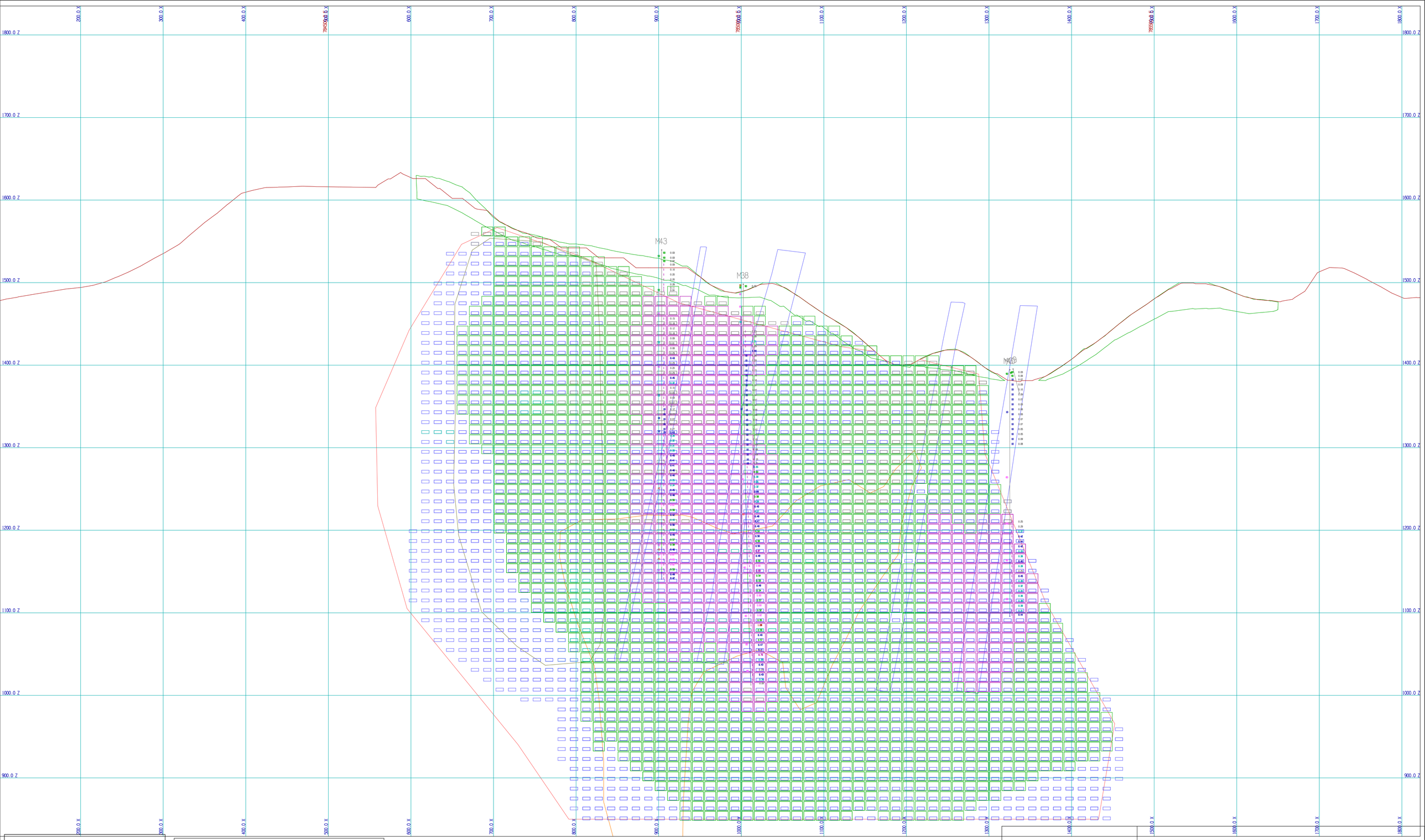
Section 3750EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100	
0.100	0.150	
0.150	0.200	
0.200	0.250	
0.250	0.300	
0.300	0.500	
0.500	10.000	

UNITS : METRES DATE: 04/10/20 TIME: 01.00.39

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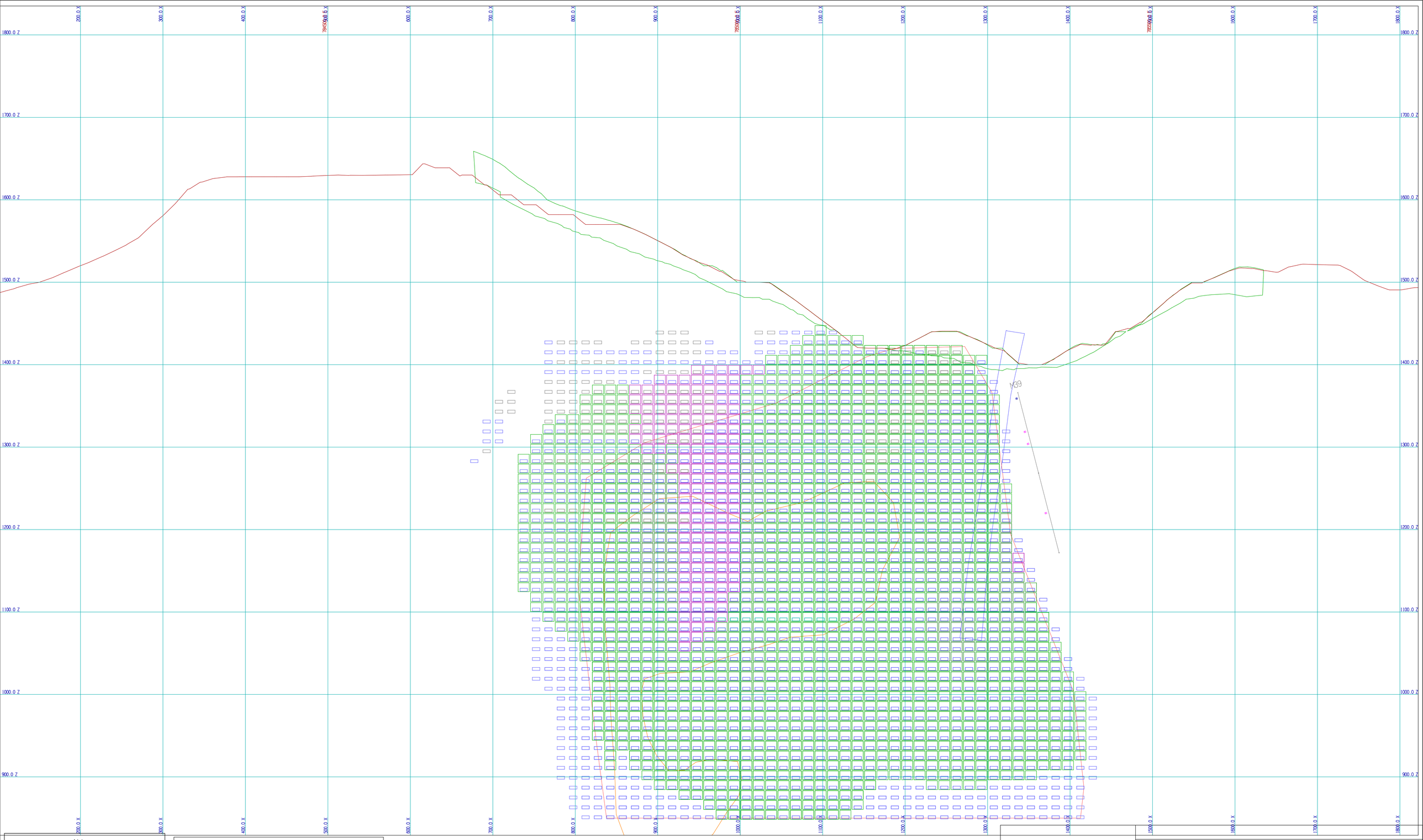
Section 3700EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:00:28

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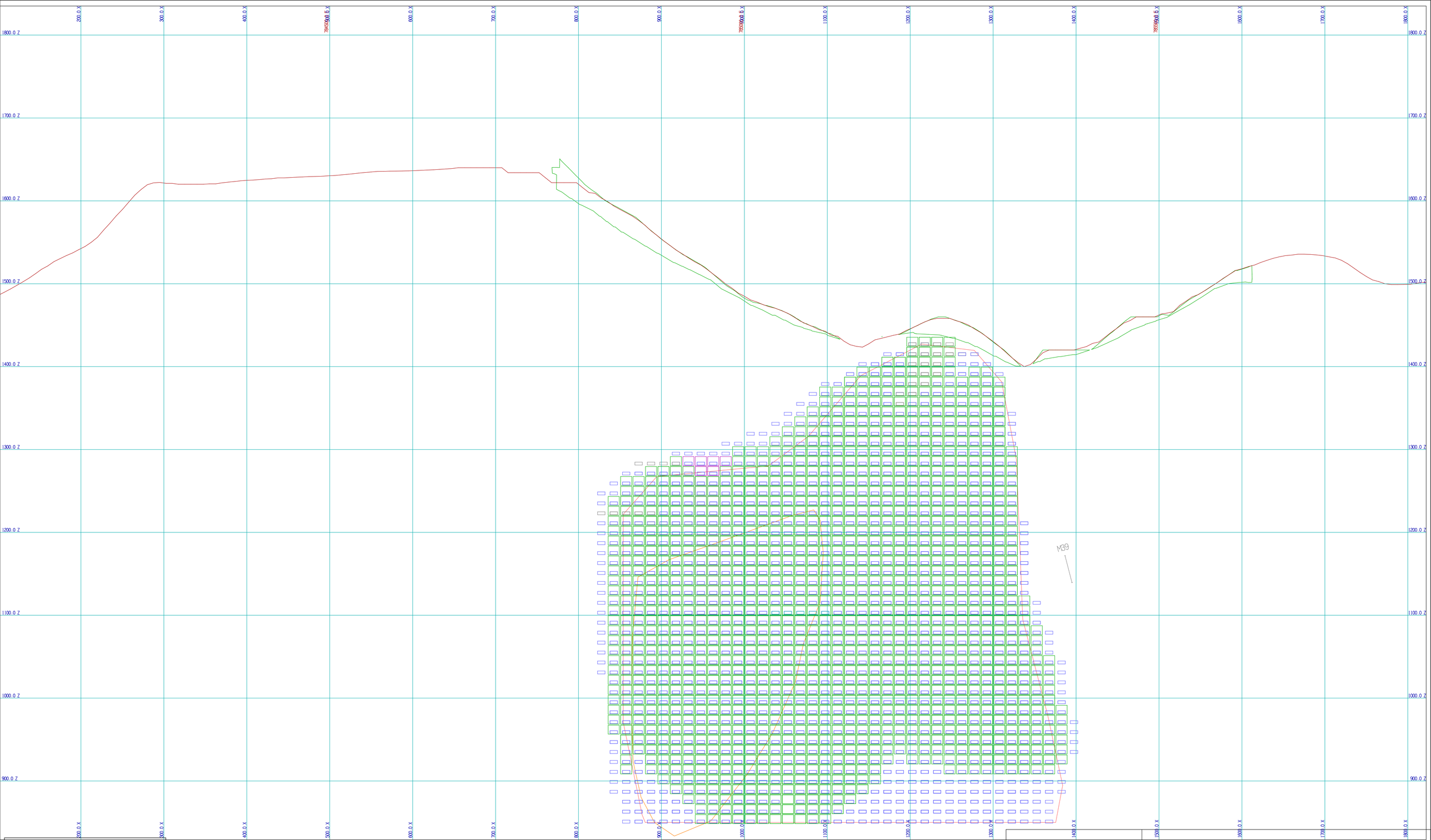
Section 3650EW Mirador Project

Block Model Plots Au Block Values

Class=blackoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geosoft Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:00:20

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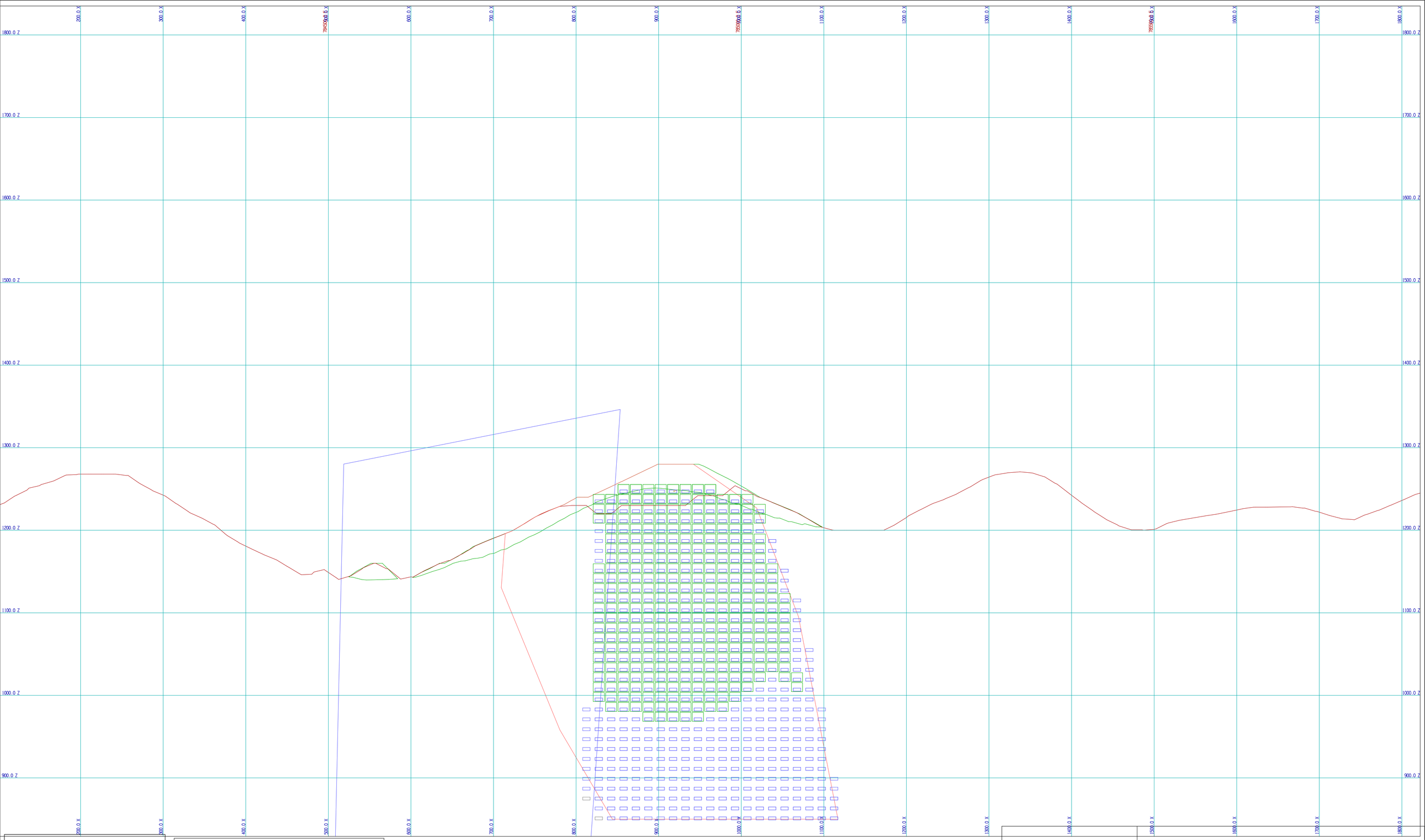
Section 3600EW Mirador Project

Block Model Plots Au Block Values

Class=blockoutline (No Outline=Unclassified)

Magenta=Indicated, Green=Inferred Scale1:2000

Software by Geovia Software International



AU

0.001	0.100
0.100	0.150
0.150	0.200
0.200	0.250
0.250	0.300
0.300	0.500
0.500	10.000

UNITS : METRES DATE: 04/10/20 TIME: 01:04:22

DRAWN BY :

Section 4700EW Mirador Project

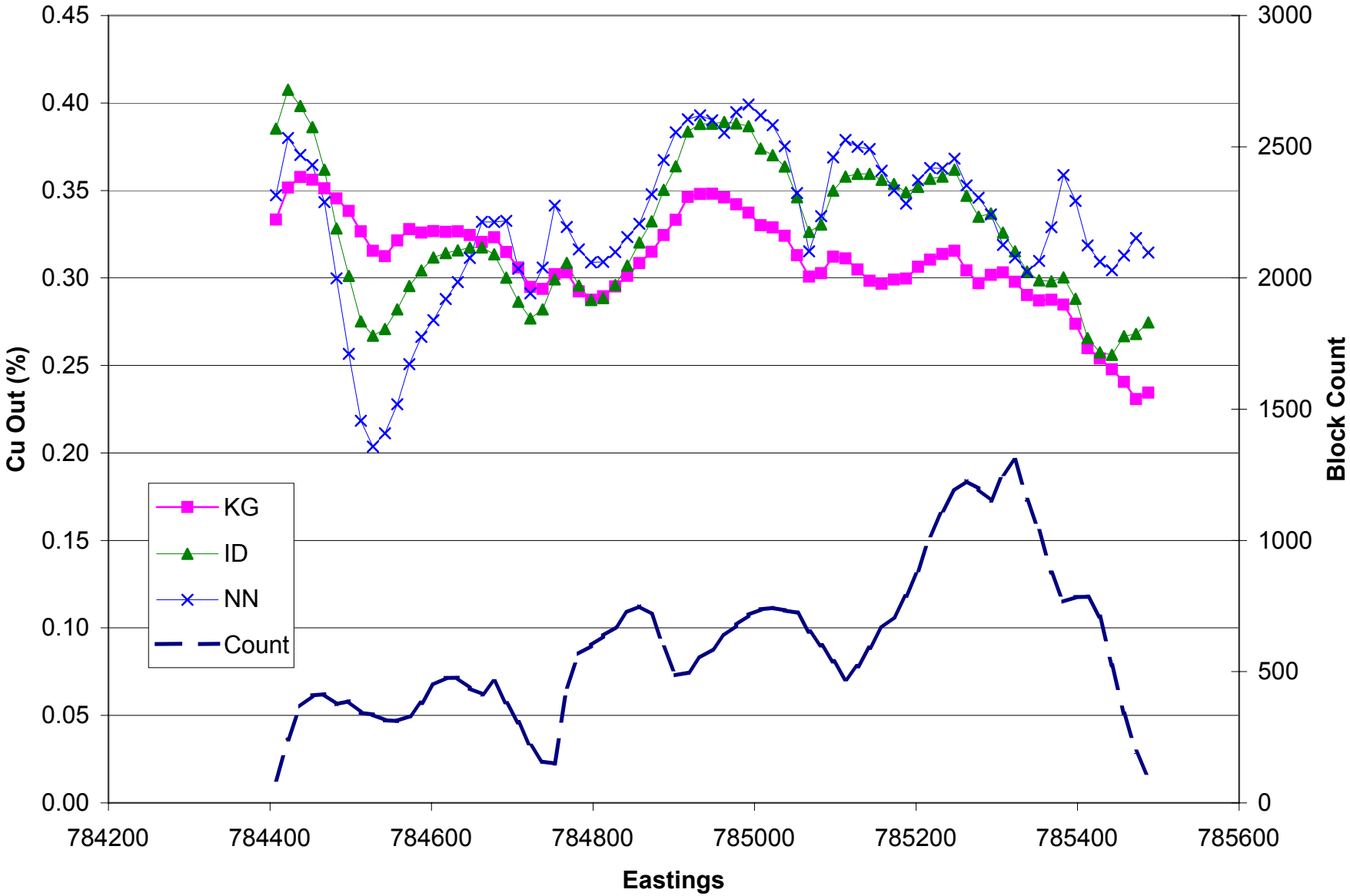
Block Model Plots Au Block Values

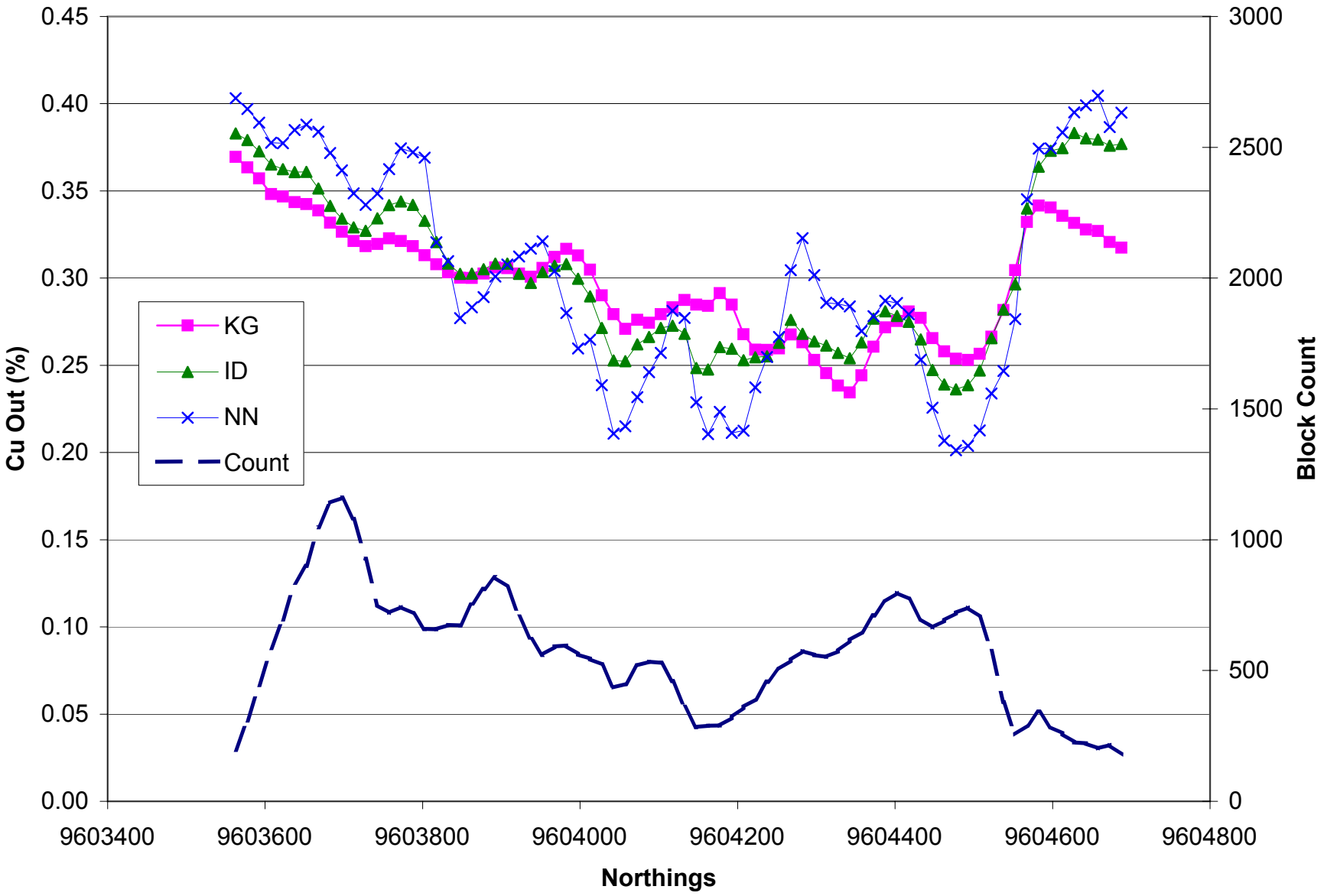
Class=blockoutline (No Outline=Unclassified)

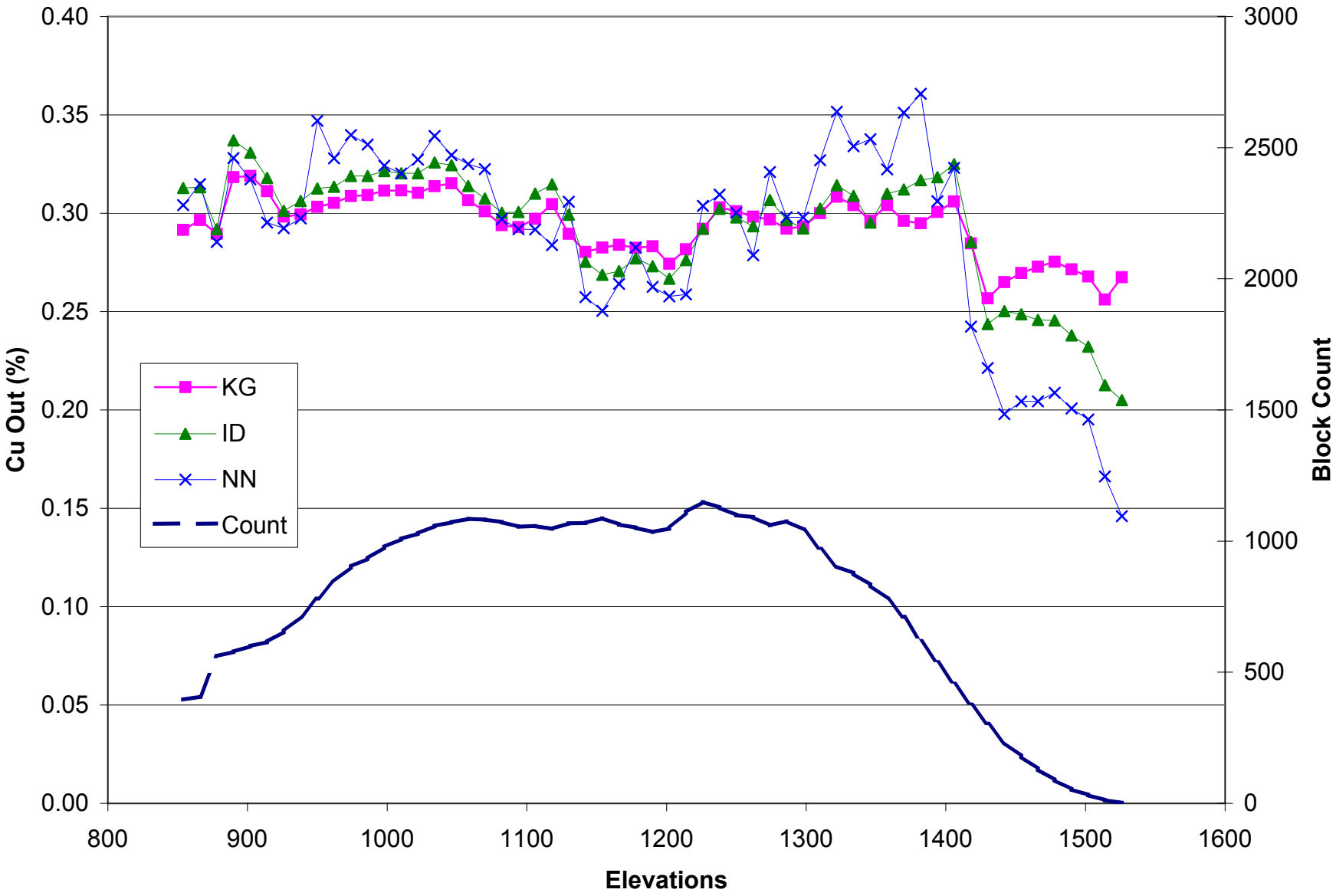
Magenta=Indicated, Green=Inferred Scale1:2000

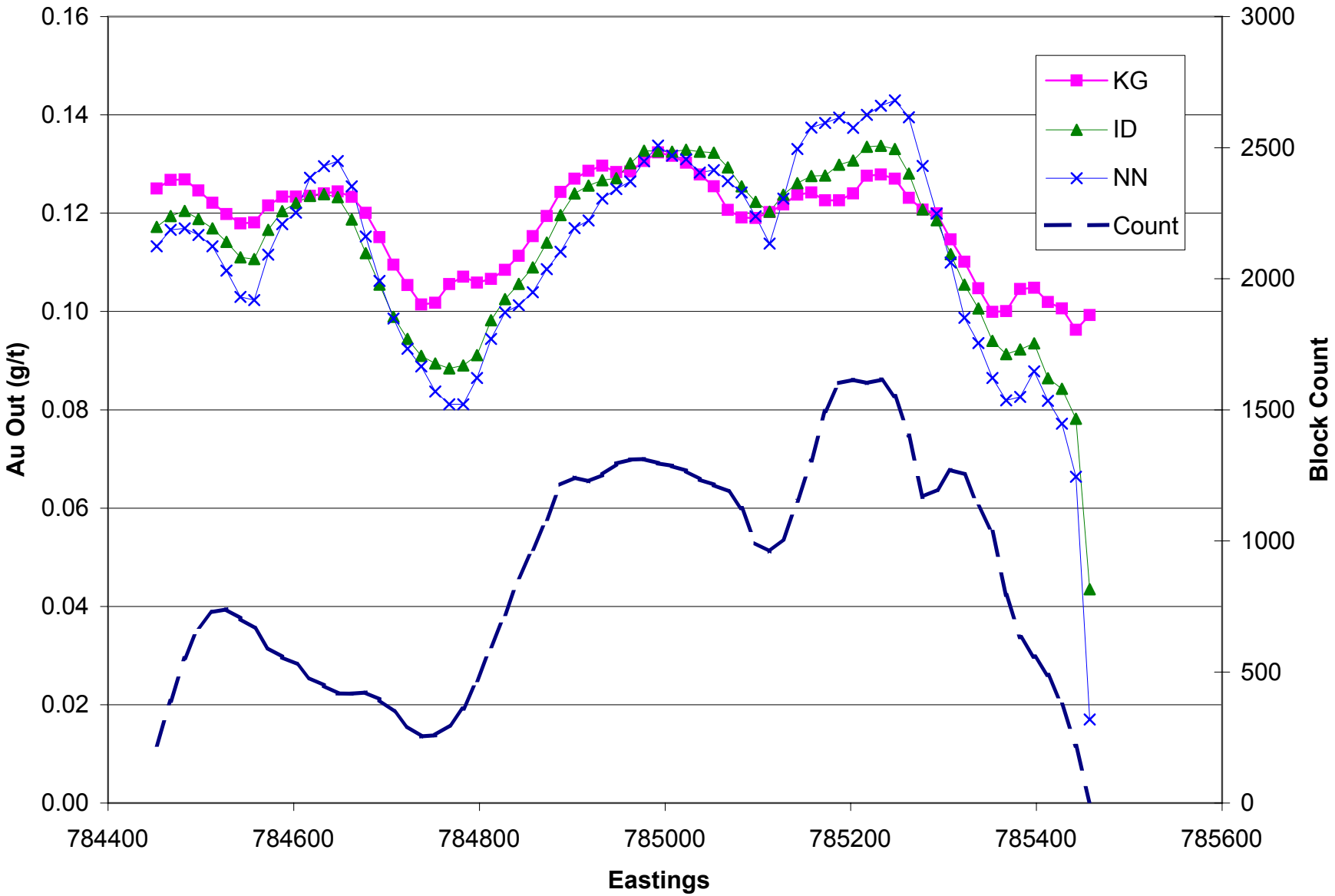
Software by Geovia Software International

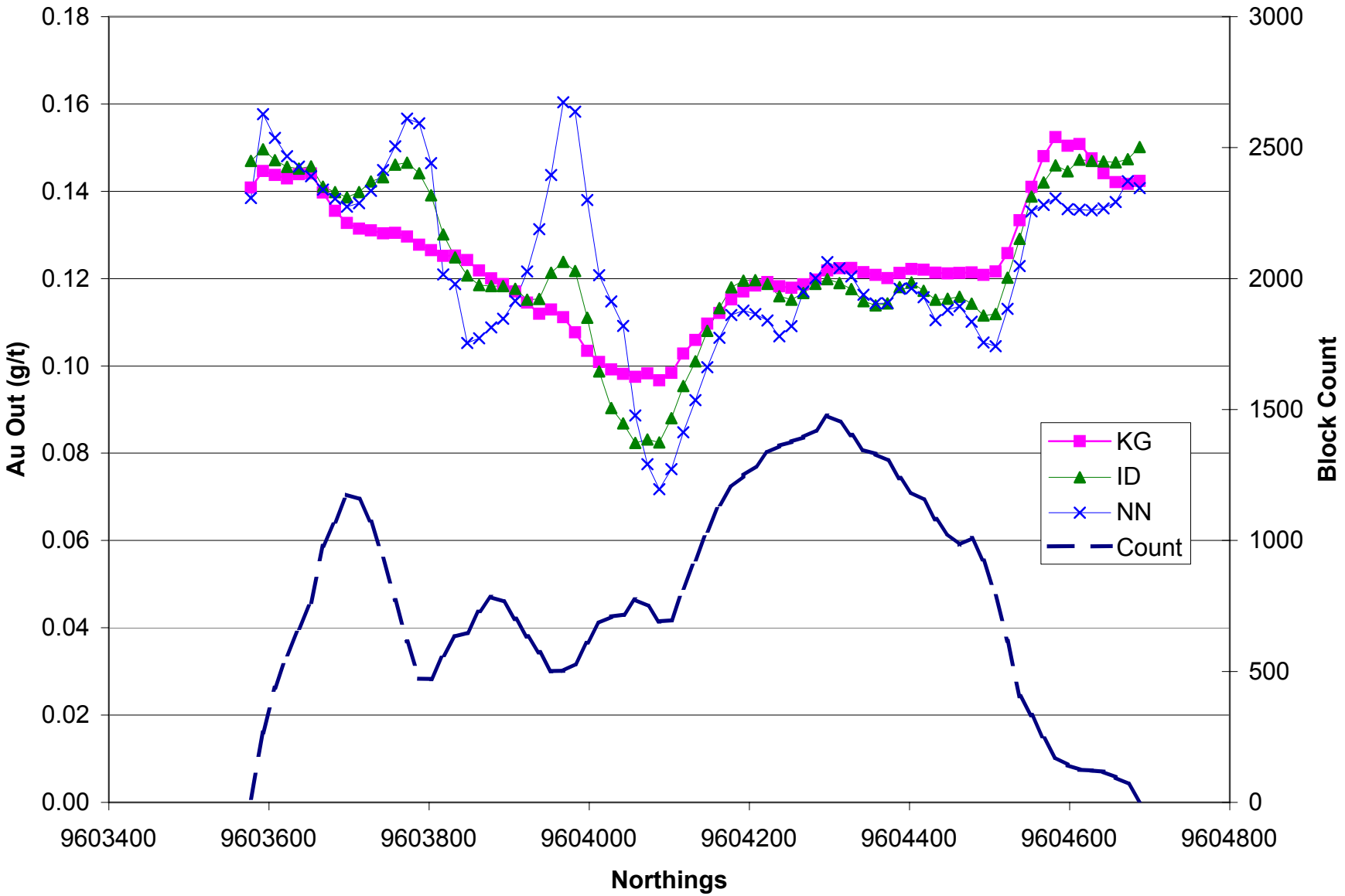
APPENDIX E COPPER AND GOLD SWATH PLOTS

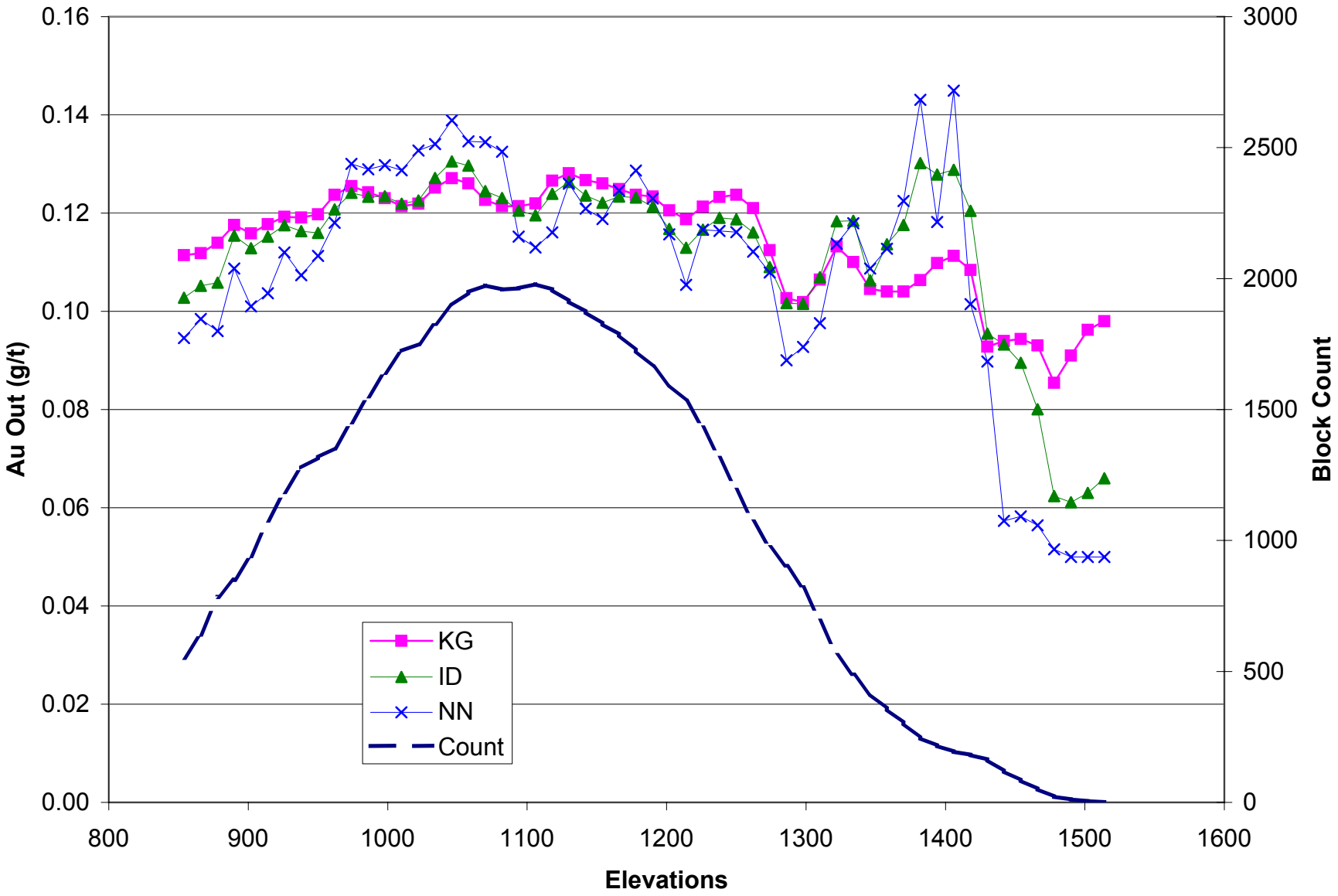

0.45
0.40
0.35
0.30
0.25
0.20
0.15
0.10
0.05
0.00
Cu Out (%)
3000
2500
2000
1500
1000
500
0
Block Count
KG
ID
NN
Count
784200
784400
784600
784800
785000
785200
785400
785600
Eastings

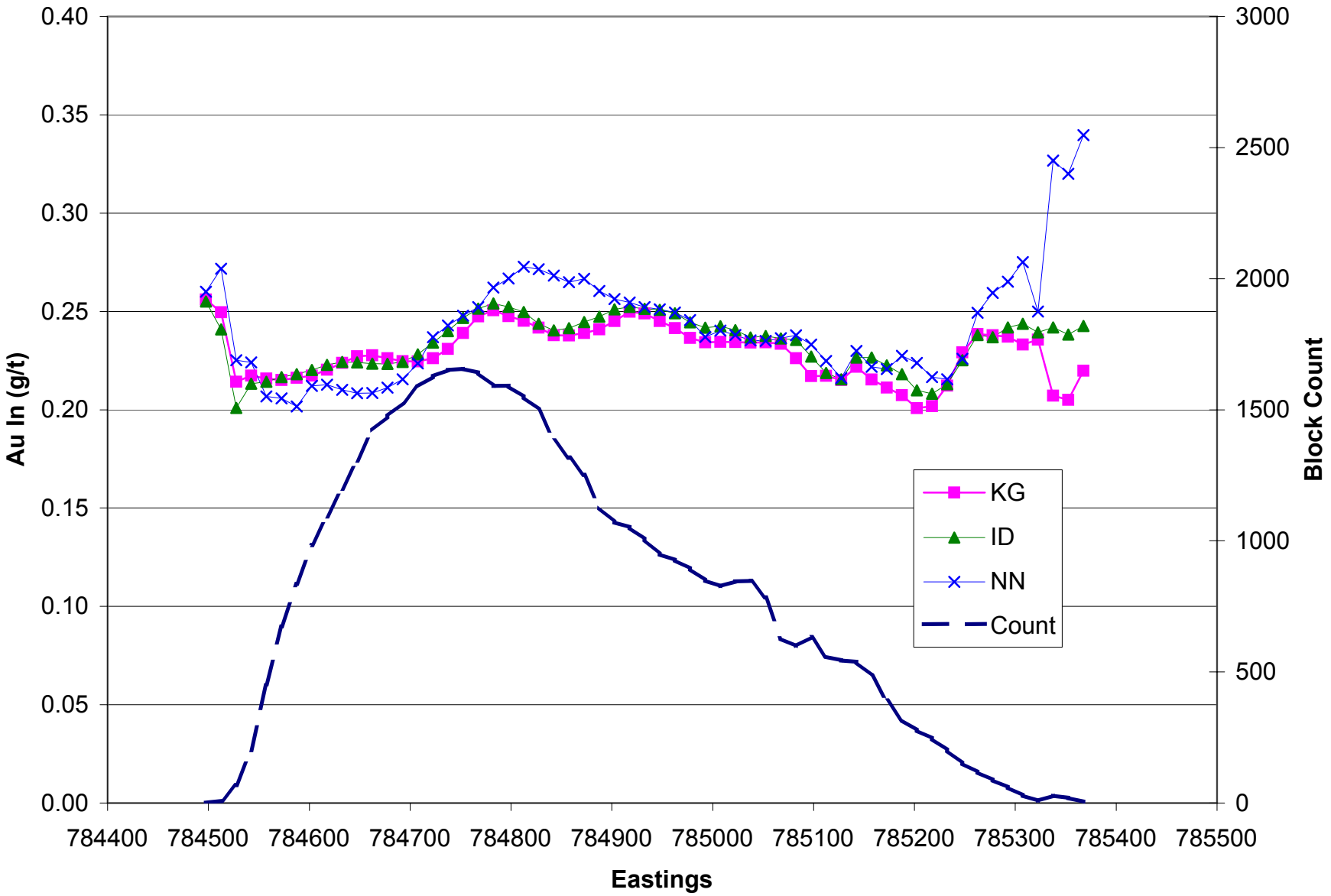

0.45
0.40
0.35
0.30
0.25
0.20
0.15
0.10
0.05
0.00
Cu Out (%)
3000
2500
2000
1500
1000
500
0
Block Count
KG
ID
NN
Count
9603400
9603600
9603800
9604000
9604200
9604400
9604600
9604800
Northings

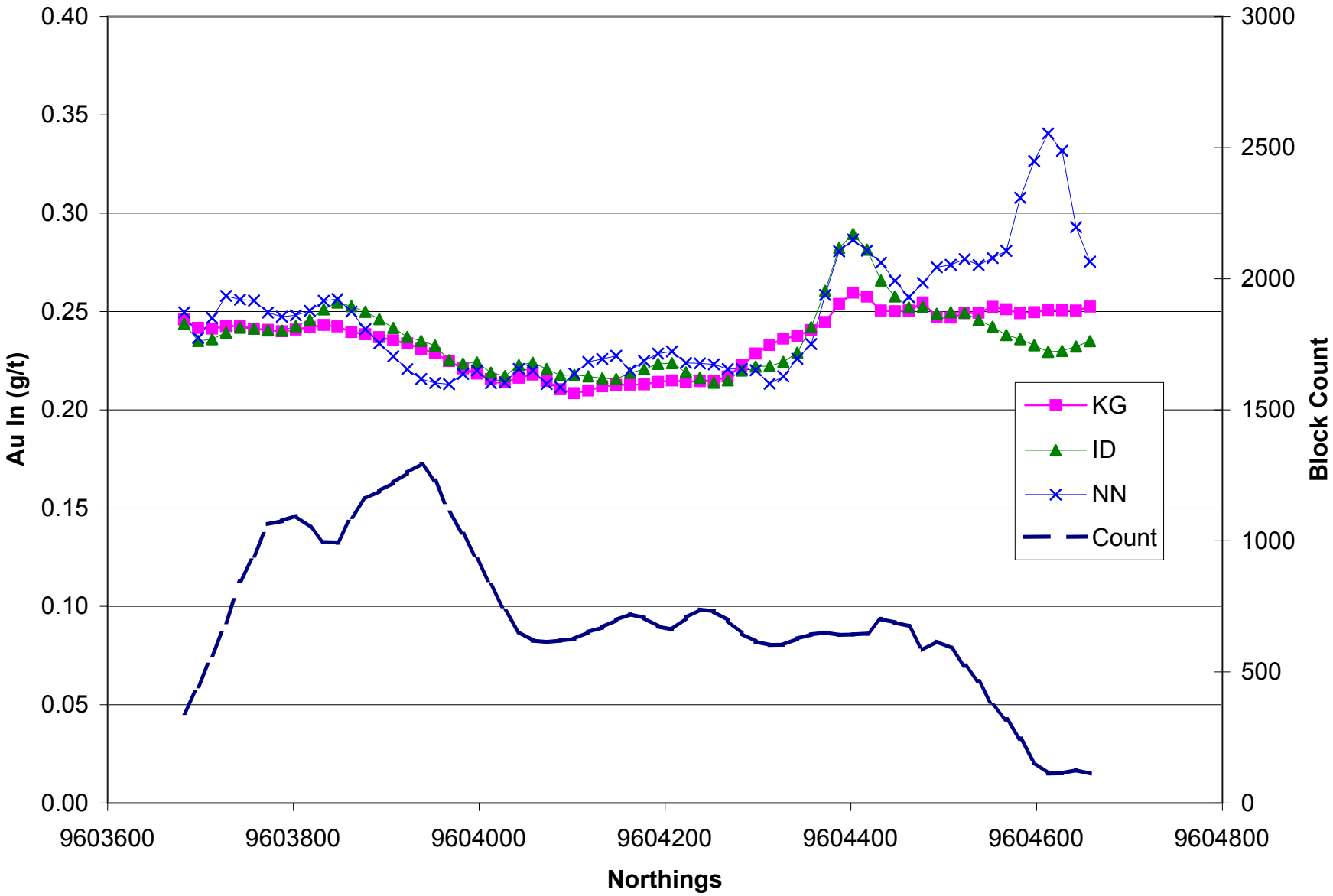

0.40
0.35
0.30
0.25
0.20
0.15
0.10
0.05
0.00
Cu Out (%)
3000
2500
2000
1500
1000
500
0
Block Count
KG
ID
NN
Count
800
900
1000
1100
1200
1300
1400
1500
1600
Elevations

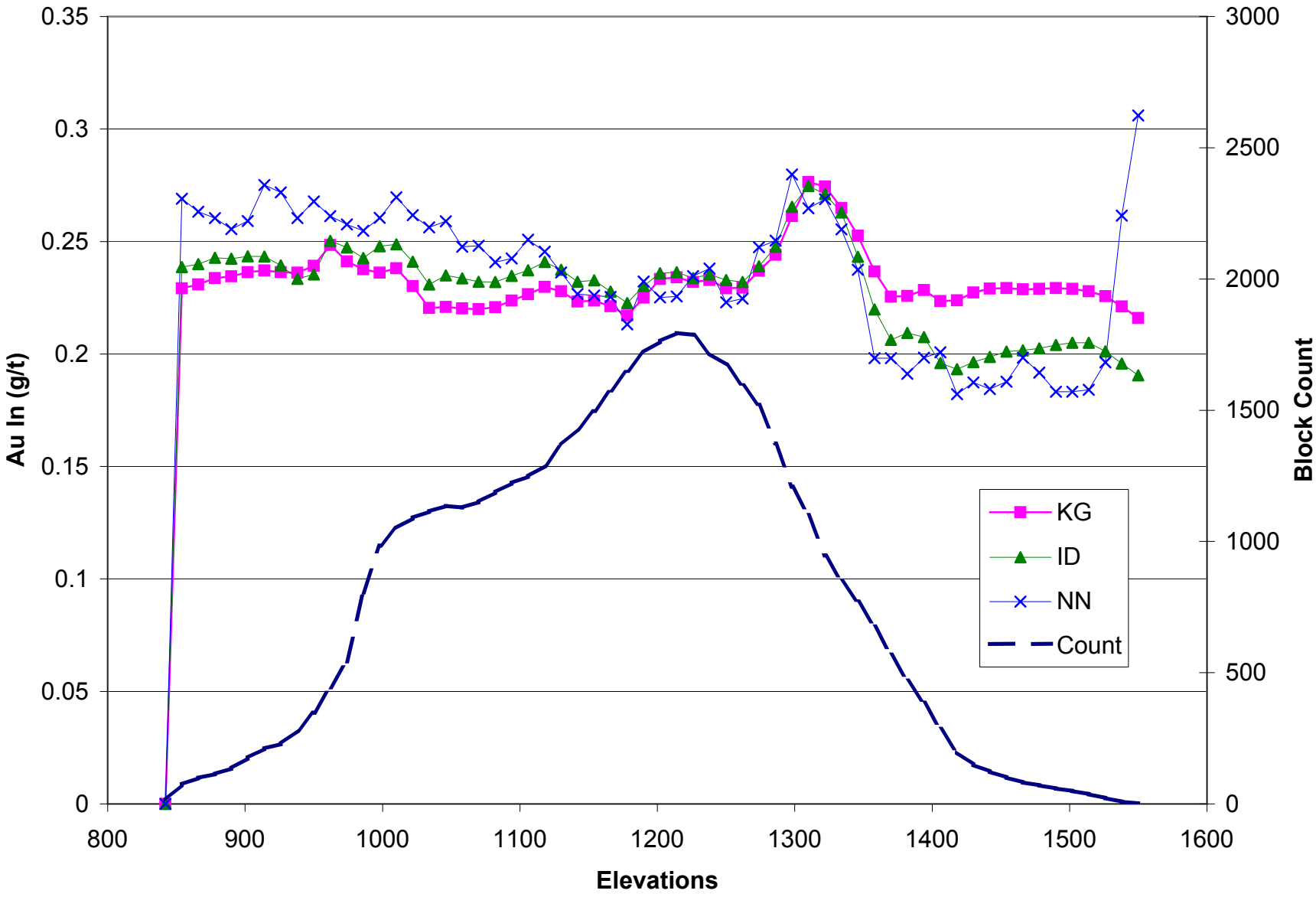

0.16
0.14
0.12
0.10
0.08
0.06
0.04
0.02
0.00
Au Out (g/t)
3000
2500
2000
1500
1000
500
0
Block Count
KG
ID
NN
Count
784400
784600
784800
785000
785200
785400
785600
Eastings


0.18
0.16
0.14
0.12
0.10
0.08
0.06
0.04
0.02
0.00
Au Out (g/t)
3000
2500
2000
1500
1000
500
0
Block Count
9603400
9603600
9603800
9604000
9604200
9604400
9604600
9604800
Northings
KG
ID
NN
Count


0.16
0.14
0.12
0.10
0.08
0.06
0.04
0.02
0.00
Au Out (g/t)
3000
2500
2000
1500
1000
500
0
Block Count
800
900
1000
1100
1200
1300
1400
1500
1600
Elevations
KG
ID
NN
Count


0.40
0.35
0.30
0.25
0.20
0.15
0.10
0.05
0.00
Au In (g/t)
3000
2500
2000
1500
1000
500
0
Block Count
784400
784500
784600
784700
784800
784900
785000
785100
785200
785300
785400
785500
Eastings
KG
ID
NN
Count


0.40
0.35
0.30
0.25
0.20
0.15
0.10
0.05
0.00
Au In (g/t)
3000
2500
2000
1500
1000
500
0
Block Count
9603600
9603800
9604000
9604200
9604400
9604600
9604800
Northings
KG
ID
NN
Count


0.35
0.3
0.25
0.2
0.15
0.1
0.05
0
Au In (g/t)
3000
2500
2000
1500
1000
500
0
Block Count
800
900
1000
1100
1200
1300
1400
1500
1600
Elevations
KG
ID
NN
Count